

Į

Engineers & Scientists Environmental Services Waste Management Water Resources Site Development Special Structures Geotechnical Analysis

April 25, 1988 13076.28

Ms. Margaret Guerriero Project Officer 5 HR 11 Region V, U.S. EPA 230 S. Dearborn Street Chicago, IL 60604

Re: Technical Memorandum Wausau Water Supply NPL Site

Dear Ms. Guerriero:

Warzyn is pleased to provide you with our Phase I Remedial Investigation Technical Memorandum for the Wausau Water Supply NPL site. The Technical Memorandum includes results of our Phase I Field Investigation and conclusions and recommendations for Phase II Work.

Please feel free to contact us if you have any questions.

Sincerely,

WARZYN ENGINEERING INC.

Craig S. Rawlinson

Cra'fg S. Rawlinson Project Hydrogeologist

Lemia Lourson

Dennis L. Iverson, P.E. Project Manager

DLI/ndj/CSR [ndj-104-82]

Enclosures: 11 Copies

cc: Ms. Michell DeBrock-Owens - WDNR (2)
Mr. Mark Giesfeld - WDNR (2)
Ms. Elissa Speizman, U.S. EPA (1)

Warzyn Engineering Inc. One Science Court University Research Park P.O. Box 5385 Madison, Wisconsin 53705 (608) 273-0440



Technical Memorandum 13076 Phase I Remedial Investigation Wausau Water Supply NPL Site Wausau, Wisconsin

Prepared for: United States Environmental Protection Agency Region V Chicago, Illinois

> Prepared by: Warzyn Engineering Inc. Madison, Wisconsin

> > April 1988



Phase I Remedial Investigation Wausau Water Supply NPL Site Wausau, Wisconsin

April 1988

## TABLE OF CONTENTS (Continued)

· · ·

•

	1. 2.	Contaminant Transport Modeling Procedure Results of Landfill Source Simulation	58 58
۷.	CONCLUS	IONS	60
VI.	RECOMME	DATIONS FOR PHASE II WORK	63
REFE	RENCES .	• • • • • • • • • • • • • • • • • • • •	65

# **TABLES**

TAD1 C			
TABLE	1	-	VOLATILE ORGANIC COMPOUND RETENTION ORDER
TABLE	2	-	SOIL GAS ANALYSIS DETECTION LIMITS
TABLE	3	-	TARGET VOC DETECTION LIMITS FOR WATER HEADSPACE
TABLE	4	-	OTHER VOC'S DETECTION LIMITS FOR WATER HEADSPACE
TABLE	5	-	SURFACE WATER SAMPLE LOCATIONS
TABLE	6	-	WELL LOCATION RATIONALE
TABLE	7	-	CONTRACT LABORATORY SOIL SAMPLE ANALYSES RATIONALE
TABLE	8	-	SURFACE WATER SAMPLE LOCATIONS
TABLE	9	-	VERTICAL GRADIENTS GROUNDWATER FLOW
TABLE	10	-	SUMMARY OF HYDRAULIC CONDUCTIVITY TESTS
TABLE	11	-	HENRY'S LAW CONSTANTS FOR SOME COMMON INDUSTRIAL SOLVENTS AT 25°C
TABLE	12	-	COMPARISON OF CONTRACT LABORATORY VS. FIELD GC RESULTS
TABLE	13	-	CROSS INDEX OF EXISTING WELL DESIGNATIONS

# DRAWINGS

13076-B10	-	LOCATION OF MUNICIPAL WELLS AND INDUSTRIAL SURVEYED
		BUSINESSES
13076-B11	-	MONITORING WELL, SAMPLE COLLECTION AND CROSS-SECTION
		LOCATION MAP
13076-B12	-	BEDROCK TOPOGRAPHIC MAP
13076-B13	-	GEOLOGIC CROSS-SECTION AA'
13076-B14	-	GEOLOGIC CROSS-SECTION BB'
13076-B15	-	POTENTIOMETRIC SURFACE MAP (1/7-8/88)
13076-B16	-	POTENTIOMETRIC SECTION AA'
13076-B17	-	POTENTIOMETRIC SECTION BB'
13076-B18	-	SOIL GAS TEST LOCATIONS, WEST STUDY AREA
13076-B19	-	RESULTS OF SOIL GAS INVESTIGATION, WEST STUDY AREA
13076-B20	-	RESULTS OF SOIL GAS INVESTIGATION. EAST STUDY AREA
13076-B21	-	PRELIMINARY ESTIMATE OF TOTAL CHLORINATED ETHENES
		OCCURRENCE IN THE AQUIFER
13076-B22	-	ISOCONCENTRATION SECTION AA'
13076-B23	-	ISOCONCENTRATION SECTION BB'
13076-B24	-	GROUNDWATER FLOW MODEL FINITE DIFFERENCE GRID
13076-B25	-	SIMULATED HEAD MAP. APRIL 1987
13076-B26	-	SIMULATED HEAD MAP. SEPTEMBER 1985
13076-B27	-	EXTENT OF CONTAMINANT MIGRATION. SIMULATED LANDETLL SOURCE
13076-A15	-	CLP LAB VOC VS. FIELD GC
13076-A16	-	INDUSTRIAL SURVEY. MARATHON FLECTRIC AND THE ABANDONED
		CITY LANDFILL
	13076-B10 13076-B11 13076-B12 13076-B13 13076-B13 13076-B14 13076-B15 13076-B16 13076-B17 13076-B19 13076-B19 13076-B21 13076-B21 13076-B22 13076-B23 13076-B24 13076-B25 13076-B25 13076-B27 13076-A15 13076-A16	13076-B10 - 13076-B11 - 13076-B12 - 13076-B13 - 13076-B14 - 13076-B15 - 13076-B15 - 13076-B17 - 13076-B18 - 13076-B19 - 13076-B20 - 13076-B21 - 13076-B21 - 13076-B23 - 13076-B24 - 13076-B25 - 13076-B26 - 13076-B27 - 13076-A15 - 13076-A16 -



.

#### TABLE OF CONTENTS (Continued)

#### APPENDICES

APPENDIX A - FIELD METHODS FOR EXPLORATION AND SOIL SAMPLING APPENDIX B - BORING LOGS

B.1 - WARZYN PERFORMED BORING LOGS B.2 - DEPARTMENT OF TRANSPORTATION BORING LOGS

APPENDIX C - WELL CONSTRUCTION DETAILS

APPENDIX D - SOIL GAS INVESTIGATION RESULTS

APPENDIX E - RESULTS OF ROUND 1 SAMPLE DESCRIPTIONS AND GENERAL WATER QUALITY PARAMETER ANALYSES

APPENDIX F - RESULTS OF ROUND 1 VOLATILE ORGANIC COMPOUND ANALYSES

APPENDIX G - RESULTS OF FIELD GAS CHROMATOGRAPH AND CONTRACT LABORATORY ANALYSES OF GROUNDWATER SAMPLES COLLECTED DURING DRILLING

G.1 - CLP LAB RESULTS VOC SAMPLES COLLECTED DURING DRILLING G.2 - FIELD GC VOC SAMPLES COLLECTED DURING DRILLING

APPENDIX H - SUMMARY OF MONITORING WELL CONSTRUCTION DETAILS AND OBSERVED GROUNDWATER ELEVATIONS

APPENDIX I - HYDRAULIC CONDUCTIVITY TEST METHODS AND RESULTS

APPENDIX J - GROUNDWATER MODEL INPUT PARAMETERS

APPENDIX K - OBSERVED VS. SIMULATED WATER LEVELS USED IN FLOW MODEL CALIBRATION

APPENDIX L - INDUSTRIAL SURVEY REPORT

[kam-600-50b]



# TABLE OF CONTENTS

. . . .

.

ľ

J

1

I

,

			<u>PAGE</u>				
I.	INT	ITRODUCTION					
	A. B.	BACKGROUND	1 4				
II.	FIE	LD INVESTIGATION METHODS	7				
	A. B.	SITE PREPARATION EXISTING WELL SAMPLING (ROUND I)	7 8				
		<ol> <li>Purpose</li> <li>Sample Collection Procedures</li> </ol>	8 9				
	с.	SOIL GAS SAMPLING	10				
		<ol> <li>Purpose</li> <li>Sample Collection Procedures</li> </ol>	10 11				
	D. E.	FIELD ANALYTICAL METHODS FOR VOCS ON-SITE ANALYSIS OF SURFACE WATER SAMPLES	12 14				
		<ol> <li>Purpose</li> <li>Sample Collection Procedures</li> </ol>	14 15				
	F.	DRILLING AND MONITORING WELL INSTALLATION	15				
		<ol> <li>Purpose</li> <li>Drilling Equipment</li> <li>Drilling Methods</li> <li>Soil Sampling</li> <li>Groundwater Sampling</li> <li>Geophysical Logging</li> <li>Well Installation</li> <li>Well Development</li> <li>Decontamination</li> </ol>	16 16 17 18 19 19 20 21				
	G.	GROUNDWATER SAMPLING (ROUND II)	21				
		<ol> <li>Purpose</li> <li>Sample Collection Procedures</li> </ol>	21 21				
	Η.	SURFACE WATER AND SEDIMENT SAMPLING	22				
		<ol> <li>Purpose</li> <li>Sample Collection Procedures</li> </ol>	22 22				
	I.	HYDRAULIC CONDUCTIVITY TESTING	23				



.

# TABLE OF CONTENTS (Continued)

۰.

· .

		1. 2.	Purpose Test Methods	23 23		
	J. K.	LOC/ WATE	ATION AND ELEVATION SURVEY	24 25		
		1. 2.	Purpose Procedure	25 25		
III.	RESI	JLTS	OF THE PHASE I FIELD INVESTIGATION	26		
	Α.	GEOI	LOGY	26		
		1. 2.	Bedrock Geology Glacial Geology	26 27		
	Β.	HYDI	ROGEOLOGY	30		
		1. 2.	Groundwater Flow	30 34		
	C.	SOI	L GAS RESULTS	35		
		1. 2. 3.	West Study Area East Study Area Discussion of Soil Gas Results	35 36 38		
	D.	SURI	FACE AND GROUNDWATER QUALITY	42		
		1. 2.	General Water Quality Parameters Occurrence of Total Chlorinated Ethenes in the Aquifer	42 43		
IV.	PRE	PRELIMINARY GROUNDWATER MODELING				
	Α.	INTI	RODUCTION	49		
		1. 2.	Available Data Model Selection	49 50		
	Β.	MODI	EL DEVELOPMENT	50		
		1. 2.	Hydrogeology Discretization and Model Setup	50 51		
	с.	FLO	M MODEL CALIBRATION	54		
		1. 2. 3. 4.	Calibration Data Calibration Procedure Parameter Selection Groundwater Flow Model Results	54 54 54 56		
	D.	CON	TAMINANT TRANSPORT MODELING	58		



. .

ŕ

ķ

ľ

į

#### PHASE I INVESTIGATION TECHNICAL MEMORANDUM WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

#### I. INTRODUCTION

#### A. BACKGROUND

The City of Wausau is located along the Wisconsin River in north central Marathon County, Wisconsin. The City operates six ground water production wells, which provide water for approximately 33,000 residents. Five of the production wells are located on the north side of the City. Production well CW8 is located adjacent to the Wausau Municipal Airport, on the south side of the City. The water from Production Well CW8 contains high iron concentrations, therefore the well is used only during peak demand periods. Production wells CW6, CW7 and CW9 are located west of the Wisconsin River and are collectively referred to as the West Well Field. The West Well Field is located in a predominantly residential area. However, Marathon Electric Inc., a manufacturing facility, currently occupies a large area south of the West Well Field. Production Wells CW3 and CW4 are located on the east side of the Wisconsin River and are referred to as the East Well Field. The East Well Field is located in a predominantly industrial section of the City. Area businesses include: Marathon Box Company, Marathon Press Company, Wausau Chemical Company, Wausau Energy Company and Wergin Construction Company. Refer to Drawing 13076-B10 for the location of the northern municipal production wells and area businesses.

The six production wells are screened in an aquifer of glacial outwash and alluvial sand and gravel deposits adjacent to the Wisconsin River. This unconfined aquifer supplies nearly all potable, irrigation and industrial water to residents and industries in this portion of the Wisconsin River Valley. The aquifer formed when the ancestral Wisconsin River eroded a deep valley into the Precambrian aged igneous bedrock. This valley was widened by continental glaciation during the Pleistocene glacial epoch. When the glaciers retreated from north central Wisconsin, coarse outwash sand and gravel sediments were deposited within the valley. Continued erosion of the



١

upland areas resulted in the deposition of additional fluvial sediments. Within the study area (see Drawing 13076-B10), the aquifer ranges from 0 to 160 feet thick and has an irregular base and lateral boundaries.

Volatile organic compounds (VOCs) were first discovered in Production Well CW4 in 1975 after the well had been placed in service during an extended dry spell. Analyses conducted at that time indicated tetrachloroethylene (PCE) and trichloroethylene (TCE) concentrations of approximately 1 ug/L (WDNR, 1975). Since Production Well CW4 was only used during peak demand periods. the PCE and TCE concentrations were not considered to pose a health risk. In 1982, the City discovered higher levels of VOCs in the City distribution system. Further analysis indicated Production Wells CW3, CW4 and CW6 were contaminated or became contaminated by volatile halogenated hydrocarbons (VHHs). Petroleum related compounds (primarily toluene) were also detected at relatively low levels ( $\langle 25 \text{ ug/L} \rangle$  in Production Wells CW3 and CW4. In addition, trihalomethanes 1 (THMs) were detected in the distribution system but were attributed to chlorination in the water treatment process. In order to reduce the VHH concentrations, the City instituted a program where uncontaminated water from Production Wells CW9, and CW7 was blended with water from wells CW3, CW4 and CW6 to dilute the VHH concentrations to meet demand.

The City, with the support of the Wisconsin Department of Natural Resources (WDNR), made several attempts to mitigate the problem and locate the source. Monitoring wells were installed and sampled and an unsuccessful attempt was made to aerate the water by modifying treatment practices.

In 1983, the U.S EPA awarded the City of Wausau a Federal grant to help fund the design and installation of a packed tower VOC stripper in order to provide sufficient water of acceptable quality to City residents. As an interim measure in May 1984, the U.S. EPA installed a granular activated carbon (GAC)



Note: Trihalomethanes (THMs) are also volatile halogenated hydrocarbons (VHHs) but will be treated separately for the sake of discussion. In this report, VHHs is used generically to refer to chlorinated ethene compounds, including: PCE, TCE, 1,2DCE, 1,1DCE and vinyl chloride.

treatment system on Production Well CW6. Air strippers were installed in the Summer and Fall of 1984 at the water treatment plant to treat water from CW3 and CW4. Subsequently, the GAC system was removed from service in October, 1984. The City has been blending treated water with well water from uncontaminated supply sources (Production Wells CW7 and CW9) to reduce VHH concentrations in the water supply distribution system.

-3-

Data indicate that prior to treatment (pre-July 1984), the water supply consistently contained trichloroethene (TCE) with concentrations ranging from detectable levels (> 1 ug/L) to 80 ug/L. Lower levels of tetrachloroethene (PCE) and 1,2-dichloroethene (DCE) were identified shortly after discovery of the contamination, probably before blending had reduced the levels of VHHs. Following installation of the packed tower VOC stripper treatment systems, the water supply distribution system has had relatively low levels of VHHs (generally  $\langle 5 ug/L \rangle$ ). These levels are dependent on continued effective operation of the treatment system, the influent VHH concentrations for each well, and continued use of the two uncontaminated wells (Production Wells CW7 and CW9).

Previous investigations have identified several potential point sources of VHH contamination in the vicinity of City production wells (refer to the list of References, pp. 65-66 for complete titles and dates of available reports). Becher-Hoppe Engineers, Inc. was contracted by the City of Wausau to conduct a remedial investigation in the vicinity of Production Well CW3. The study concentrated on the Wergin Construction Co. property, the former site of a City of Wausau maintenance garage. Foth & Van Dyke and Associates, Inc. performed a groundwater investigation at the Wausau Energy Company property in order to determine the effect of past bulk oil operations at the site. STS Consultants Ltd. have performed groundwater investigations at the Wausau Chemical Co. and instituted a groundwater extraction and treatment system to remediate effects of past VHH releases from their facility operations. Twin City Testing and Engineering Laboratory, Inc. conducted investigations in the East Well Field vicinity on behalf of the Wisconsin Department of Natural Resources (WDNR). Roy F. Weston Inc. conducted an investigation of both the East and West Well Fields as part of the U.S. EPA emergency response action.



13076.28

CH<sub>2</sub>M Hill Inc. was contracted by the WDNR to perform a hydrogeologic investigation of the abandoned City of Wausau landfill, located on property presently owned by Marathon Electric Company. RMT Inc., representing Marathon Electric, in conjunction with Geraghty & Miller, Inc., representing the City of Wausau, performed a hydrogeologic investigation to determine the source of TCE in the groundwater in the vicinity of City Production Well CW6. Geraghty & Miller Inc. also installed several wells in the East Well Field in order to investigate VHH contamination of Production Well CW3. As a result of these investigations, only Wausau Chemical has been identified as a source of VHH contamination of City Production Wells.

#### **B. PURPOSE AND SCOPE**

Groundwater investigations conducted to date have produced inconclusive results. Potential sources have been identified, but data gaps exist on source concentration, release rates, migration routes, aquifer characteristics, effect of river stage and groundwater pumping on flow direction, and velocity of groundwater and contaminants. Warzyn Engineering Inc. (Warzyn) was retained by the U.S. EPA to conduct a comprehensive RI/FS of the well field. A summary of available data, data needs and a detailed Work Scope was described in the Work Plan and the Quality Assurance Project Plan prepared by Warzyn in September 1987. The major objectives of Phase I Remedial Investigation (RI) as outlined in the Work Plan included:

- Identification of contaminant sources of VHHs identified at each well field;
- Determination of the nature and extent of impacts;
- Obtaining and evaluating data to determine aquifer characteristics;
- Obtaining and interpreting data to determine the effect of groundwater pumping and river stage on groundwater flow direction and velocity;
- Determination of probable fate of contaminants through time;
- Assessment of the dangers to public health associated with the contamination; and
  - Identifying potential data gaps to be filled during Phase II field investigation.



-4-

This Technical Memorandum presents a summary of procedures and results of the RI activities performed in the Phase I (Subtasks 2.1.2 to 2.1.10 of the Work Plan) including:

#### 2.1.2 Preliminary Model Development

Development of a preliminary model to assess groundwater flow and contaminant transport in the vicinity of the City Well Field.

#### 2.1.3 Preparation for Site Investigation

The preparation for the site investigation consisted of construction of a decontamination pad and set up of on-site analytical equipment (GC).

#### 2.1.4 Existing Well Sampling

Selected existing site monitoring wells were sampled and analyzed to provide information on site conditions prior to the beginning of the field investigation.

#### 2.1.5. Soil Gas Survey

The soil gas survey was conducted to help identify potential source areas and to map the distribution of VHHs at the water table surface near potential source areas.

#### 2.1.6 Monitoring Well Installation

Groundwater monitoring wells were installed to collect groundwater quality samples, groundwater levels and in-situ hydraulic conductivity data. Groundwater and soil samples were obtained during drilling to identify site geology and obtain preliminary information on the distribution of VHHs in the aquifer.

2.1.7 Surface Water and Sediment Sampling Surface water and sediment samples were collected to assess potential impact on surface water bodies in the vicinity of the City Well Field.

2.1.8 Groundwater Sampling and Aquifer Testing Groundwater samples were collected from existing and newly installed monitoring wells. The analytical results formed the basis for the RI and FS



evaluations, including source identification, extent of contamination, and the identification of remedial action alternatives.

2.1.9 Groundwater Level Monitoring

Groundwater level and river stage monitoring was conducted to determine changes in groundwater flow direction due to variations in pumping rates, river stages and groundwater recharge.

2.1.10 Location and Elevation Survey

A survey was conducted to determine the location and elevation of project monitoring and production wells.

This document also includes an interim site assessment based on the evaluation of data available from the Phase I investigation and presents recommendations for additional work to be conducted during the Phase II investigation.



#### II. FIELD INVESTIGATION METHODS

Phase I field investigation activities including: groundwater sampling, soil gas survey, drilling, monitoring well installation, groundwater sampling during drilling, surface water and sediment sampling, groundwater level monitoring, hydraulic conductivity testing and monitoring well location and elevation survey were conducted in substantial conformance with procedures presented in the Quality Assurance Project Plan (QAPP) and the site Sampling Plan prepared by Warzyn dated September 1987. Specific procedures used in the analysis of groundwater and soil gas samples for VOCs are presented in Appendix G of the QAPP. Minor modifications of procedure were made in the field based on acquisition of additional data or in response to site specific needs. Modification of specific procedures or the investigation approach were made in consultation with the U.S. EPA Project Officer. The subsequent sections describe these procedural modifications and present a discussion of alternative methods.

The Phase I field investigation consisted of several tasks which were conducted from August 1987 to January, 1988. An Industrial Survey of area businesses was conducted on August 6 and 7, 1987. Results of the Industrial Survey have been submitted to the U.S. EPA for comment. The final Industrial Survey report will be released as a separate document. Generally, the tasks were completed sequentially. However, the soil gas survey and drilling and installation of monitoring wells were conducted concurrently, in order to optimize the use of the field GC. Similarly, groundwater levels were often recorded prior to groundwater sampling, to optimize the use of field personnel.

#### A. SITE PREPARATION (Task 2.1.3)

In preparation for the field investigation program, a laboratory gas chromatograph (GC) was mobilized to the City of Wausau for the purpose of analysis of soil gas, groundwater and surface water for volatile organic compounds (VOCs). A site trailer was located at the City of Wausau Water treatment plant and was used as a base of operations for the project. The trailer housed the GC in one room and site operations headquarters and



-7-

supplies in two separate rooms. A decontamination area for the drilling rig, associated tools and well construction materials was constructed adjacent to the trailer. The decontamination area consisted of a 40-foot by 50-foot polyurethane lined area that had been graded to drain into a trench sump containing two 55 gallon drums. Permission was obtained from the City of Wausau to pump decontamination water collected in the sump to a sanitary sewer manhole located near the pad.

A field GC equipped with a PID and Hall detector in series was shipped to the on-site trailer on Wednesday, October 7, 1987. The instrument was unpacked and assembled on October 7, 1987. The GC was allowed to equilibrate and preliminary injections were made on October 8, 1987 to determine system performance. Initial results indicated poor sensitivity and an unstable, noisy baseline. On October 9, 1987 additional adjustments were made and by late in the day the sensitivity began to increase while baseline noise decreased. The system was left to equilibrate over the weekend of October 10-11, 1987. On Monday, October 12 a calibration curve was analyzed. The curve was linear with sensitivity requirements met, indicating the system was stable and analysis could begin.

#### <u>B. EXISTING WELL SAMPLING (ROUND I)</u> (Task 2.1.4)

#### 1. Purpose

In order to acquire updated information on the extent of VHH contamination, samples were collected from existing groundwater supply and selected groundwater monitoring wells during the period September 29 - October 6, 1987. Samples were collected from a total of 57 wells including:

- 5 municipal Production wells (CW3, CW4, CW6, CW7 and CW9);
- 1 private well (Wergin Construction Company);
- 13 existing monitoring wells installed by STS Consultants Ltd. for Wausau Chemical Company;
- 2 existing monitoring wells installed by CH<sub>2</sub>M Hill at the abandoned city of Wausau landfill;
- 13 existing U.S. EPA monitoring wells installed by Roy F. Weston Inc.;



- 7 existing monitoring wells installed by RMT Inc. in the vicinity of Marathon Electric;
- 12 existing monitoring wells installed by Geraghty & Miller Inc. and Becher-Hoppe Engineers, Inc. for the City of Wausau; and
- 4 existing monitoring wells installed by Foth & Van Dyke and Associates, Inc. for Wausau Energy Inc.

Depths to water were measured prior to sampling with an electronic water level indicator, or a measuring tape attached to a sounding device. The water level indicator probe was rinsed with deionized water between water level measurements. The well integrity was evaluated through visual inspection and comparison of total well depths to as-built well information. Based on the well inspections, Monitoring Well WC-1 appears to have been damaged and requires repair before it can be sampled. Refer to Appendix H for observed water levels and a summary of well construction details.

#### 2. Sample Collection Procedures

Prior to mobilization to the site, sampling pumps, tape measures, bottom loading bailers and stainless steel cable were decontaminated using a trisodium phosphate (TSP) wash and clear water rinse. Between wells, sampling equipment was decontaminated with a laboratory wash solution (Liquinox) followed by a rinse with deionized water.

A Johnson-Keck submersible pump was used to sample the existing monitoring wells. A packer was attached to the pump to sample piezometers. The pump was lowered to a depth of approximately five feet above the top of the piezometer screen and the packer inflated to seal the sampling zone. The sampling interval was then purged of at least three volumes of water in the isolated interval. The water level above the packer was monitored to determine if the the packer was effective in sealing off the water above the packer. Water level measurements recorded during purging indicated no evidence of packer leakage. The sample was then collected directly from the pump discharge. Purged groundwater was screened with a 10.2 eV HNu photoionization meter for detection of VOCs. Purge water from monitoring wells with historically high (>1000 ug/L) total VOC concentrations was discharged to the City sanitary



sewer system. Purge water which indicated above background HNu readings was also discharged to the City sanitary sewer. Where practical, purge water from other monitoring wells was disposed in the City storm sewer system.

The Johnson-Keck pump was also used to sample most water table wells. The pump was lowered to a position about three to four feet above the bottom of the well to prevent potential damage to the pump by fine residual materials which might be present in the well. The well was then purged of at least three well volumes prior to sampling. Samples were collected directly from the pump discharge. Water table wells at the Wausau Chemical site (WC2, WC3B, WC4A, WC5A, WC6A and WC7A), could not be sampled with the Johnson-Keck pump due to screen obstructions. These wells were purged and sampled using a 1 inch diameter stainless steel bailer.

Temperature, specific electrical conductance, and pH were measured upon sample collection prior to sample filtration and preservation. Samples requiring filtration and preserving were prepared as outlined in Table 3 of the QAPP. Samples were shipped daily (on ice) to the laboratory designated by U.S. EPA's Contract Laboratory Program (CLP) for analysis of VOCs and general water chemistry parameters (see parameter list in Table 2 of the QAPP). VOC analyses were completed using the methods in Appendix D of the QAPP (low level GC/MS with 7 day turnaround) so that the rapid turnaround would allow use of data in the Phase I investigation.

## <u>C. SOIL GAS SAMPLING</u> (Task 2.1.5)

#### <u>1. Purpose</u>

Soil gas sampling with on-site analysis of samples was conducted (151 sampling points vs 93 sampling points planned in the Work Plan) to help identify potential VOC source areas, and to potentially assist in locating the VOC plume present at the water table in the vicinity of source areas.

The soil gas survey conducted at various facilities/areas was based on the size and type of operation at the site, the results of the Industrial Survey, results of existing monitoring well sampling in the area, and results of the initial soil gas sampling. The facilities/areas investigated in the soil gas survey included those outlined in the Work Plan including:



- Marathon Box Company;
- Marathon Press Company;
- Wergin Construction Company;
- The C.M. St P. & P. Railroad and right of way;
- Wausau Energy Corp.;
- Wausau Chemical Company;
- Marathon Electric Inc.; and
- The two concentric rings of points around Well CW6, including Schofield Park, and Bos Creek potential fill Areas.

In addition to these areas, the following areas were surveyed:

- Camelot cleaners;
- ETCO Electric Company;
- Gorwitz Furs; and
- The former City landfill on Marathon Electric Property.

#### 2. Sample Collection Procedures

The soil gas survey was performed on October 13-29, and November 10-11 in substantial conformance with the Sampling Plan.

The soil gas sampling vessels consisted of 250 mL cylinders fitted with teflon stopcocks at either end and a septa. The vessels were decontaminated prior to and between samples by purging with the ultra-pure helium gas used for the field GC carrier gas. Prior to use, each sampling tube was again purged with helium for a minimum of 30 seconds.

Sampling consisted of driving a rod to a depth of approximately 3 feet. The drive rod was removed from the ground and the sampling probe was inserted into the hole made by the drive rod to a depth of approximately 2.5 feet. A surface seal was obtained using an 8-inch diameter PVC cover plate attached to the sampling probe. One and one-half volumes of the sampling tube, probe and sample vial was purged using a calibrated air pump. The stopcocks on the sampling tube were closed and the air pump turned off. The sampling tube was



wrapped in aluminum foil (to minimize photo-chemical alteration of the gas sample) and was stored on ice until analyzed. The drive rod was decontaminated by cleaning with a paper towel. The sampling probe and tubing was decontaminated by purging with several volumes of ambient air after each sample collection.

Duplicate and blank samples were also collected and analyzed every 10 samples. Blank samples were obtained by collecting an ambient air sample through the probe and tubing after decontamination.

D. FIELD ANALYTICAL METHODS FOR VOCS (as used by Task 2.1.5 and 2.1.6) Field GC analytical methods for soil gas and water headspace samples were intended to provide detection and quantitation of the following compounds:

- Benzene
- Bromodichloromethane
- Bromoform
- Chloroform
- Chlorodibromomethane
- 1,1-Dichloroethane
- 1,2-Dichloroethane
- 1,1-Dichloroethene\*
  1,2-Dichloroethene\*
- Ethyl Benzene
- Methylene Chloride
- Tetrachloroethene'
- Toluene<sup>3</sup>
- 1,1,1-Trichloroethane
- Trichloroethene'

\*Target Compounds

Field analysis was performed according to the methods listed in Appendix F of the approved QAPP. A Varian 3400 model GC was used with photoionization and Hall Electrolytic Conductivity detectors (PID/HECD) in series. Each analytical run (one field day or less) included a standard sequence consisting of a 4-point standard curve for headspace target compounds (50, 10, 5, and 1 ug/L), a headspace blank of a 50 ug/L headspace non-target compound and 5 uL injections of both target and non-target compounds for soil gas. Every eleventh analysis thereafter and the last sample each day were continuing calibration standards. Continuing calibration standards were generally within



±10% of the original standard. However, the continuing calibration standards exceeded ±30% (limit approved in the QAPP) of the original standard on six occasions. In these instances, the groundwater analysis results were footnoted as being estimated values. Due to time constraints and field logistics (need to determine well screen locations) recalibration and reanalysis of samples was not performed. Duplicate analytical samples were analyzed on a 1 in 10 or fewer basis.

Water samples were collected in 40 mL vials with open screw-caps and teflon faced silicone septa. Water samples were collected so that no headspace remained in the vial. Soil gas samples were collected in 250 mL glass vessels. The samples were protected from sunlight, stored in coolers, and transported to the field laboratory as soon as practical.

When received by the field laboratory, soil gas bulbs were allowed to equilibrate to ambient air temperature. A 5 mL aliquot of sample was removed through the sampling septa and injected into the GC.

Just before analysis, water samples were uncapped and 10 mL of sample was removed from the vial. The vial was then recapped and placed in a 55°C water bath for 10 minutes for headspace equilibration. A 5 mL aliquot of headspace air was removed from the vial through the septa and injected into the GC. Headspace dilutions were made by bringing an aliquot of the sample to 40 mL with organic free-water in a new 40 mL vial and repeating the above procedure.

Concentrations of target headspace VOCs in water were calculated based on a linear regression obtained from the initial calibration curve. Non-target compound headspace results were calculated on the basis of a 1-point standard using the following equation:

ug/L = 
$$\frac{R(samp)}{R(Std)}$$
 x C(Std) x DF (Equation 1)  
where: R(samp) = Response of parameter in sample (counts)  
R(Std) = Response of parameter in standard (counts)  
C(Std) = Concentrations of standard in ug/L  
DF = Dilution Factor



Calculations of soil gas concentrations were performed according to the

R(samp) x ng(Std) ng(injected) = -(Equation 2) where: ng(injected) = Nanograms of compound injected R(samp) = Response of compound in sample (area counts) ng(Std) = Nanograms of standard injected R(std) = Response of compound in standard (area counts) ng(injected) x 1000 mL/L nq/L =(Equation 3) Va where: ng/L = Nanograms of compound per liter of soil gas ng(injected) = Nanograms of compound injected from equation 1 Va = Volume of soil gas injected (mL)

Results for equation 2 where calculated at the end of the day on a summary page in the field laboratory notebook.

Sample results, standard conditions and notes were recorded in a bound log book. Field results of GC analyses were considered tentatively identified with estimated concentrations. Retention time order and detection limits for headspace and soil gas target and nontarget compounds are shown in Tables 1 through 4.

<u>E. ON-SITE ANALYSIS OF SURFACE WATER SAMPLES</u> (Supplemental to Work Plan) Surface water samples were collected at 11 locations from October 14 to October 29, 1987. The on-site analysis of surface water samples was not identified as a specific task in the Remedial Investigation Work Plan, but was conducted to evaluate conditions not previously anticipated. Sample locations are presented on Drawing 13076-B11 and are summarized in Table 5.

#### 1. Purpose

The discharge at Well CW6 was reportedly to a storm sewer which discharged to the Wisconsin River. During the field investigation it was found that the storm sewer discharged to Bos Creek. Water levels measured at well nests R2



approved QAPP using two steps and the following equations:

and R3 indicated downward gradients in the vicinity of the creek. Therefore, Bos Creek was identified as a potential source of VOC contamination to the shallow aquifer. Surface water samples were collected from Bos Creek to determine if discharge from production well CW6 was affecting groundwater quality through induced recharge of surface water into the aquifer. The collection and analysis of surface water supplemented groundwater data collected from adjacent wells.

#### 2. Sample Collection Procedures

Surface water samples were collected by slowly submerging a 40 mL VOA vial into the surface water body while standing on shore. The vial was then capped so that no headspace remained. Samples were transported to the on-site GC within 1 hour. Duplicate samples of stations SW09 and SW10 were collected and submitted to the CLP for verification of field GC results.

# F. DRILLING AND MONITORING WELL INSTALLATION (Task 2.1.6)

The subsurface exploration and groundwater monitoring well installation program was conducted between October 12 and December 12, 1987. Drilling, soil sampling, monitoring well installation and groundwater sampling while drilling was performed by Wisconsin Test Drilling, Inc. (WTD) of Schofield, Wisconsin, under the supervision of Warzyn.

Warzyn field personnel recorded activities in log books, prepared boring logs, collected soil and groundwater samples during drilling, and acted as safety officers at their respective drilling rigs.

Twelve (12) monitoring wells were installed at eight (8) locations in the west well field area and eighteen (18) wells were installed at thirteen (13) locations in the east well field area. An additional six (6) shallow soil borings were conducted in the east well field area in order to obtain shallow soil and groundwater samples for field and laboratory VOC analysis. Monitoring well and boring well locations are presented in Drawing 13076-B11. Boring logs and well details are presented in Appendices B and C, respectively.



13076.28

## 1. Purpose

Monitoring wells were installed to provide data on aquifer characteristics, groundwater quality and groundwater flow directions. The nested wells provide information on vertical groundwater gradients and water quality at depth in the aquifer. Well nests generally included a shallow water table well, installed in the upper aquifer, and a deep piezometer installed near the base of the aquifer. Well locations and depths were modified from planned locations outlined in the Work Plan based on results of Round 1 water quality analyses, field VOC analyses of soil gas and water samples collected during drilling, and results of the preliminary groundwater model. The well locations selected were agreed upon with the U.S. EPA Project Officer. Refer to Table 6 for summary of well location and depth rationale.

## 2. Drilling Equipment

WTD provided drilling rigs, (CME 45C, CME 750, CME 55, D 50 and Canterra CT 311), associated tools, rig operators and support personnel, steam cleaning equipment, soil sampling equipment, groundwater sampling drivepoint and riser, and well construction materials. WTD also provided two Brainard Kilman (BK) 1.7 inch hand pumps for groundwater sampling during drilling. Warzyn provided a Johnson-Keck submersible pump with packer for sampling groundwater in deep borings while drilling.

#### 3. Drilling Methods

Drilling required the use of two methods. A 4-1/4 inch I.D. hollow stem auger was used to drill and install shallow water table monitoring wells. A 4-1/4 inch I.D. hollow stem auger with screened lead auger was also used to obtain soil and groundwater samples from shallow borings at locations E32, E33, E34, E35, E36, E37 and E38 (See Drawing 13076-B11).

Deep piezometers were installed using mud rotary methods. A bentonite drilling mud with no dispersing agents (Aquagel Gold Seal) was used to provide the viscosity needed to remove drill cuttings. Four inch I.D. casing was advanced in five foot increments to completion depths in borings E21, E22, E24, E25, E26, W50 and W55 using either a 4-7/8 or a 5-7/8 O.D. roller bit. Water quality analyses conducted during drilling suggested a need for a



greater number of deep wells. Due to a shortage in the quantity of available temporary casing, several monitoring wells were drilled without driving casing to the boring completion depth. Borings E20, E27, E30, E31, W52, W53, W54, W56 and W57 were advanced using mud rotary drilling with casing advanced to the water table. Bentonite slurry was used to support the borehole and remove drill cuttings below the water table in these borings. In general, very little drilling fluid was lost to the formation during boring advancement. Well development provided substantial well yields with little or no turbidity. VOC analyses performed on samples obtained during well development indicated VOC concentrations consistent with results obtained from samples collected during drilling (refer to Appendix G).

Water used for drilling well E25 was obtained from the City water distribution system at the filtration plant. This water was analyzed by the field GC and was found to have elevated trihalomethane concentrations (chloroform 50.8 ug/L, see Appendix G results). Subsequently, water for steam cleaning and drilling was obtained from test well CW10. Field GC analysis of water collected from Well CW10 indicated no detectable VOCs (see Appendix G sample CW10). Well CW10 was welded shut prior to drilling well E27, therefore, well E27 was drilled using water from the City distribution system.

## 4. Soil Sampling

Split spoon soil samples were collected at drilling locations E20 through E31 and W50 through W57, using ASTM method D-1586 (Standard Penetration Test). Samples were generally collected at five foot intervals from the ground surface to a depth of 25 feet. Soil samples were collected at either 10 foot or 15 foot intervals from 25 feet to completion, depending on the proximity of previously sampled borings. Sampling was divided between the shallow and deep boring at each well nest location, as needed, to obtain a complete set of samples for that location. Boring E27 was drilled from ground surface to a depth of 89 feet without soil sampling and was sampled on a 15 foot interval from 89 feet to completion. With the exception of two contract laboratory soil samples collected from 29 to 32 feet, boring E21 was drilled unsampled from ground surface to 89 feet and was sampled on a 15 foot interval from 89 feet to completion depth. Soil samples were collected from auger cuttings at shallow borings E32 through E38. The auger cuttings provided a vertical



composite of unsaturated zone soils. These samples were submitted for contract laboratory target compound analysis. Split spoon soil samples were also collected at discrete depth intervals at 12 locations. Refer to Table 7 for soil sample locations, analysis parameters and rationale. The samples were shipped and preserved according to Table 3 of the QAPP. Samples collected for VOC analyses were transferred immediately to the respective bottles without compositing. Grain size samples were also not composited in order to preserve soil texture. Soil samples collected for total organic carbon (TOC) analyses and Acid Base Neutral analyses were composited prior to placement in the sample bottle.

Soil samples recovered from the borings were visually classified in accordance with the United Soil Classification System (USCS). Classifications are preliminary pending results of the physical soil testing and are presented on boring logs in Appendix B. When weather conditions permitted, soil samples were screened for the presence of volatile organic compounds (VOCs) using an HNu photoionization detector (see Boring Logs in Appendix B for results). The HNu photoionization detector is capable of detecting compounds with an ionization potential below 10.2 eV. The instrument was calibrated daily using an HNu calibration gas. HNus were also used to screen drill cuttings for VOCs. Drill cuttings which yielded HNu readings over 1 ppm were contained in 55 gallon drums. The drums were labeled and cross-referenced to field notebooks. The drums are being retained adjacent to the site trailer.

#### 5. Groundwater Sampling

Groundwater samples were generally collected for VOC analysis at 10 or 15 foot intervals below the water table at each monitoring well location. However, a few zones of fine grained soils with relatively low hydraulic conductivity were encountered, from which groundwater samples could not be obtained within a reasonable time period. Because a deep (> 100 feet) plume of VHH was suspected (due to the vertical distribution of contaminants in Monitoring Wells E30 and E31), groundwater samples were not obtained from borings E21 or E27 from depths shallower than 90 feet. However, a water table well (E21A) was installed adjacent to Monitoring Well E21 and was subsequently sampled during the Round 2 sampling event.



Groundwater samples were collected using a three-foot long section of two inch I.D. stainless steel well point attached to a galvanized steel riser pipe. The well point was driven into the base of the borehole so that the slots were exposed to the aquifer. Three casing volumes (or isolated interval) of groundwater were then purged using either a Brainard Kilman 1.7 inch O.D. hand pump or a Johnson-Keck submersible pump with packer. Water samples were collected, for on-site GC analysis, in VOA vials directly from the pump discharge. Several duplicates of these samples were also collected and sent to a CLP lab for verification purposes.

Shallow groundwater samples were obtained from borings E32, E33, E34, E35, E36 and E38 using a screened hollow stem auger which had been drilled several feet into the water table. The sample was collected using either a Brainard Kilman 1.7 inch O.D. hand pump or a stainless steel bailer. Prior to sample collection 3 to 5 casing volumes of water were removed from the auger.

#### 6. Geophysical Logging

Several deep borings were gamma logged using a Mount Sopris 1000 C stratigraphic logger. Results of gamma logging were used to provide information on clay content of penetrated formations and to determine depth to bedrock. Results of the gamma logging were used in combination with the field water quality analyses of samples collected while drilling to optimize well screen location in the aquifer. Logging followed methods outlined in the manual in Appendix E of the QAPP.

## 7. Well Installation

Water table monitoring wells and piezometers were installed according to construction details contained in Appendix C and summarized in Appendix H. Wells were constructed using 2 inch I.D. flush joint, galvanized steel riser pipe, with No. 10 slot, flush joint, stainless steel screens. Wells screened at the water table were constructed with 10 foot screens. Wells screened at depth in the aquifer, were constructed with 5 foot screens with a 10 foot stainless steel riser pipe directly above the well screen. The annular space between the well and the borehole (sand pack) was backfilled with either No. 30 flint sand, caved formation, or a combination of both. The sand pack



generally extended to a height of 3 to 5 feet above the well screen. In cases where the boring extended past the intended location of the screen interval by more than 3 feet, flint sand interbedded with bentonite pellets were used to backfill the borehole so the well screen could be placed at the desired depth in the aquifer. A 2 to 3 foot seal of bentonite pellets was installed above the sand pack of each well. In deep wells, a thick bentonite slurry was used to seal the annular space from the top of the pellet seal to the ground surface. A tremie pipe with lateral exit holes was set above the top of the pellet seal and pumped at a slow rate until the slurry began to run out the top of the auger or casing. Additional bentonite slurry was added as needed to compensate for removed casing. The shallow well annular space was also backfilled with a thick bentonite slurry which was installed from the surface using a pump hose. A surface seal of granular bentonite was installed in the upper 3 to 5 feet of borehole. A locked protective casing was then set into the surface seal. Locked flush mount protective casings were generally installed in driveways, parking lots, City right-of-ways and other highly traveled areas. Cement grout and bumper posts were placed around stick up protective casings adjacent to highly traveled areas. The well installation was completed by marking the protective casing with the well identification numbers.

All wells, with the exception of E28A, appear to function properly. E28A appears to have a slight kink in the screen and therefore must be sampled with a one-inch diameter bailer.

#### 8. Well Development

Shallow wells were developed using either a bailer or a Brainard Kilman 1.7 inch O.D. hand pump. Deep wells were developed using either a Brainard Kilman 1.7 inch O.D. hand pump or a Johnson-Keck submersible pump with packer. Deep wells were surged with a two inch bailer prior to pumping. The pump was also periodically raised and lowered during development, so that the entire screened interval was developed. The well was pumped until a minimum of 10 well volumes had been extracted and the water became visually clear. pH and conductivity were measured at frequent time intervals during development of several wells. In general, changes in theses parameters indicated minimal change after the first two to three well volumes had been removed.



#### 9. Decontamination

Decontamination of well screen, well riser, drive points, drill rig, casing, drill rod, drill bits and other tools consisted of steam cleaning at the decontamination pad. Each drill rig and tools was decontamination prior to start up and between holes. Brainard Kilman hand pumps were also steam cleaned between holes. The Johnson-Keck submersible pump was decontaminated by running Liquinox wash solution through and over the pump for several minutes. Deionized water was circulated through the pump and ran over the tubing for rinse. Water used for steam cleaning was obtained from city test well CW10.

#### <u>G. GROUNDWATER SAMPLING (ROUND II)</u> (Task 2.1.8)

#### <u>1. Purpose</u>

Round II groundwater samples were collected from 116 monitoring wells between November 30 and December 12 throughout both the east and west well field areas. Sample locations included the following:

- Five City Production wells (CW3, CW4, CW6, CW7, CW9);
- Two City test wells (Plum Dr. test well, Wilson Hurd test well);
- One private well (Wergin);
- Five Wausau Chemical Extraction Wells (EXW4, EXW5, EXW6, EXW7, EXW15);
- Wausau Chemical treatment system influent and effluent; and
- One hundred and one groundwater monitor wells.

The analytical results obtained from Round II sampling will provide additional data for the RI evaluation, including source identification, extent of contamination and determination of the mass of contaminants present in the aquifer. Results of Round II sampling were not available at the time this document was prepared but will be presented in the Remedial Investigation Report.

## 2. Sample Collection Procedures

Round II groundwater samples were collected according to procedures described for Round I sampling. Round II groundwater samples were analyzed for VOCs and



-22-

general water chemistry parameters by a designated U.S. EPA Contract Laboratory Program (CLP) according to the special analytical services (SAS) methods specified in Appendix D of the approved QAPP. An additional 20 samples were analyzed for Hazardous Substance List (HSL) parameters by the CLP using Routine Analytical Services (RAS) methods outlined in Appendix B of the QAPP.

## H. SURFACE WATER AND SEDIMENT SAMPLING (Task 2.1.7)

Surface water and sediment samples were collected at 7 locations on December 9, 1987. Sample locations are described in Table 8 and are shown on Drawing 13076-B11.

## 1. Purpose

Surface water and sediment samples were collected to assess potential affects of surface water discharges on the groundwater through induced recharge.

## 2. Sample Collection Procedures

Surface water samples were collected within a stainless steel cup prior to sediment sample collection. The cup was submerged slowly in the water body to minimize turbulence and potential for volatilization of VOCs. The sample was immediately transferred to a 40 ml VOA vial with minimal turbulence. Following surface water sample collection, sediment samples were collected using a stainless steel core barrel. The samples were composited in a stainless steel mixing bowl and were transferred to 8 oz VOA vials using a stainless steel spatula. The sediment samples were sealed in the VOC vials within 3 to 4 minutes of sample extraction. Ambient temperatures during sampling were below freezing, therefore minimizing potential for loss of volatiles. Sampling equipment was decontaminated with a TSP wash followed by a deionized water rinse after collection of each sample.

In order to maintain consistent analysis of field indicator parameters, pH, specific electrical conductivity and temperature of the surface water samples were measured at the site trailer within 1 hour of sample collection. By analyzing the samples at the site trailer, utilization of field personnel was maximized and consistency maintained, since the samples were analyzed by one



operator using the same equipment for all analyses. Surface water samples undergoing metals analyses were filtered and preserved prior to shipment according to Table 3 of the QAPP. Surface water samples were shipped daily to designated CLP Laboratories for VOC and general water quality parameter analyses according to SAS procedures (see Appendix D of the QAPP for analytical methods). Sediment samples were also shipped daily to a designated CLP Laboratory for VOC analysis according to RAS procedures (see Appendix B in the QAPP for CLP target compound lists and required detection limits).

-23-

# I. HYDRAULIC CONDUCTIVITY TESTING (Task 2.1.9)

## <u>1. Purpose</u>

The purpose for conducting baildown tests in selected monitoring wells is to measure the in-situ saturated hydraulic conductivity of subsurface materials. Baildown tests methods were selected over laboratory tests because the field method tests a larger, less disturbed zone of the aquifer than laboratory testing methods.

The general procedure for a baildown test is to instantaneously change the hydraulic head within the well and measure the rate at which the water level in the well recovers to the static level. The hydraulic conductivity of the aquifer material is a function of the rate of water level recovery and the well geometry. Due to the effects of partial well penetration on the analytical solution, the location of the well screen with respect to the water table and the base of the aquifer must be considered. The configuration of a typical baildown test is illustrated in Figure A (Appendix I).

#### 2. Test Methods

Piezometers were tested using air pressure to create a head within the well. The water level within the well fell until the total head within the well (water column plus air pressure) equaled the total head outside the well. The air pressure was instantaneously released, creating a low head within the well and subsequent water level recovery. A pressure transducer with an In-Situ Environmental Logger Model SE 1000B (Hermit Data Logger) was used to measure and record the water level recovery in the well.



A PVC air pressure manifold was fitted over the top of the well casing and a non-reactive fluorosilicate gel was used to create an air seal. An electric water level indicator and the pressure transducer were lowered into the well through a rubber gasket in the top of the device. The air space above the water column in the well was pressurized using breathing air (SCBA tank) or nitrogen until the water level dropped to the desired depth (indicated by the electric water level probe). Generally, the system was pressurized to 5 to 10 psi causing approximately 10 to 15 feet of drawdown. When the desired water level was attained, a 2-inch ball valve was opened to instantaneously release the air pressure. The data logger was started simultaneously with the release of pressure to measure the rate of water level recovery.

Hydraulic conductivity tests were conducted on water table wells by instantaneously removing a known volume of water from the well with a stainless steel bailer. Water level recovery was measured using a pressure transducer with data logger.

The hydraulic conductivity test data was reduced using the Bouwer and Rice Method, summarized in Appendix I.

# J. LOCATION AND ELEVATION SURVEY (Task 2.1.10)

Monitoring wells installed by Warzyn and selected previously installed monitoring wells were surveyed by Warzyn from December 21 through December 29, 1987. A discrepancy of approximately 0.25 feet was discovered between the previous surveyed east well field monitoring well elevations and elevations determined during the present study. Therefore, the east well field monitoring wells, extraction wells and production wells were resurveyed on January 4 and 5, 1988. The west well field monitoring well elevations were generally within ±0.05 feet of the previous survey results.

Monitoring well and production well elevations were surveyed using U.S.G.S. Monument TT135FJH (Elevation 1202.571 feet MSL) located at Gilbert Park, as reference. Monitoring wells were surveyed for top of protective casing elevation, top of riser elevation and ground surface elevation. The vertical accuracy of the survey was approximately 0.01 feet. However, ground surface



elevations were surveyed to  $\pm 0.1$  feet due to surface irregularities. Monitoring well locations were determined by measuring distances and angles from existing features and structures. Monitoring well locations are shown on Drawing 13076-B11. Monitoring well elevations and construction details are summarized in Appendix H.

### K. WATER LEVEL MONITORING (Task 2.1.9)

#### 1. Purpose

Groundwater levels were measured at 3 different time periods during the course of the Phase I field investigation. Groundwater elevations were used to determine flow directions, and vertical and horizontal gradients. Variations in groundwater elevations between monitoring periods were used to assess aquifer response to river fluctuations and pumping variations.

### 2. Procedure

Water levels were measured and recorded during three time periods: October 5, 1987; December 10, 1987; and January 7-8, 1988. Water levels were measured using either a fiberglass tape with attached sounding device or an electronic water level indicator. On occasions when two different measuring devices were used to obtain groundwater levels, the instruments were first calibrated to a base station (well) and the response of one of the instruments was adjusted to be consistent with the other instrument.



#### -26-

## III. RESULTS OF THE PHASE I FIELD INVESTIGATION

## A. GEOLOGY

## 1. Bedrock Geology

The City of Wausau is located near the southern margin of the exposed Precambrian shield in Wisconsin. Wausau and the surrounding area is predominantly underlain by Early Proterozoic basaltic to rhyolitic metavolcanics which have been intruded by Early to Middle Proterozoic granitic plutons (La Berge and Meyers, 1983). Investigations in the vicinity of the Wausau Well field indicate a distinct break in bedrock lithology exists beneath the Wisconsin River. Based on available boring logs and on samples observed during this investigation, the East Well Field appears to be underlain by rhyolitic bedrock whereas, syenitic bedrock underlies the west well field area. The difference in bedrock lithology is supported by the observation that the bedrock surface in the vicinity of the West Well Field is much more irregular than the bedrock surface present below the east well field (refer to Drawing 13076-B12). The preglacial bedrock topography east of the Wisconsin River is chracteristic of a mature erosional landscape. It possesses a subtle, somewhat uniformly eroded bedrock surface with tributary valleys that tend to be broad and shallower than tributary valleys located west of the Wisconsin River. Bedrock ridges are generally wider and not as highly dissected as ridges on the west side of the Wisconsin River. The bedrock surface west of the Wisconsin River indicates considerably greater relief of bedrock topography suggesting a more youthful erosional landscape. This landscape appears to be a function of a more weathering resistent bedrock lithology than that present of the east side of the Wisconsin River.

Bedrock topography in the vicinity of the Wausau Well Field is obscured by glacial outwash and alluvial sediments ranging in thickness from 0 to 170 feet. Glacial outwash sediments were deposited in the Wisconsin River Valley as Late Wisconsinan Stage glaciers retreated from the Wausau area. The outwash deposits fill the Wisconsin River Valley to an elevation of approximately 1230 feet MSL. The bedrock topography underlying the outwash deposits is predominantly a function of preglacial drainage patterns. The preglacial drainage patterns are evident from the topography of the exposed



bedrock above the glacial outwash terrace. The bedrock topographic map in the vicinity of the well field (Drawing 13076-B12) was developed using available boring logs and extrapolations of preglacial drainage based on exposed bedrock topography.

The bedrock surface contour map indicates the irregular nature of lateral and vertical aquifer boundaries in the vicinity of the City Well Fields. As previously stated, the bedrock surface west of the Wisconsin River tends to exhibit greater relief then the bedrock surface east of the Wisconsin River. The west bedrock surface is characterized by deeply incised tributary valleys, narrow ridges, and isolated bedrock highs. The West Well Field is located near the junction of a tributary valley and the main Wisconsin River Valley. This tributary valley extends from near the intersection of Campus Drive and Schofield Avenue and trends southeast. Boring W55 was performed during this investigation to determine whether a bedrock ridge, identified by a previous geophysical survey, was present. This well did not indicate the presence of the narrow northwest-southeast trending bedrock ridge between Production Well CW6 and Bos Creek. Therefore, it is unlikely that a bedrock ridge the size described by previous investigations (Weston, 1985; RMT, and Geraghty & Miller, 1987) exists.

A tributary valley also appears to be located in the southern portion of the East Well Field. This tributary valley extends from near the Intersection of Bridge St. and 13th Avenue and trends toward the west.

#### 2. Glacial Geology

Glacial outwash deposits in the Wisconsin River Valley are generally very heterogeneous due to lateral channel migration and vertical bedload aggradation. While it is difficult to correlate specific depositional units in such a braided stream environment, it is possible to recognize general depositional trends. The distribution of glacial outwash sediments appears to be strongly controlled by the underlying bedrock topography. North of the City of Wausau Well Fields, the Wisconsin River Valley narrows to less than 1/2 mile wide. Glacial outwash sediments deposited in this portion of the Wisconsin river Valley are predominantly coarse sands and gravels that are



often greater than 150 feet thick. As the Wisconsin River Valley widens toward the south the outwash deposits grade from coarse sand and gravels to fine to medium sands. The thickness of the glacial outwash deposits also decrease toward the south (Kendy, 1983).

Geologic cross-sections constructed through the well field area (Drawings 13076-B13 and 13076-B14) indicate the heterogeneous nature of the glacial outwash sediments. The correlation shown in cross-section should be considered preliminary until soil classifications can be reviewed using the grain-size analyses from the CLP lab. Cross-section AA' extends from boring E28A in the East Well Field across the Wisconsin River to Marathon Electric monitoring well nest R1S, R1D. Cross-section BB' is located on the west side of the Wisconsin River and extends from well nest C4S, C4D, south of the Marathon Electric foundry, to well nest GM4S, GM4D located north of the City's West Well Field. Refer to Drawing 13076-B11 for monitoring well and cross-section locations.

Cross-section AA' indicates a glacial outwash terrace that onlaps against the crystalline bedrock valley. The maximum elevation of this outwash terrace is approximately 1230 feet MSL. The outwash terrace is shown as predominantly composed of undifferentiated sand deposits. However, borings W52, W53, R1D and R4D indicate an apparently continuous sequence of deposits. This sequence consists of a fine sand unit overlying a thin gravel bed which is underlain by a fine to medium sand unit. The lower sand unit appears to pinch out against the bedrock surface beneath the Wisconsin River. The gravel layer is shown correlating to a basal gravel layer beneath the East Well Field. This soil correlation may be somewhat uncertain due to the relatively large distance between borings E27 and W53. The overlying fine sand unit grades toward the east into the undifferentiated fine to coarse sands. The bedrock surface beneath the East Well Field has weathered to a poorly sorted clayey residuum. This material is characterized by high silt and clay content and frequently contains angular feldspar fragments. The weathered bedrock can usually be distinguished from the overlying gravel deposits because it generally turns drilling fluids a burnt reddish color. A gray silty gravel material was encountered at the base of boring W53. This material may also be a weathering



product of the bedrock surface or a relict till not removed during the glacial outwash scouring of the bedrock surface.

Cross-section AA' shows fill materials on both sides of the Wisconsin River Valley. The fill materials encountered in the east study area consist largely of granite cuttings from local quarry and stone cutting operations. Much of the fill placed in low lying areas surrounding the East Well Field reportedly dates back to the early to mid 1900's (see Industrial Survey, Appendix L). The fill materials were used to build up the river terrace prior to and during river front industrialization. Additional fill materials were observed west of Lake Wausau Granite and at Schofield Park on the west side of the Wisconsin River. Approximately five to ten feet of granite cuttings are filled into a former sand and gravel pit located beneath the Wergin Construction Company property. The former City of Wausau landfill occupies a sand and gravel pit located beneath the southern portion of Marathon Electric on the west bank of the Wisconsin River. The landfill ranges in thickness from approximately 35 feet near the river bank to a couple of feet thick at the former gravel pit's west excavation face. Refer to Drawing 13076-B10 for approximate landfill boundaries. The gravel pit was filled with unknown quantities of residential, commercial and industrial wastes. The Industrial Survey (Appendix L) provides more specific information on landfill filling practices.

Cross-section BB' roughly parallels the west bank of the Wisconsin River (refer to Drawing 13076-B11). With the exception of Bos Creek and the gravel pit located north of monitoring well GM4D, the surface topography is relatively flat. The outwash sand deposits shown are somewhat heterogeneous and frequently appear discontinuous at the scale of this cross-section. Where the sand deposits could not be differentiated the unit is referred to as "fine to coarse sand". The depositional sequence described in the western part of section AA' is less apparent. The gravel unit appears relatively continuous throughout the southern portion of the cross-section area and may extend along the bedrock surface to well GM4D, located north of the City Well Field. The gravel unit was not logged in boring R3D, however, the driller reported difficult drilling at the approximate elevation of the unit (RMT, 1986). The underlying "fine to coarse sand" unit apparently pinches out to the north, in



-29-
the vicinity of well W52. The fine sand unit overlying the gravel appears to grade into undifferentiated sands toward the north.

The northern portion of the cross-section BB' indicates an increased abundance of coarse sand and gravel deposits. The coarser sediments are probably the result of the braided stream possessing higher depositional energy due to the narrow bedrock valley in the northern portion of the study area. Based on the extent of sand and gravel operations north of wells GM4S, GM4D the sand and gravel deposits appear relatively extensive throughout this area.

#### B. HYDROGEOLOGY

Groundwater flow in the vicinity of the City Well Fields is influenced by several factors including:

- bedrock topography;
- soil heterogeneities;
- variable production well pumpage;
- the presence and fluctuation of river and stream elevations;
- the hydraulic resistance of the stream and the river beds; and
- the rate and distribution of rainfall percolation recharging the aquifer.

Each of these factors play a role in the groundwater flow, contaminant flow and contaminant migration routes and velocities. Discussion of the dynamic relationships of these factors are beyond the scope of this document, except in so far as they are incorporated into the preliminary groundwater flow model. The following discussion on groundwater flow implicitly includes these factors into the observations on groundwater flow.

### 1. Groundwater Flow

Horizontal groundwater flow in the vicinity of the City Well Fields is shown in Drawing 13076-B15. The map was developed from groundwater elevations determined from water levels measured on January 7-8, 1988. Where possible, only water table wells have been used to construct the potentiometric



contours. However, the lack of data in some areas has made it necessary to use wells screened below the water table surface. The inaccuracy associated with using these water levels should be minimal considering the relatively low vertical gradients compared to the potentiometric surface contour interval (0.5 feet to 1.0 feet). Although water table elevations were used at most locations to construct this map, it is strictly a potentiometric map, because the aquifer beneath the Wisconsin River and portions of Bos Creek are semi-confined by the potentially lower hydraulic conductivity river bed deposits. The map indicates pronounced cones of depression around the five active City production wells. However, Production Well CW9 appears to have been turned off prior to water level monitoring. Therefore, the water levels in CW9 and CW9 OBS (CW9 observation well) may be recovering. Each of the other wells appear to be pumping.

The combined cone of depression of the West Well Field extends asymmetrically away from the pumping wells. Presently, the southern extent of the cone of depression at the water table appears to be limited by Bos Creek, which acts as a recharge boundary. This is shown by the higher head within the Bos Creek pond north of Randolph Street (1191 feet) than in the surrounding water table (1186 to 1187 at well nests R-2 and R-3). The effectiveness of this recharge boundary is evident in potentiometric cross-section BB' (Drawing 13076-B17) and from the vertical gradients presented in Table 9. The potentiometric section shows the divide extends through the fine to coarse sand into the underlying fine sand. The section indicates there may be continuity of flow from south of Bos Creek to production well CW6 within the basal gravel deposit.

The recharge boundary effect of Bos Creek may be more pronounced since early 1986, when well CW6 began regularly discharging to the creek, substantially increasing the flow. Prior to 1986, the groundwater divide may have been located further south than its present location. Refer to Section IV -Groundwater Flow Model Results for additional discussion of this phenomenon.

The cone of depression around the West Well Field shown on the potentiometric map is relatively steep southwest of the well field, because the aquifer thins



-31-

13076.28

and eventually pinches out against the bedrock high located west of Bos Creek Drive. The northern extent of the cone of depression is also limited by the aquifer thinning against a bedrock high located approximately 1200 feet north of Production Well CW9. Based on on the observation that water levels in monitoring wells between the west production Well Field and the Wisconsin River are lower than the river, it appears that significant infiltration is induced from the Wisconsin River. However, the amount and rate of river recharge has not been estimated.

-32-

Groundwater elevations in the vicinity of the East Well Field indicate considerable pumpage at Production Well CW3 and somewhat lower pumpage at Production Well CW4. The zone of influence of the east well(s) encompasses a large part of the riverfront industrialized area in northern Wausau. The cones of depression from wells CW3 and CW4 are separated by a groundwater divide on this particular date. The presence and location of the groundwater divide is dependent on pumping rates and schedules of Production Wells CW3 and CW4. Based on water levels measured on January 7, the groundwater divide appears to extend from the central portion of the Wausau Chemical property to the northern portion of the Marathon Box property. Small cones of depression were observed or interpreted to be present around the groundwater extraction system at Wausau Chemical (reported to be pumping at approximately 100 gpm) and the well at Wergin (reported at approximately 60 gpm).

The combined cone(s) of depression from the East Well Field also appears to affect groundwater flow below and to the west of the Wisconsin River. This is shown by the continuity in the gradient from the east to the west side monitoring wells (e.g.,monitoring wells E21 and E27 to W53 and C3S). The affect of the East Well Field production well pumpage is also shown on the potentiometric contours shown on section AA' (Drawing 13076-B16). The potentiometric contours on section AA' indicate a relatively strong component of vertical flow (recharge) adjacent to the bedrock valley walls, especially on the west end of section AA'. This recharge may be the result of inflow of groundwater from bedrock fractures but more likely from infiltration of surface water runoff from the bedrock uplands. The potentiometric contours become increasingly vertical toward the east, indicating a higher component of



horizontal groundwater flow. Monitoring Well Nests C4D, C4S and W53, W53A, located at Marathon Electric property, indicate very slight downward vertical gradients adjacent to the Wisconsin River. Below the Wisconsin River, the East Well Field production well pumpage has induced surface water recharge of the aquifer causing flow downward through the river bed and toward Production Well CW3. Deep groundwater flow remains predominantly eastward (horizontal) as indicated by the almost vertical equipotential lines. Potentiometric contours of the aquifer below the East Well Field indicate groundwater flow converging at Production Well CW3. Groundwater flowing at the base of the aquifer flows upward into the pumping well. Shallow groundwater flows downward to reach the screened section of the production well.

During the groundwater level monitoring period (January 7-8, 1988), the Wisconsin River was maintained at an elevation of approximately 1187.3 feet However, watertable monitoring wells adjacent to the River had much MSL. lower groundwater elevations than the River, indicating substantial head loss or resistance to flow through the river sediments. Monitoring Well E21A located approximately 25 feet east of the Wisconsin River had a groundwater elevation of approximately 1185.01, approximately 2.3 feet lower than the Wisconsin River. Water table Monitoring Wells C2S, C3S, C4S and C7S, located west of the Wisconsin River also had groundwater elevations considerably lower (0.90 to 0.70 feet) than the Wisconsin River indicating drawdown from the City Well Field had extended to the west side of the river. Refer to Appendix H for a summary of observed groundwater elevations. Potentiometric section AA' (Drawing 13076-B16) indicates the 1187.0 and 1186.5 potential contours are interpreted to be roughly parallel the river bed due to the head loss in the river sediments (actual head loss may be in a narrower zone than shown on section AA'). Below the river, the 1186.0 potential contour is extended nearly vertically, indicating predominantly horizontal groundwater flow at depth. Based on an aquifer thickness of approximately 140 feet and a river depth of approximately 20 feet, the Wisconsin River penetrates approximately 15% of the aquifer. The observed head loss in the river sediments combined with the relatively small penetration depth appear to support the idea of deep horizontal groundwater flow beneath the Wisconsin River.



## 2. Hydraulic Conductivity Results

Aquifer hydraulic conductivity was determined from baildown tests performed on nineteen monitoring wells. Duplicate analyses were performed at three monitoring wells in order to maintain quality control. The hydraulic conductivity test data was evaluated using a Fortran program developed for data reduction using the Bouwer and Rice Method (See Appendix I for description of method). Input parameters such as well diameter, penetration depth and aquifer thickness were determined from well construction details and boring logs from each test location. Hydraulic conductivity test data, recovery graphs, input parameters and results are shown in Appendix I. Test results and quality control analyses are summarized in Table 10.

-34-

Hydraulic conductivity values range from a low of 1.7 x  $10^{-4}$  cm/s at Monitoring Well C4D to 8.1 x  $10^{-2}$  cm/s at Monitoring Well E22. The boring log for Monitoring Well C4D describes the screened formation as fine sand. However, the baildown test results appear to indicate a somewhat less permeable formation or possible drilling mud exfiltration into the formation. Monitoring Well C4D was advanced using mud rotary drilling without driving casing. A bentonite drilling mud was used to keep the borehole open and to remove drilling cuttings. As a result, the actual aquifer hydraulic conductivity may be somewhat greater than indicated by the test at Well C4D. Similar drilling techniques were used at Monitoring Wells E20, E30 and W56. Therefore, hydraulic conductivity values determined from baildown tests performed on these wells may be lower than actual values. Monitoring well drilling methods are also presented in Table 10. Comparison of hydraulic conductivity values for Monitoring Wells E20 and E22, which are located approximately 150 feet apart and are apparently screened in the same unit. indicate a relatively large difference in hydraulic conductivity (8 x  $10^{-2}$  vs  $0.2 \times 10^{-2}$  cm/s). This indicates that the hydraulic conductivity may vary over short distances due to subtle changes in soil or that drilling procedures used may have a strong influence on the results.

Results of duplicate hydraulic conductivity test performed on three wells are presented in Table 10. The average, difference and percent error are also presented in order to show the degree to which the tests could be replicated.



The percent error was calculated by dividing the difference of the two tests by the average. In general, the percent error ranged from approximately 1% in Monitoring Well W55 to almost 20% at Monitoring Well E20. This appears to be within the range of other variations as described above.

#### C. SOIL GAS RESULTS

### 1. West Study Area

Soil gas samples were collected at a total of 151 locations (64 East Well Field, 87 West Well Field). The West Well Field soil gas station locations are presented on Drawing 13076-B18. Soil gas stations SG1 through SG15 were located on an inner arc surrounding Production Well CW6. Soil gas stations SG16 through SG30 were located on an outer arc surrounding well CW6. The soil gas stations on each arc were located approximately 200 feet apart. Soil gas stations SG31 through SG57, SG101 through SG107, SG111 through SG125 and SG132 through SG143 were located at Marathon Electric.

Soil gas results are presented in Appendix D. No quantifiable volatile organic compounds (VOCs) concentrations were detected at soil gas stations located on either arc surrounding Production Well CW6 (stations SG1 through SG30). The "BMDL" PCE concentrations reported at stations SG21 through SG28 and in blank SB03, and the TCE concentration reported at station SG21 appear to be the result of a carryover error in the gas chromatograph from a water sample analyzed earlier in the same day. Repeated analyses conducted at soil gas stations SG21 and SG25 did not indicate detectable PCE or TCE concentrations. TCE was detected at concentrations below reportable limits at soil gas stations SG34 and SG50. The source of these soil gas detections is not known at this time. However, soil gas station SG50 is located adjacent to the service department of Marathon Electric where TCE was reportedly used to degrease wire used in manufacturing generators and motors (WDNR, 1982). Benzene was detected at concentrations below reportable limits at stations SG39, SG40 and SG43. These stations are located adjacent to a Marathon Electric employee parking lot and an underground fuel tank.

Elevated concentrations of TCE were detected at soil gas stations SG105, SG121, SG122, SG123, SG124, SG125, SG141 and SG142. These stations are



located in a paved parking lot directly south of the Marathon Electric Assembly building shipping area (refer to Drawing 13076-B19 for results). The former City of Wausau landfill reportedly occupies a sand and gravel pit which was located beneath this parking lot. Based on interviews with former landfill employees, the limits of refuse of the former landfill encompasses the soil gas detection areas. The highest TCE soil gas readings appear to be concentrated near the north central portion of the former landfill. However, TCE was also detected at concentrations below reportable limits at stations SG136 and SG140, located at the southern and central portions of the former landfill, respectively.

In addition to TCE, several other volatile organic compounds (VOCs) including tetrachloroethene, 1,1-dichloroethene, toluene, benzene and 1,1,1-trichloroethane were detected in the soil gas within the former landfill boundary (Refer to Appendix D). In general, these compounds were present at concentrations below reportable limits.

## 2. East Study Area

Soil gas samples were collected at 64 locations throughout the east well field area. Investigated properties included: Marathon Box, Marathon Press, Wergin Construction, Camelot Cleaners, C.M. St. P. & P. Railroad, Wausau Chemical, Wausau Energy, Gorwitz Furs, and ETCO Electric. Soil gas station locations and PCE concentrations are shown in drawing 13076-B20. A summary of analytical results are presented in Appendix D.

Soil gas analyses indicate detectable concentrations of PCE at several locations including:

- The northwest portion of Marathon Box Co.;
- Camelot Cleaners;
- Wausau Energy;
- Marathon Press;
- ETCO Electric Co.;
- Gorwitz Furs;
- . The City filtration plant; and
  - Wausau Chemical.



13076.28

The highest concentration of PCE in the soil gas was detected at station SG57, located near the south side of Wausau Chemical. Station SG57 is located next to the southwest corner of the impoundment structure, which surrounded the former solvent storage tanks. A documented release of approximately 900 gallons of PCE occurred in this area in December 1983. Due to instrument overrange, the PCE soil gas concentration at station SG57 was estimated at 4080 ug/L. The soil gas PCE concentrations appeared to abruptly decrease toward the north, south and west away from the former solvent storage area. A more gradual decrease in soil gas PCE concentrations was observed toward the east-northeast (refer to Drawing 13076-B20).

Elevated concentrations of PCE were also detected at soil gas stations SG118 and SG119. These stations are located near the north side of Wausau Chemical where a release of approximately 200 gallons of PCE reportedly occurred in February 1983 (Refer to Industrial Survey). Soil gas samples from stations SG92 and SG93 also indicated elevated concentrations of PCE. These stations are located near the intersection of E. Wausau Avenue and the C.M. St. P. & P. Railroad right-of-way, directly northeast of Wausau Chemical.

Relatively low PCE concentrations were detected in soil gas samples taken from several other facilities located in the vicinity of the East Well Field. PCE concentrations ranging from below the minimum reportable limit of 1.0 ug/L (BMDL) to 1.30 ug/L were detected at several soil gas stations located at the Marathon Press facility. In addition to the PCE soil gas concentrations shown in Drawing 13076-B20, TCE and bromodichloromethane were also detected at concentrations below minimum reportable limits (BMDL) at soil gas station SG76. Soil gas stations SG76 and SG77 are located along the south side of the Marathon Press north building. PCE was also detected at relatively low concentrations (<5.0 ug/L) at soil gas stations SG130 (Gorwitz Furs), SG131 (ETCO Electric), SG73 and SG74 (Wausau Energy), SG147 (Wergin Construction) and SG88 and SG100 (Camelot Cleaners). 1,1,-dichloroethene (1,1,-DCE) was detected at concentrations below minimum reportable limits at soil gas station SG88 (Camelot Cleaners).



## 3. Discussion of Soil Gas Results

Presently, the application of soil gas investigations in determining the extent of VOCs in groundwater is in a state of development. Several investigations (Marrin and Thompson 1987 and Kerfoot et.al., 1986) have indicated areal distribution of contaminants in soil gas correspond to contaminant distributions in watertable aquifers. However, most of these investigations were performed in arid climates such as the southwestern United States. In humid-temperate climates, precipitation tends to flush the vadose (unsaturated) zone more frequently, obscuring potential soil gas patterns. In addition, recharge of precipitation creates an upper surface of uncontaminated water so that the VOCs in the groundwater are not readily volatilized into the gaseous phase above the water table. The rate of volatilization may also be limited by the lower average temperature in the northern United States.

The distribution of volatile halogenated hydrocarbons (PCE and TCE) shown on Drawings 13076-B19 and 13076-B20 appears to be a function of several variables including: soil type, surface cover material, proximity to source area, soil moisture content, surface topography and/or depth to watertable, and Henry's Law Constant. The Henry's Law Constant describes a compound's ability to partition from a liquid phase to a gaseous phase. The Henry's Law Constant may be estimated from the aqueous solubility, vapor pressure and molecular weight of a compound. Table 11 shows the Henry's Law Constant for a variety of common solvents. Those compounds possessing the highest Henry's Law Constants tend to partition to the greatest extent into the gaseous phase and therefore are most readily detected by soil gas methods. For example, if PCE and trans-1,2-DCE were present in the soil at equal concentrations, the PCE may be present in the soil gas at concentrations considerably greater than those of trans-1,2-DCE.

Based on the preceding discussion, it is apparent that soil gas distribution of halogenated hydrocarbons does not always reflect the distribution of the volatile compounds in the watertable aquifer. Rather, the distribution of VOCs in the soil gas is a function of several influencing factors including: concentration of volatile compounds in the groundwater, depth to groundwater, presence of unsaturated zone contamination, nature of the surface cover,



temperature, barometric pressure, Henry's Law constants and several other factors. Despite these influencing factors, analysis of the magnitude and distribution of soil gas detection points can be very useful in identifying potential source areas.

-39-

The TCE concentrations observed on the west side at soil gas stations SG105, SG121, SG122, SG123, SG124, SG125, SG141 and SG142 (Appendix D) probably indicate the presence of TCE contaminated soils or refuse materials within the landfill. The relatively large depth to the watertable (±30 feet) in the vicinity of the landfill make it unlikely the soil gas detections are solely the result of volatilization from contaminated groundwater beneath the area. The Marathon Electric parking lot, which presently covers much of the landfill, may have acted as a cap, limiting the release of TCE from the soil/refuse to the atmosphere and resulting in elevated concentrations of TCE in the gaseous phase below the pavement (refer to Drawing 13076-B19).

The distribution of PCE in soil gas in the vicinity of the East Well Field is somewhat more complicated. Theoretically, the relatively shallow depth to water (approximately 12 feet) should increase the likelihood that the detected soil gas concentrations would correspond to groundwater contamination. However, soil gas stations SG144, SG145 and SG146 do not indicate detectable PCE concentrations even though they are located directly adjacent to watertable Monitoring Well GM9S, which has a PCE concentration in excess of 5,000 ug/L (refer to Appendix G). However, based on the boring log of GM9S, it is possible that a relatively low permeability material may be present which hinders the migration of soil gas vapors from the watertable to the sample collection depth. The boring log for GM9S indicates approximately five feet of sand gravel and clay just above the watertable. Conversely, PCE concentrations at watertable Monitoring Well WC3B were 19 ug/L whereas soil gas PCE concentrations at station SG127 (approximately 15 feet north of WC3B) were 37.6 ug/L. Groundwater PCE concentrations in the vicinity of Monitoring Well WC3B have apparently been reduced by the groundwater extraction system operating directly west of well WC3B. The relatively high soil gas concentrations probably indicate remaining PCE contamination in the unsaturated zone. These observations appear to indicate that volatile



halogenated hydrocarbons partition into the gaseous phase and are more readily detectable in soil gas when released from soils impacted by the compound rather than from a groundwater impact. However, the volatile organic compounds may be introduced to the vadose zone by either a surface release of the compound into the soils or by a sharp watertable drop which results in retention of the volatile compound by soils just above the watertable.

-40-

The distribution of PCE in soil gas in the vicinity of the East Well Field (see Drawing 13076-B20) appears to be the result of multiple releases. The relatively high soil gas concentrations present at the south end of the Wausau Chemical property may be the result of one or more PCE releases from the bulk solvent storage operations on the south side of Wausau Chemical. The southwest-northeast elongation of the soil gas distribution may be indicative of the present PCE concentrations at the watertable or may be a remnant in soils above the watertable. PCE was observed in the shallow aquifer east of the former solvent storage area at concentrations of nearly 1000 ug/L at boring E32 (refer to Occurrence of Total Chlorinated Ethenes section). The PCE distribution in the soil gas may also be the result of additional PCE releases northeast of the former solvent tank farm.

Whatever the source of PCE, the observed PCE distribution in the soil gas appears to be influenced by topographic variations. The southeastern portion of the 5.0 ug/L contour generally conforms to a steep topographic rise toward the east and southeast. The depth to water increases from approximately 12 feet at SG96 to approximately 30 feet at SG62, decreasing the soil gas concentration gradient in the unsaturated zone.

There are also several potential explanations for the observed PCE distribution in the soil gas at the north side of the Wausau Chemical property and at the C.M. St. P. & P. Railroad near E. Wausau Avenue. The observed PCE soil gas concentrations at SG118 and SG119 may be the result of the February 1983 release of approximately 200 gallons of PCE at the Wausau Chemical northwest loading dock area. Since Production Well CW3 has been pumped nearly continuously since 1983, the product probably migrated northeast toward Production Well CW3 (refer to Drawing 13076-B15 for potentiometric map). If



13076.28

the watertable was to fluctuate in response to variations in production well pumpage and/or changes in river elevation, the soils directly above the watertable could become periodically affected by the PCE in the groundwater. The resulting soil gas distribution could then appear as zones of residual PCE in the liquid and gas phase of the unsaturated zone along a flow line to the production well. This theory may be supported by the present PCE groundwater impact at Monitoring Well GM9S (refer to Occurrence of Total Chlorinated Ethenes in the Aquifer section) which lies along a flow line downgradient of the February 1983 PCE release and soil gas stations SG118, SG92 and SG93. An alternative hypothesis suggests the PCE detected at SG92 and SG93 is the result of a separate release event unrelated to the February 1983 PCE spill near the northwest loading dock of Wausau Chemical.

-41-

The relatively low PCE concentrations detected at SG88 and SG100 (Camelot Cleaners) may be the result of a single or several releases during the course of operation of the dry-cleaning establishment. Given the distance from production wells CW3 and CW4, the operating practices and the low concentration of PCE detected in the soil gas surrounding the facility, Camelot Cleaners is probably not a potential source area for the municipal well field contamination.

The relatively low level PCE concentrations detected from soil gas samples obtained at Marathon Press and from the north side of Wausau Energy may be the result of present or past groundwater PCE impacts from off-site sources and/or may be due to several small surface releases in the area. Eastward migration of PCE impacted groundwater from the Wausau Chemical releases may have resulted in residual contamination of soils in the vicinity of the water table at the Marathon Press and Wausau Energy facilities. However, Foth and Van Dyke (December, 1986) described slight PCE impact in shallow soils (depth of 2 to 3 feet) from borings performed along the north side of the facility. Due to the location with respect to the water table, this soil impact does not appear to have resulted from contaminated groundwater migration.

The PCE detected at SG130 and SG131 is probably the result of either sampling device carry-over error from SG129 or GC carry-over error from SG129.



-42-

13076.28

# D. SURFACE AND GROUNDWATER QUALITY

### 1. General Water Quality Parameters

Round 1 Groundwater samples were collected from existing wells on September 29 through October 7, 1987. The sample color, odor and turbidity were described immediately after sampling. The sample pH and specific conductance were also recorded immediately after sampling. Sample descriptions, pH measurements and specific conductance readings are presented in Appendix E. The sample nomenclature system is defined in the Site Sampling Plan, Appendix A of the Final QAPP, dated September, 1987. In general, the sample code consists of the sample location name (see Drawing 13076-B11) preceded by the code letters "WE" which refer to Wausau, U.S. EPA lead. The sample location is followed by a sampling event round number. The round number preceded by 9 indicates a duplicate sample.

The groundwater pH generally tended to range from neutral (7.0) to slightly acidic. However, a pH of 9.64 was recorded from the groundwater sample obtained from Monitoring Well MW1A. This pH is considerably higher than any other well, probably indicating calcium carbonate contamination by cement grout used in the well construction. Therefore, the reliability of samples from this well is questionable.

Specific conductance readings ranged from 140  $\mu$ mho/cm at Monitoring Well W3A to 570  $\mu$ mho/cm at Monitoring Well MW13. The specific conductance readings are generally low, indicating relatively low concentrations of dissolved solids in groundwater. The low dissolved solid concentrations are probably due to low aquifer residence times (rapid groundwater flow rates from recharge to discharge areas) or groundwater recharge from surface water bodies. In addition, aquifer materials are composed predominantly of relatively insoluble silicate sand, derived from glacial erosion and transport of igneous and metamorphic rock.

Results of Round 1 general water quality parameters analyses are presented in Appendix E. The analyzed parameters consisted of common anions and cations. Groundwater in the vicinity of the City Well Field can generally be described as calcium, magnesium-bicarbonate, chloride type water. The inorganic data



was plotted on trilinear diagrams, however, the vertical partitioning of groundwater described by other investigations (RMT, and Geraghty & Miller, 1987) was not apparent. Further evaluation of these data will be conducted after receiving results of Round 2 analyses.

# 2. Occurrence of Total Chlorinated Ethenes in the Aquifer

The distribution of total chlorinated ethenes in the aguifer (Drawings 13076-B21, 13076-B22 and 13076-B23) is based on a combination of data obtained from contract laboratory VOC analyses of Round 1 groundwater samples (Appendix F) and field GC analyses of groundwater samples collected during drilling (Appendix G). In order to verify the field GC analyses of groundwater samples collected during drilling, thirty duplicate groundwater samples were submitted to the CLP for VOC analyses. Results of the contract laboratory analyses of groundwater samples collected during drilling are presented in Appendix G. A comparison of total chlorinated ethene concentration as determined by the Warzyn field GC and by the contract laboratory analyses is presented in Table 12 and shown graphically in Drawing 13076-A15. The contract laboratory analyses generally agree closely with the results of the field GC analyses. However, the field GC analyses of the high concentration samples (WE-GW55-115, WE-GE35-18, WE-GW53-125, and WE-GW53-85) tend to be consistently higher than contract laboratory results for these samples. The discrepancy probably results from estimation of field GC concentrations when the sample concentration was outside the linear range of the working standards. A second dilution was generally not made due to time constraints.

Based on the specific types of compounds detected and the vertical and lateral distribution of these compounds, there appears to be at least three Chlorinated Ethene sources affecting the City Well Field. TCE is the predominant volatile organic compound detected at City Production Well CW6, although below minimum reportable limit (BMDL), concentrations of PCE and DCE have also been previously reported (Weston, 1985). The East Well Field (Production Wells CW3 and CW4) have indicated considerable PCE, TCE and DCE impacts at both wells. Production Well CW4 has indicated steadily decreasing concentrations of all three constituents since February 1984 (Weston, 1985). Production Well CW3 has indicated decreasing PCE and DCE concentration since

WARZYN

. . .

the problem was discovered in early 1982. However, TCE concentrations at Production Well CW3 have remained relatively constant at concentrations ranging between 80 ug/L and 210 ug/L.

The areal distribution of Total Chlorinated Ethenes is presented in Drawing 13076-B21. The drawing indicates four distinct total chlorinated ethene plumes in the aquifer. These plumes were differentiated on the basis of chemical composition, vertical occurrence in the aquifer, and suspected source location. The specific plumes were also differentiated based on which production wells they affected.

Monitoring Wells W52, W53, W54, W55, C4D, R2D, and R4D appear to delineate a deep (greater than 100 feet) north-south trending TCE plume which has affected Production Well CW6. Based on the soil gas results (Drawing 13076-B19), and the vertical distribution of TCE in the aquifer (Drawing 13076-B23), the plume appears to be derived from a source located within the northern portion of the abandoned City landfill (property now owned by Marathon Electric).

Groundwater samples collected during drilling indicate Total Chlorinated Ethenes (predominantly TCE) vertically distributed throughout the aquifer in the vicinity of Monitoring Wells W53 and W54. The maximum Total Chlorinated Ethene concentration (2280 ug/L) in Monitoring Well W53 was observed at a depth of approximately 115 feet below surface. Monitoring Well W54 was drilled to a depth of 85 feet and encountered a maximum Total Chlorinated Ethene concentration of 404 ug/L. The Total Chlorinated Ethene concentration contours shown on Drawing 13076-B21 appear to be inconsistent with the highest concentration detected at Monitoring Well W54. This inconsistency is based on the assumption that maximum concentrations would be encountered in Monitoring Well W54 at depths ranging between 115 and 130 feet as encountered in Monitoring Wells W53 and R4D, respectively.

The vertical distribution of TCE below the northern portion of the former City landfill may be the result of slight downward vertical gradients. However, interviews of former landfill employees indicated that bulk liquid wastes were disposed in the landfill during its operational period (1948-1955). Refer to



Appendix L for Industrial Survey report. Reportedly, these liquids were dumped into the gravel pit and were not containerized. If TCE was present in these liquids, it is possible the concentrations may have exceeded the solubility limit of the compound, and therefore might have migrated downward as a non-aqueous phase liquid (NAPL), due to the gravity flow.

Isoconcentration section BB' (Drawing 13076-B23) indicates the TCE plume migration north toward City Production Well CW6. The plume was detected in concentrations in excess of 500 ug/L in Monitoring Wells W53, R4D, C2S, W52, R2D and W55. With the exception of C2S, all of these monitoring wells are screened at depths greater than 100 feet deep. During Round 1 sampling (October, 1987), Monitoring Well C2S had a TCE concentration of 1370 ug/L, possibly indicating northward migration of the shallow TCE impact detected in groundwater below the northern portion of the former City landfill (located approximately 300 feet south of Monitoring Well C2S). The abrupt discontinuity in the plume in the vicinity of Monitoring Well R3D appears to be the result of the cross-section line diverging from the zone of maximum TCE concentrations shown on Drawing 13076-B21 (refer to Drawing 13076-B11 for cross-section location). The abrupt discontinuity in the TCE concentrations in the vicinity of R3D may also be attributed to altered groundwater flow patterns caused by the additional recharge from Bos Creek as a result of Production Well CW6 being pumped to waste into the creek since February 1986. Based on Drawing 13076-B17, it is apparent Bos Creek presently acts as a significant recharge boundary. However, the recharge influence of Bos Creek was probably considerably less, prior to Production Well CW6 pumpage into the creek. Total Chlorinated Ethene concentrations substantially increase in the vicinity of Monitoring Well W55 (4320 ug/L) possibly indicating the release of TCE from the source area was greater in previous time periods and has since diminished.

TCE was observed in the shallow aquifer at Monitoring Wells R3S, R2S, W55A, W56A and MW4B. This plume is shown on Drawing 13076-B21 by the lightly screened contours between Bos Creek and Production Well CW6. A probable source of the TCE in this area is the pumping of TCE contaminated water from Production Well CW6 to waste into Bos Creek. Based on field GC analyses,



surface water TCE concentrations within the creek range from 160 ug/L at the CW6 discharge to 108 ug/L at the ponded area north of Randolph Street (refer to Appendix G). TCE was not detected in surface water upstream of the CW6 discharge. Relatively strong downward vertical groundwater flow gradients at Monitoring Well nests R3 and R2 combined with elevated TCE levels at these wells strongly indicate the induced recharge of TCE impacted water into the aquifer. Once in the aquifer, the shallow TCE contaminated water appears to migrate north toward Production Well CW6 (refer to Drawing 13076-B23 for isoconcentration profile).

-46-

The distribution of TCE in Monitoring Wells E21, E27, E30, E31 and Production Well CW3 suggest eastward migration of TCE below the Wisconsin River, from the vicinity of the former City landfill (refer to Drawing 13076-B21). Isoconcentration section AA' (refer to Drawing 13076-B22) shows the east-west vertical distribution of TCE originating from the location of the former City landfill. The section indicates TCE vertically distributed throughout the aquifer in the vicinity of Monitoring Well W53. The maximum TCE concentrations in Monitoring Well W53 were observed at a depth of approximately 115 feet below surface. A portion of the TCE entering the deep aquifer below the landfill is shown to be induced to flow east by Production Well CW3. Where TCE concentrations are not available, such as below the Wisconsin River, the contours are inferred based on the potentiometric cross-section AA' (Drawing 13076-B16). The strong induced recharge from the Wisconsin River forces the TCE to flow along the base of the aquifer, where it is detected at Monitoring Well E27 at concentrations in excess of 500 ug/L. The TCE then appears to migrate toward Production Well CW3 along a flow line which extends just north of Monitoring Well E30. As the plume approaches Production Well CW3, groundwater flow converges, causing the contaminated groundwater to ascend to the screened interval. The apparent discontinuity of the 10 ug/L and 100 ug/L contours between Monitoring Well E27 and Production Well CW3 are the result of the cross-section line diverging slightly out from the apparent zone of maximum TCE concentrations.

The resulting TCE concentrations in Production Wells CW3 and CW6 is significantly less than the highest observed TCE concentrations in the surrounding aquifer due to dilution across the screened interval. The TCE



contamination portion of the aquifer appears to be less than 20 feet thick and is laterally restricted to a relatively narrow flow path into the well. Whereas the pumping well produces water nearly equally from all sides of the 50 foot screened interval, resulting in a dilution factor that appears to range from 15 to 25 times less than the concentrations observed within the aquifer.

Drawing 13076-B21 also indicates substantial concentrations of total chlorinated ethenes (predominantly PCE) within the vicinity of the East Well Field. However, the concentrations in the vicinity of the East Well Field were consistently higher in the water table monitoring wells. Therefore, monitoring wells screened below the water table were not used in contouring the PCE distribution in the vicinity of the East Well Field. Monitoring Well FVD2 was also omitted because the chlorinated ethene concentrations were obscured by dilution due to high xylene concentrations.

The distribution of chlorinated ethenes (Drawing 13076-B21) appears to indicate three plumes within the East Well Field area, one from the west side landfill and two southwest of City well CW3. The two plumes southwest of CW3 are shown on Drawing 13076-B21 as two peaks but appear contiguous. These can be separated based on compounds present, as discussed below.

A plume composed predominantly of PCE was observed directly southwest of Well CW3, centered around Monitoring Well GM9S (Wergin Construction). Based on CLP analyses, the PCE concentration in this well is presently greater than 5,000 ug/L. Volatile organic compound analyses conducted by Geraghty & Miller Inc. in 1986 indicated a PCE concentration of 27.6 ug/L at this well. This increase in PCE concentration appears to indicate a slug of contamination is moving through this area toward Well CW3 rather than a continuous plume.

A second plume southwest of CW3 was observed in the vicinity of Monitoring Well WC2 (east of Wausau Chemical). The groundwater in this area contained total chloroethenes concentrations ranging up to 1,450 ug/L at Boring E32. Comparatively, the total chloroethenes in this vicinity is divided approximately equally between PCE, TCE and 1,2-DCE (refer to Appendix G). In addition, vinyl chloride was detected in Monitoring Wells E24A and WC6. The



presence of these additional compounds separates this plume from that observed in the vicinity of GM9S. The presence of the lower chlorinated compounds indicates that a significant amount of degradation has occurred through reductive dehalogenation (Parsons et. al., 1984).

-48-

Based on the difference in plume composition and the difference in areal distribution, the two VHH impacts appear to be the result of separate release events. The distribution of PCE in the soil gas beneath the northern portion of Wausau Chemical and the location along a flow path downgradient from a documented release, indicate the impact in the vicinity of GM9S may have resulted from the February 1983 release of approximately 200 gallons of PCE at the north loading dock of Wausau Chemical. The southern chlorinated ethene plume may be the result of undocumented releases in the vicinity of the C.M. St. P & P Railroad, on the east side of Wausau Chemical or the result of eastward migration from one or more releases from the former bulk solvent storage tanks located on the south side of Wausau Chemical. A documented release of approximately 900 gallons of PCE occurred in the area during December 1983. In addition, PCE, TCE, 1,2-DCE, toluene and xylene were reportedly observed in soils and groundwater during the 1975 expansion of the City Water Treatment Plant, directly south of Wausau Chemical (WDNR 1983). Therefore, the observed VHH distributions in the groundwater (Drawing 13076-B21) may be the result of initial impact from these releases or may have been caused by precipitation flushing PCE from the soils in the vicinity of the source. The elevated soil gas concentrations (refer to Drawing 13076-B20) recorded in the vicinity of the former Bulk Solvent storage area appear to indicate a residual impact of PCE on soils in the vicinity of the south side of Wausau Chemical. This impact will be further investigated during the Phase II investigation.

Based on the potentiometric map shown in Drawing 13076-B15, a groundwater divide extends through the south central portion of Wausau Chemical in January 1988. Depending on city well pumpage and river levels this divide could disappear or shift considerably. Contaminants released in the vicinity of this groundwater divide could migrate toward the east resulting in a contaminant distribution similar to the one observed directly east of Wausau Chemical.



#### IV. PRELIMINARY GROUNDWATER MODELING

### A. INTRODUCTION

Preliminary groundwater flow and contaminant transport modeling of the alluvial aquifer in the vicinity of the City of Wausau was conducted to provide an estimate of groundwater flow directions and the potential fate of contaminants introduced into the aquifer at known or potential source locations. Specific objectives of this preliminary modeling effort included:

- Identification of groundwater flow directions under variable pumping rates and river stages;
- Determination of the zones of capture of the municipal wells and identification of potential contaminant source areas within those zones of capture;
- Identification of the aquifer parameters (i.e., recharge, permeability, riverbed leakance) to which the simulated groundwater flow direction and velocity are most sensitive.

### 1. Available Data

Data available for use in development of the preliminary groundwater flow and contaminant transport model included field and laboratory data collected prior to the RI activities. This includes:

- Reports from previous hydrogeologic investigations of the contaminated well field (Weston, 1985; Geraghty & Miller Inc. and RMT, 1987; and Twin Cities Testing, 1986).
- Published and unpublished hydrogeologic reports (Kendy 1986, unpublished thesis - U.W.-Madison).
- Pumping records for the City of Wausau municipal wells, obtained from the Wausau Water and Sewage Utility (both to the water supply system and pumping to waste).
- Pumping records for the Wausau Chemical Company extraction well, obtained from the WDNR.
- Wisconsin River stage data obtained from the Wisconsin Valley Improvement Corporation (WVIC).

In addition to these available data, preliminary results obtained from the concurrent Phase I RI were incorporated as they became available. In



particular, this includes the absence of a bedrock ridge south of Well CW6, the location of contaminant source areas and aquifer permeabilities.

## 2. Model Selection

The USGS modular 3-dimensional groundwater flow model (McDonald and Harbaugh, 1984) referred to as MODFLOW was selected for simulation of groundwater flow. The MODFLOW program was selected for its ability to represent the variety of hydrogeologic conditions encountered in the Wausau area. The flexibility of the MODFLOW code enables modeling of detailed areal variations in hydrogeologic conditions and can also incorporate variations in parameters in the vertical dimension, including uneven bedrock surfaces, variable saturated thicknesses and seepage through low permeability layers overlying the aquifer (i.e., the bed of the Wisconsin River). MODFLOW can simulate the area as a 2-dimensional (2-D) areal problem or can be upgraded to simulate the problem as a quasi 3-dimensional problem if the 2-D simulation appears inadequate.

The version of MODFLOW used in the study was modified by Warzyn to produce output files containing simulated head values and velocity vectors in a format usable by graphics software and for use in subsequent contaminant transport modeling.

The evaluation of potential source areas and contaminant migration to the municipal wells was performed using the transport portion of the "Random Walk" solute transport model (Prickett, et.al., 1981). This model approximates the solution of the contaminant transport equation using advection based on the MODFLOW generated velocity vectors and dispersion through a random process generator. The contaminant transport model described by Prickett was modified by Warzyn to allow direct use of the output from the MODFLOW groundwater flow model. These modifications include the ability to import site grid data files and the groundwater flow velocity vector files.

#### **B. MODEL DEVELOPMENT**

#### <u>1. Hydrogeology</u>

The primary aquifer in the vicinity of the City's Well Field consists of glacial outwash within a low permeability bedrock valley. The aquifer



presence and thickness is controlled by the topography of the underlying Precambrian bedrock valley. Principal sources of water to the glacial aquifer, within the bedrock valley, appear to be from rainfall percolation within the valley, runoff from the bedrock hills and the Wisconsin River.

-51-

Under natural conditions the Wisconsin River would be a regional discharge area for groundwater flowing away from the bedrock highs. Comparison of river stage levels and water levels in monitoring wells adjacent to the river indicate that pumping from the City of Wausau municipal wells has resulted in induced infiltration from the river. This data also indicates considerable head loss (resistance to flow) in the river sediments. However, very little data is available on the geologic characteristics of the river bed sediments adjacent to the well fields. Generally, it can be assumed that finer grained sediments would be deposited toward the south, closer to the Wausau Dam. Coarser sediments can be expected upstream due to swifter currents. Sediments encountered during borings for the Bridge Street renovation (1984) range from fine to coarse grained sand (SP) to organic silts (OL). Refer to Appendix B for a description of soil samples obtained from Wisconsin Department of Transportation (DOT) borings. DOT soil boring locations are shown on Drawing 13076-B11.

Data from previous investigations and Phase I RI activities indicate variable pumping rates at the municipal wells and variable river stages have a strong influence on groundwater flow direction and probable contaminant migration routes. Bos Creek, on the west side of the river, has been shown to be a probable source of infiltration (recharge) to the aquifer between Marathon Electric and the West Well Field. The potential recharge rate appears to have increased after Well CW6 began pumping to waste to a storm sewer which discharges to Bos Creek at Burns Street. The additional recharge at Bos Creek appears to have decreased the radius of influence of the West Well Field at the water table. However, continuity of flow from the south to the north beneath Bos Creek may exist at depth.

## 2. Discretization and Model Setup

The groundwater flow model was set up initially as a single layer areal flow model to determine if adequate results could be obtained using the simpler 2-D



solution. The model was run in the transient (time-variant) mode to allow simulation of variable pumping rates at the municipal wells and variations in river stage elevation.

The transient model, which was developed to simulate flow conditions from January 1976 to May 1987, has one month stress periods (in single time steps) with the exception of October 1986. A temporary one-week drop in the river stage elevation (1187.9 to approximately 1182) in October 1986 was simulated using two stress periods with several additional time steps within the stress periods. The smaller time steps were necessary to accurately simulate the rapid drop and recovery in the river stage elevation and the resultant effects in the aquifer.

The finite difference grid developed for the site model consists of 36 columns and 69 rows (2484 cells) and covers an area 16,100 feet east-west by 19,000 feet north-south. The grid configuration was governed by the following factors:

- The eastern and western limits of the grid extend beyond the bedrock highs that define the limits of the alluvial aquifer;
- The northern and southern limits of the grid were placed beyond the zone of expected influence of the City of Wausau municipal wells;
- Grid spacing was decreased (100 feet spacing) in the vicinity of the municipal wells to increase the numerical accuracy of the simulation of groundwater flow and contaminant migration in areas of increased flow velocities and to try to anticipate future simulation of potential remedial alternatives.

The central portion of the model grid, which covers the areas of concern including the east and west municipal well fields, is illustrated in Drawing 13076-24.

The selection of representative boundary conditions is important as they affect results computed in the interior of the grid. Boundary conditions specified for the Wausau model were either no-flow or head-dependent flow. No-flow boundaries were generally established where bedrock elevations exceed



1200 feet in elevation. This bedrock elevation appears to be approximately where the water table would intersect the bedrock or where the aquifer becomes too thin to model. No-flow boundaries were set along the east and west sides of the model where the alluvial aquifer interfaces with the relatively impermeable bedrock valley walls. To the north and south, head-dependent flow boundaries were established between the bedrock valley walls.

The Wisconsin River, which bisects the modeled area was simulated using the RIVER module in MODFLOW. Leakage through the river bed is computed at each river cell and is dependent on the constant head assigned to the river, the computed head in the aquifer beneath the river and the leakance of the river bed. This is defined as the vertical hydraulic conductivity of the river bed divided by the river bed thickness (K'/m'). Detailed stage data obtained from the WVIC was evaluated and several different river elevations were used at different time steps in the transient simulation. The river elevation was set at 1187.9 above the dam and 1161 below the dam from January 1976 for approximately 129 months until October 1986. The head was dropped to 1182 above the dam for one week and then raised to 1187.5 for the remainder of the simulation. Bos Creek was added to the model in February 1986 when City Well CW6 began pumping to waste. Prior to this time it is assumed that Bos Creek did not have sufficient flow to create a significant effect on the groundwater flow system. This needs to be evaluated further.

Detailed daily pumping records obtained from the Wausau Water and Sewage Utility were used to develop the pumping file used in MODFLOW. Monthly pumping volumes and an average monthly pumping rate (in cubic feet per second) were calculated for each municipal well for every month from January 1976 to May 1987. The monthly pumping rates were then used in the transient flow model. Additional pumping data for the Wausau Chemical Company extraction system was obtained from the WDNR. The City of Wausau also supplied additional data on the Wergin Construction pumping well which has been operated as a barrier well to protect Production Well CW3 since July 1982. This well was originally installed in September, 1980 to function as a heat pump well.



# C. FLOW MODEL CALIBRATION

# 1. Calibration Data

The single layer flow model provides simulated heads which are representative of the potential across the entire thickness of the aquifer. In the absence of significant vertical gradients, the simulated heads generated by the calibrated model should be comparable to the water table elevations at the same locations.

Observed water level data at selected site monitor wells were plotted against time. Simulated head at corresponding locations were then plotted for each model calibration run in order to provide a basis for determining the ability of the model to simulate observed conditions.

## 2. Calibration Procedure

Flow model calibration proceeded through numerous iterations with variation of hydrogeologic input parameters for each run. The primary calibration parameters were aquifer hydraulic conductivity and the river bed conductance.

Significant changes in pumping rates at the municipal wells resulted in marked changes in water levels in site monitor wells and provided a good basis for making adjustments in aquifer hydraulic conductivity.

The drop in the river stage elevation in October 1986, also had a significant effect on observed water levels. The decrease in water levels in the aquifer provided a good basis of comparison for determining river bed leakance. The river bed leakance controls, in part, the magnitude of the drop in water levels in wells adjacent to the river and the rate of water level recovery in those wells after the river level returned to its normal stage.

## 3. Parameter Selection

The following discussion is a brief description of the procedures used to select the parameters used in the flow model.

Aquifer permeability was initially set at  $1 \times 10^{-3}$  ft/s for the entire aquifer. In order to obtain a better match at the selected calibration



points, a variable permeability array was developed. The central portion of the study area, which encompasses the West Well Field and City Well CW3 was set at a higher permeability (5 x  $10^{-3}$  ft/s) based in part on results of the pumping test conducted by Geraghty & Miller Inc. The high permeability window is set in the center of the relict river valley where surface water flow velocities during deposition may have been highest and the coarser grained material would have been the primary deposits. West and north of this high permeability window, permeabilities were decreased toward the bedrock highs that formed the sides of the former river valley. This was done in part to minimize problems with heads decreasing to elevations lower than the bedrock elevation (no-flow boundary) at a large number of nodes adjacent to the bedrock valley during certain time steps. The permeability of the aquifer to the east of the high permeability window was set at 1 x  $10^{-3}$  ft/s. To the south, the permeability values were adjusted several times in an effort to match observed conditions in the vicinity of Well CW4. As discussed below, observed levels for Well WGS10 were always below simulated levels. Therefore, the permeability was reduced during calibration efforts. Discussion of the results will provide recommendations to resolve this issue. However, preliminary model results presented had permeabilities set at 1 x  $10^{-3}$  ft/s to a point midway between Wells WGS9 and WGS10. South of that, the permeability was set at 5 x  $10^{-4}$  ft/s.

-55-

Recharge was initially assumed to be 10 inches per year across the entire study area. The high permeability of the valley bottom deposits and the relatively flat topography in the valley would result in low runoff and high infiltration. Initial calibration runs resulted in difficulty matching points near the bedrock/aquifer interface. Runoff from the bedrock highs into the valley would result in increased recharge at the base of the bedrock highs. Therefore, recharge was increased to 30 inches per year in the cells at the base of the bedrock highs, with little change in head. Recharge values on the east and west edges of the aquifer were increased to 90 inches per year to increase flow velocities. Although this seems large, there was little change in the simulated water levels.

River bed leakance (K'/m') was varied during the course of the preliminary modeling efforts. The thickness of the river bed sediment was assumed to be



1 foot for all calibration runs. Initially the river bed conductivity was set at 1 x  $10^{-3}$  ft/s. This resulted in reasonable matches in the vicinity of the West Well Field. Lower hydraulic conductivities resulted in reasonable matches in the vicinity of the East Well Field. The final preliminary model calibration run used river bed conductivities of 1 x  $10^{-3}$  ft/s in the upper reaches of the river adjacent to the West Well Field, 1 x  $10^{-4}$  ft/s for a short reach of the river where Bos Creek discharges to the river and  $5 \times 10^{-5}$  ft/s from Bos Creek to the southern end of the modeled area. Bos Creek was modeled using a bed conductivity of 1 x  $10^{-5}$  ft/s. Although no independent measurements of the river bed conductivity are available, it can be argued that the narrower river adjacent to the West Well Field has higher river flow velocities and fewer fines deposited than the wider river adjacent to the East Well Field. In addition, it is expected that the thickness of the river bed may be greater closer to the dam due to slower flow and increased deposition of fines.

A detailed cell-by-cell description of all model input data, including calibration parameters is included in Appendix J.

## 4. Groundwater Flow Model Results

Transient head files from the final preliminary model calibration run were used to generate the observed versus simulated head plots contained in Appendix K. In general, simulated heads in the central portion of the study area appear to match well with the observed heads. This includes Wells MW1A, MW9, MW12, TCT44 and C2S. Deviations between the simulated and observed conditions occur only on the perimeter of the study area, with the exception of R2D.

Simulated heads at Well R2D, adjacent to Bos Creek, are lower than observed heads. Recharge of the aquifer from Bos Creek appears to be underestimated. Therefore, it appears that the hydraulic conductivity of the stream bed sediments in Bos Creek may be greater than was assumed.

North of the West Well Field, simulated heads at wells CW9-OBS and GM4D and the Plum Street test well are lower than observed head levels at those wells.



The presence of a sand and gravel operation on Campus Drive, in the vicinity of these wells, would likely result in increased recharge in this area due to ponding of surface water runoff in the sand and gravel pit. The increased recharge should increase the simulated head levels at the above mentioned wells.

Simulated heads at Well WGS10, adjacent to the Bridge Street bridge, are higher than observed levels. The magnitude of the difference (2 to 3 feet) appears to indicate that there may be a pumping well, in the vicinity of this well, that has not been incorporated into the model. Variations of river bed conductance and/or aquifer hydraulic conductivity will change the simulated head at this well but not likely to the degree necessary to obtain a reasonable match with observed head levels. Both possibilities will be evaluated in future analyses.

Groundwater head contour maps for two stress periods in the final preliminary calibration are shown in Drawings 13076-B25 and 13076-B26. The head contour map from September 1985 (Drawing 13076-B25) shows the zone of influence around the West Well Field extends south of Bos Creek to the Marathon Electric property. A groundwater divide created by pumping at the West Well Field and at City Wells CW3 and CW4 on the east side of the river, occurs within the vicinity of the Marathon Electric property and the former City of Wausau landfill. Flow from the vicinity of the former landfill on the west side of the river would occur toward wells CW6, CW7 and CW9 to the northeast and toward wells CW3 and CW4 to the southeast. Flow on the east side of the river is divided between Well CW3 and Well CW4 on this particular date. The divide, which is shown in the vicinity of Wausau Chemical, is quite variable depending on the pumping rates at Wells CW3 and CW4.

The head contour map from April 1987 generally shows an overall head distribution similar to the simulated heads in September 1985. In close proximity to the municipal wells, flow directions are somewhat different due to the variable pumping rates. One significant difference from the September 1985 map is that discharge of water pumped from Well CW6 to Bos Creek results in increased recharge in this area, creating a small mound.



This groundwater mounding may result in a barrier to flow between areas south of Bos Creek and the West Well Field.

### D. CONTAMINANT TRANSPORT MODELING

1. Contaminant Transport Modeling Procedure

The purpose of the preliminary contaminant transport modeling was to determine the potential fate of contaminants introduced into the aquifer at known or potential contaminant source locations. Input parameters from the last preliminary groundwater flow model calibration run were used for the contaminant transport simulation. The contaminant transport simulation was run in the transient mode for the same time period as the groundwater flow model (January 1976 to May 1987). However, because the transport model requires equal length stress periods, no change in river stage in October 1986 was simulated. Due to the very short duration and rapid recovery this appears reasonable. No attempt was made to calibrate simulated concentrations with observed concentrations during the preliminary modeling effort. The contaminant transport model will be calibrated to VHH concentrations observed during the round II sampling event (November-December, 1987), during the Phase II investigation. The calibrated contaminant transport model will then be used to evaluate selected remedial actions during the Feasibility Study.

Soil gas sampling and groundwater sampling, conducted during the course of Phase I RI field activities, indicate the presence of potential sources at the former City of Wausau landfill, on the west side of the Wisconsin River and on Wausau Chemical Company property, on the east side of the river. Due to the lower level of calibration in the vicinity of Well CW4 (see discussion regarding Well WGS10) no transport results for the Wausau Chemical source are reported. For the purpose of the preliminary modeling, simulation of the landfill source was simplified by creating a constant source of one contaminant particle per day. The mass of the particles was set at one pound. Longitudinal dispersivity and transverse dispersivity were set at 20 and 10, respectively. The retardation factor was set at 1.0.

## 1. Results of Landfill Source Simulation

Drawing 13076-B27 shows the extent of contaminant migration from a source at the landfill at the end of the contaminant transport simulation (May 1987).



The simulation of a source in the vicinity of the former landfill indicates the contaminant plume diverges, with a portion of the plume moving to the northeast toward city well CW6 and a portion moving beneath the river to the east toward city well CW3. The simulation of both flow and transport indicates the river does not form a hydraulic barrier to contaminant migration. Based on this simulation, contaminants would reach city wells CW3 and CW6 approximately 5 and 6 years, respectively, after reaching the water table.

-59-



## V. CONCLUSIONS

Based on the results of the Phase I investigation of the Wausau Water supply, the following conclusions were reached:

- Bedrock lithology below the East Well Field differs distinctly from the bedrock lithology underlying the West Well Field. The difference in bedrock weathering apparently causes a much more irregular surface below the West Well Field;
- Boring W55 did not confirm the presence of a high relief bedrock ridge between Production Well CW6 and Bos Creek as described by previous investigations (Weston, 1985 and RMT, Geraghty & Miller, 1987);
- Glacial outwash deposits fill the Wisconsin River Valley in the vicinity of the City well field, forming a terrace which has a maximum elevation of approximately 1230 feet MSL;
- The aquifer in the vicinity of the City well field appears wedge shaped in cross-section and ranges in thickness from 0 to 140 feet;
- The ancestral Wisconsin River bedrock valley narrows toward the north generally resulting in deposition of coarser sand and gravel sediments;
- The majority of the City well field is underlain by undifferentiated fine to coarse sand deposits. However, a relatively continuous sequence of fine sand overlying a thin gravel appears to extend beneath the central portion of the study area;
- Several fill areas exist along the Wisconsin River including the former City landfill which occupies a sand and gravel pit directly south of the Marathon Electric Assembly building, Schofield Park, beneath Wergin Construction and the river front area between Lemke Cheese and Lake Wausau Granite;
- Groundwater flow in the vicinity of the City Well Field is strongly influenced by: bedrock topography, soil heterogeneities, production well pumpage, stream and river elevations, and the stream and river bed hydraulic resistance;
- The radius of influence of the West Well Field at the water table extends at least as far south as Bos Creek and may have extended further south prior to Production Well CW6 being pumped to waste into the creek. The zone of influence at the base of the aquifer may presently extend considerably further south, possibly encompassing the northern portion of the former City of Wausau landfill;



- The cone of depression from the East Well Field extends across the Wisconsin River, resulting in groundwater flow from the vicinity of the west side landfill towards Well CW3:
- The hydraulic conductivity tests appear to be affected by well installation techniques as well as the geologic materials. The hydraulic conductivity values determined from the baildown tests range from  $1.73 \times 10^{-4}$  cm/s at Monitoring Well C4D to  $8.17 \times 10^{-2}$  at Monitoring Well E22. The average hydraulic conductivity of aquifer materials not influenced by drilling fluids is estimated by the baildown tests to be  $3 \times 10^{-2}$  cm/s;
- Relatively high concentrations of TCE were detected at soil gas stations SG105, SG121, SG123, SG124, SG125, SG141 and SG142 all of which appear to be located within or directly adjacent to the former City landfill;
- High concentrations of PCE and TCE (4080 and 244 ug/L, respectively) were detected from soil gas samples obtained from the south side of Wausau Chemical (SG57) near the location where 900 gallons of PCE was released in December, 1983. The PCE soil gas distribution appears to be preferentially elongated toward the east-northeast;
- Elevated concentrations of PCE were also detected from soil gas samples collected near the northwest loading dock of Wausau Chemical. A documented PCE release of approximately 200 gallons occurred in this area in February, 1983.
- The distribution of TCE in the aquifer south of Production Well CW6 appears to indicate two sources of contamination. The TCE plume in the deeper portion of the aquifer appears to originate in the vicinity of the former City landfill, located south of the Marathon Electric Assembly building. The shallow TCE plume appears to result from contaminated water from Production Well CW6 being pumped to waste into Bos Creek.
- The relatively continuous concentrations of TCE observed in Production Well CW3 since early 1982, appear to be the result of TCE migration from the area of the former City landfill, located on the west side of the Wisconsin River. The plume appears to have migrated under the river and into Well CW3.
- The distribution of total chlorinated ethenes at the water table, in the vicinity of the East Well Field indicate two chemically distinct contaminant plumes. The difference in chemistry and lateral extent of these plumes suggest either multiple sources or multiple releases from the same source.



Based on the results of the preliminary modeling the following observations and conclusions can be made about groundwater flow and contaminant migration in the vicinity of the City of Wausau municipal wells:

- A single layer finite-difference groundwater flow model can be used to accurately simulate most flow conditions in the study area.
- Preliminary calibration of the model indicates that river bed hydraulic conductivity and aquifer hydraulic conductivity are the primary input parameters affecting simulated heads.
- Preliminary modeling indicates a groundwater divide exists between the West Well Field (Wells CW6, CW7 and CW9) and the East Well Field (CW3 and CW4). The divide appears to bisect the former City of Wausau landfill.
- The two-dimensional groundwater flow model indicates that the zone of influence around the West Well Field extends south to the northern portion of the former City of Wausau landfill.
- Preliminary contaminant transport modeling indicates a source at the northern portion of the former City of Wausau landfill will result in contaminants reaching City Well CW3 in approximately 5 years and City Well CW6 in approximately 6 years.
- Discharge of water from well CW6 to Bos Creek creates a small groundwater mound which could potentially form a barrier between a contaminant source at the landfill and the West Well Field.
- Additional work is needed on the flow and transport models in the vicinity of Bos Creek to accurately simulate heads at Well R2D and Well CW4 to more accurately simulate flow and transport.



### VI. RECOMMENDATIONS FOR PHASE II WORK

Based on information obtained, several data gaps were identified during Phase I. The following additional work is recommended during the Phase II investigation:

- Repair Monitoring Well WC-1 so that groundwater samples may be collected during the Phases II investigation. This well is necessary to evaluate the effectiveness of the Wausau Chemical extraction system.
- Perform volatile compound analyses on all thirty (30) monitoring wells installed during the Phase I investigation and approximately forty (40) selected pre-existing wells to obtain a second round of water quality results;
- Obtain and perform target compound list (TCL) analyses on approximately twenty (20) groundwater samples from suspected contamination source areas:
- Perform soil borings at potential source areas located at Wausau Chemical, C.M. St. P. & P. Railroad right-of-way, Wausau Energy, Marathon Electric, and the former City of Wausau landfill;
- Submit soil and groundwater samples from these borings for VOC and TCL analyses;
- Perform approximately 8 test pits in the former City landfill and obtain approximately 20 soil/refuse samples for analysis of TCL parameters. The test pits will be used to characterize the type and extent of waste disposed in the landfill in order to evaluate potential health risks;
- Perform soil gas extraction tests at the former City landfill and at the former Wausau Chemical bulk solvent storage area to evaluate the potential effect of soil vapor extraction as a remedial action;
- Perform flow measurements on Bos Creek in order to assist the groundwater flow model calibration and evaluation of conditions ior to discharge of Well CW6 to Bos Creek. The flow measurements will also be useful in assessing potential health risks as a result of surface water exposure;
- Obtain surface water samples from Bos Creek during the spring and summer in order to evaluate seasonal influences on the VOC carrying capacity of the creek;
- Monitor groundwater levels during the spring and summer in order to assess seasonal influences on groundwater flow; and



• Continue groundwater flow and transport modeling through final calibration in order to evaluate contaminant transport under hydraulic conditions prior to existing monitoring data and to evaluate potential remedial actions during the Feasibility Study.

Recommendations for Phase II investigation will be presented in more detail in the Phase II Work Plan.



#### REFERENCES

- CH2M Hill, Central, February, 1986, Investigation of an Abandoned City of Wausau Landfill. Prepared for the Wisconsin Department of Natural Resources.
- Foth & Van Dyke and Associates, Inc., June, 1986, Infield Conditions Report on the Impact of Incidental Petroleum Spillage at the Wausau Energy Corporation Site. Prepared for Wausau Energy Corporation.

Foth & Van Dyke and Associates, Inc., December, 1986, VOC Groundwater Investigation at the Former Wausau Energy Facility in Wausau, Wisconsin. Prepared for Wausau Energy Corporation.

Geraghty & Miller, Inc. and RMT, Inc., 1987, Hydrogeological Investigation of the Alluvial Aquifer Beneath City Well 6, Wausau, Wisconsin, 54 pp.

Kendy, E., 1986, Hydrogeology of the Wisconsin River Valley in Marathon County, Wisconsin, 218 pp.

Kerfoot, H.B., J.A. Kohout and E.N. Amnick, 1986, Detection and Measurement of Groundwater Contamination by Soil-Gas Measurement Proc. Conf. Hazardous Wastes and Hazardous Materials, Hazardous Materials Control Research Institute, Silver Spring, Maryland, pp. 22-36.

LaBerge, G.L. and P.E. Myers, 1983, Precambrian Geology of Marathon County, Wisconsin: WGNHS Info. Circ., no. 45, 88 pp.

Mackay D. and Shiu W.Y., 1981, A Critical Review of Henry's Law Constants for Chemicals of Environmental Interest. Journal of Physical Chemistry Reference Data, V. 10, No. 4, pp. 1175-1199.

- Marrin, D.L. and G.M. Thompson, 1987, Gaseous Behavior of TCE Overlying a Contaminated Aquifer. Journal of Groundwater, V. 25, No. 1, pp. 21-27.
- Marrin, D.L. and G.M. Thompson, 1987, Soil Gas Contaminant Investigations: A Dynamic Approach. Groundwater Monitoring Review V. 8 No. 3, pp 88-93.
- Parsons, F., Wood, P.R. and DeMarco, J., 1984, Transformations of Tetrachloroethene and Trichloroethene in Microcosms and Groundwater, J. AWWA, February 1984, pp. 56-59.
- STS Consultants Ltd., July, 1984, Subsurface Exploration and Testing Program to Evaluate Groundwater Quality, Wausau Chemical Facilities, Wausau, Wisconsin.
- STS Consultants Ltd., April, 1985, Subsurface Exploration and Testing Program to Evaluate Groundwater Quality and Pre-Treatment Design Program at the Wausau Chemical Facility in Wausau, Wisconsin.


- STS Consultants Ltd., September, 1986, Wausau Chemical Corporation Groundwater Extraction Program Interim Report.
- STS Consultants Ltd., January, 1987, Wausau Chemical Corporation Groundwater Extraction Program Progress Report.
- Twin City Testing Inc., August, 1985, Existing Conditions Report and Exploration Program, Wausau East Municipal Well Field, Wausau, Wisconsin.
- Warzyn Engineering Inc., September 1987, Final Work Plan, Remedial Investigation/Feasibility Study, Wausau NPL Site, Wausau, Wisconsin.
- Warzyn Engineering Inc., September 1987, Final Quality Assurance Project Plan, Remedial Investigation Feasibility Study, Wausau NPL Site, Wausau, Wisconsin.
- Warzyn Engineering Inc. 1987, Industrial Survey, Wausau Water Supply NPL Site.
- Weston, Inc., 1985, Hydrogeological Investigation of Volatile Organic Contamination in Wausau, Wisconsin, Municipal Wells: A report prepared for the U.S. Environmental Protection Agency by Weston-Sper Tech. Asst. Team, Region V, 66 pp.
- Wisconsin Department of Natural Resources, (WDNR) 1982, Industrial Survey of Marathon Electric.

CSR/kam/KJQ/DLI/RWM [kam-600-50]



-

# VOLATILE ORGANIC COMPOUND RETENTION ORDER

# Photo Ionization Detector

<u>Parameter</u>	<b>Retention Time</b>
1,1-Dichloroethene	4.24
Trans-1,2-Dichloroethene	4.98
Trichloroethene	7.23
Benzene	7.39
Tetrachloroethene	9,86
Toluene	10.81
Ethyl Benzene	13.84

# Hall Detector

<u>Parameter</u>	<u>Retention Time</u>
Methylene Chloride	3.26
1,1-Dichloroethene	4,29
1,1-Dichlorothane	4.77
Trans-1,2-Dichloroethene	5.04
Chloroform	5.21
1,2-Dichloroethane	5.49
1,1,1-Trichloroethane	6.12
Bromodichloromethane	6.40
Trichloroethene	7,29
Chlorodibromomethane	7.58
Bromoform	8.76
Tetrachloroethene	9.91

13076.28 TEM/kam/CSR [kam-600-50j]

.

?

# SOIL GAS ANALYSIS DETECTION LIMITS

Compound	<u>Replicates</u>	<u>Mean(ng)</u>	<u>Deviation</u>	<u>Detection Limit(ng/L)</u>
Toluene	3	4.16	0.044	1000
1,1-Dichloroethene	3	5.06	0.086	1000
Trans-1,2-Dichloroeth	ene 3	4.95	0.021	1000
Trichloroethene	3	4.91	0.032	1000
Tetrachloroethene	3	4.21	0.219	1000
1,1,1-Trichloroethane	3	3.90	0.147	1000
Benzene	3	7.57	0.085	1000
Ethyl Benzene	3	6.08	0.301	1000
1,1-Dichloroethane	3	3.99	0.216	1000
Chloroform	3	4.02	0.132	1000
Methylene Chloride	3	3.65	0.788	1000
1,2-Dichloroethane	3	2.92	0.099	1000
Bromodichloromethane	3	4.92	0.093	1000
Chlorodibromomethane	3	8.77	0.180	2000
Bromoform	3	8.95	0.118	2000

13076.28 TEM/kam/CSR [kam-600-50k]

.

•

### TARGET VOC DETECTION LIMITS FOR WATER HEADSPACE

Compound	<u>Replicates</u>	<u>Mean</u> (1)	Standard <u>Deviation</u>	Method <u>Detection Limit</u> (2)
Toluene	7	2.49	0.208	0.65 ug/L
1,1-Dichloroethene	7	2.32	0.364	1.14 ug/L
Trans-1,2-Dichloroethene	7	2.08	0.332	1.04 ug/L
Trichloroethene	7	1.84	0.294	0.92 ug/L
Tetrachloroethene	7	2.38	0.310	0.97 ug/L

(1) Mean value for spike at 3 ug/L.

(2) Calculated D.L. according to Appendix A of EPA Test Methods for Organic Chemical Analysis of Municipal and Industrial Wastewater.

13076.28 TEM/kam/CSR [kam-600-501]

•

.

.

.

# OTHER VOC'S DETECTION LIMITS FOR WATER HEADSPACE

Compound	Replicates	Detection Limits
Benzene	3	2.0 ug/L
Ethyl Benzene	3	2.0 ug/L
1,1,1-Trichloroethene	3	1.0 ug/L
1,1-Dichloroethane	3	2.0 ug/L
Chloroform	3	2.0 ug/L
Methylene Chloride	3	5.0 ug/L
1,2-Dichloroethane	3	5.0 ug/L
Bromodichloromethane	- 3	5.0 ug/L
Chlorodibromomethane	3	25 ug/L
Bromoform	3	50 ug/L

.

13076.28 TEM/kam/CSR [kam-600-50m]

..

### SURFACE WATER SAMPLE LOCATIONS WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

.

<u>Station</u>	<u>Date</u>	Location
SW01	10-14-87	Bos Creek Pond Outfall West of Third Ave
SW02	10-14-87	Bos Creek Pond North of Randolph Street
SW03	10-14-87	Bos Creek at Schofield Park
SW04	10-14-87	Bos Creek at Culvert North of Burns Street
SW05	10-14-87	CW6 Discharge at Bos Creek
SW06	10-19-87	Bos Creek Southwest of 425 Burns Street
SW07	10-19-87	Storm Sewer Discharge East of Marathon Electric
SW08	10-26-87	Storm Sewer Discharge to Bos Creek at Randolph Street
SW09*	10-28-87	CW6 Discharge at Bos Creek
SW10*	10-28-87	Bos Creek Pond North of Randolph Street
SW10 Dup	10-28-87	Bos Creek Pond North of Randolph Street
SW11	10-29-87	Storm Sewer East of Old Landfill

### <u>Notes</u>

.

\* Sample submitted to Contract Laboratory for GC/MS verification.

13076.28 CSR/kam/CSR [kam-600-50n]

•

# WELL LOCATION RATIONALE WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

WEST STUDY AREA

<u>Well ID</u>	Depth Drilled <u>(feet)</u>	<u>Rational</u>
W50	83	Monitor water quality and levels at intermediate depth at well nest R3S/R3D.
W51	41	Monitor groundwater quality and levels west (upgradient) of Marathon Electric.
W52*	152	Define vertical and lateral extent of groundwater impact along suspected groundwater transport route to Production Well CW6.
W52A*	36	Monitor groundwater levels between former City landfill and Bos Creek.
W53*	171	Monitor water quality and levels at depth south of Marathon Electric at the former City landfill.
W53A*	41	Monitor shallow groundwater quality and water levels beneath the former City landfill.
W54*	87	Monitor water quality and levels within the northern portion of the former City landfill.
W55	130	Monitor groundwater quality and levels between Production Well CW6 and Marathon Electric, evaluate the existence of a buried bedrock ridge suggested by previous investigations.
W55A	43	Monitor water levels adjacent to Production Well CW6.
W56	66.5	Monitor deep water quality and levels adjacent to fill areas along Bos Creek.
W56A	20	Monitor shallow water quality and levels adjacent to fill areas along Bos Creek.
W57 TOTAL FOOTAGE	77.5	Monitor water quality at depth adjacent to MW-9, confirm existence of bedrock high.
DRILLED	° 948	

• . • •

	EAS.	TS	TUD	Y I	AREA
--	------	----	-----	-----	------

• •

<u>Well ID</u>	Depth Drilled <u>(feet)</u>	<u>Rational</u>
E20	80.5	Monitor water quality and levels at intermediate depth between WW1 and GM8D.
E21*	133	Monitor groundwater quality and levels between former City of Wausau landfill and Production Well CW3.
E21A*	22	Monitor groundwater levels adjacent to Monitoring Well E21 and the Wisconsin River.
<b>E22</b>	96.5	Monitor groundwater quality and levels at depth at Wausau Energy.
E22A	22	Monitor shallow groundwater quality and levels at Wausau Energy.
E23A	21.5	Monitor shallow groundwater quality and levels north of Marathon Press.
E24	85.7	Monitor deep groundwater quality and levels at Marathon Box, east of Wausau Chemical.
E24A	35	Monitor shallow groundwater quality and levels at Marathon Box, east of Wausau Chemical.
E25	135	Monitor deep groundwater quality and levels southeast (upgradient) of Marathon Box.
E25A	37.5	Monitor shallow groundwater quality and levels southeast (upgradient) of Marathon Box.
E26	95	Monitor deep groundwater quality and levels between Wausau Chemical and Production Well CW3.
E26A	23	Monitor shallow water quality between Wausau Chemical and Production Well CW3.
E27*	136.5	Monitor deep water quality and levels between former City landfill and Production Well CW3.
E28A	37	Monitor water levels east of production wells to establish control on the flow system.
E29A	29	Monitor shallow groundwater quality and levels adjacent to GM5D, east of Production Well CW3.
E30*	133	Monitor deep water quality between former City landfill and Production Well CW3.

EAST STUDY AREA

•

<u>Well ID</u>	Depth Drilled <u>(feet)</u>	<u>Rational</u>
E31*	135.5	Monitor deep water quality between former City landfill and Production Well CW3.
E32*	14	Obtain groundwater and soil sample east of Wausau Chemical at railroad right of way.
E33*	14	Obtain groundwater and soil sample east of Wausau Chemical at railroad right of way.
E34*	14	Obtain groundwater and soil sample northeast of Wausau Chemical at railroad right of way.
E35*	20	Obtain groundwater and soil sample adjacent to Wergin Construction.
E36*	17.5	Obtain groundwater and soil sample adjacent to Marathon Press drum storage area.
E37*	26	Monitor groundwater quality in vicinity of soil gas detection at Marathon Press.
E38* TOTAL FOOTAGE	18	Obtain groundwater and soil sample from west side of Marathon Press north building.
DRILLED	1381.2	

\* Well or sampled boring location different from the location proposed in Work Plan.

13076.28 CSR/kam/CSR [kam-600-50d]

.

# CONTRACT LABORATORY SOIL SAMPLE ANALYSIS RATIONALE WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

Sample Number <u>boring-depth-round</u>	Analyzed <u>Parameters</u>	Rationale
WE-SW55A-35-01	VOCs, AB\N, grain size, natural organic content	Classify aquifer materials based on grain size and natural organic content. Determine if past migration of potentially contaminated groundwater had impacted aquifer materials.
WE-SE24-24-01	VOCs, AB\N, grain size, natural organic content	Analyze unsaturated zone soils to determine if groundwater impact in vicinity of W24A is the result of a source at Marathon Box.
WE-SSG18-01	VOCs, AB\N	Background surface soil sample
WE-SW57-10-01	VOCs, AB\N, grain size, natural organic content	Classify geologic materials, investigate possible fill materials adjacent to Bos Creek.
WE-SS01-01	VOCs, AB\N, grain size	Analyze unsaturated zone soils in the vicinity of potential VOC source area at Wausau Energy.
WE-SS02-01	VOCs, AB\N, grain size	Analyze unsaturated zone soil adjacent to an area where PCE was detected in soil gas samples (Camelot Cleaners).
WE-SS03-01 WE-SS03-90 (dup)	VOCs, AB\N, grain size	Analyze unsaturated zone soils in the vicinity of areas where TCE was detected in soil gas (former landfill).
WE-SE31-25-01	VOCs, AB\N, grain size	Classify geologic materials in the vicinity of CW3 and analyze unsaturated zone soils adjacent to C.M. St. P. & P. Railroad and Lemke Cheese.
WE-SW53A-20-01 WE-SW53A-40-01	VOCs, AB\N, grain size, natural organic content	Analyze soils beneath potential source area at former City Landfill.
WE-SW52-32-01	VOCs, AB\N, grain size, natural organic content	Analyze unsaturated zone soils at Marathon Electric.

# TABLE 7 (Continued)

•

.

Sample Number <u>boring-depth-round</u>	Analyzed <u>Parameters</u>	Rationale
WE-SS04-01	VOCs, AB\N, grain size, natural organic content	Analyze soils in the vicinity of a leachate seep from the former City landfill.
WE-SS05-01 WE-SS05-91 (dup)	VOCs, AB\N, grain size	Analyze unsaturated soils in the vicinity of the former Wausau Chemical Bulk Solvent storage area.
WE-SE26A-14-01	VOCs, AB\N, grain size, natural organic content	Analyze soils unsaturated zone soils beneath the north side of Wausau Chemical.
WE-SS06-01	VOCs, AB\N, grain size, natural organic content	Analyze surficial soils adjacent to leachate seep from former City landfill.
WE-SS07-01	VOCs, AB\N, grain size, natural organic content	Analyze surficial soils in the vicinity of the former Marathon Electric hazardous waste storage area.
WE-SW54-5-01 WE-SW54-5-91 (dup) WE-SW54-20-01 WE-SW54-30-01	VOCs, AB\N, grain size, natural organic content	Obtain depth integrated soil samples in the vicinity of soil gas stations indicating TCE at the former City landfill.
WE-SE21-31-01	VOCs, AB\N, grain size, natural organic content	Investigate geologic characteristics of soil samples immediately adjacent to Wisconsin River. Obtain shallow aquifer soil samples in vicinity of Lake Wausau Granite.
WE-SE32-10-14-01 WE-SE33-10-14-01 WE-SE34-10-14-01	VOCs, AB\N, grain size, natural organic content	Obtain vertically composited soil samples from potential source area at C.M. St. P. & P. Railroad right-of-way east of Wausau Chemical.
WE-SE35-16	VOCs, AB\N, grain size, natural organic content	Investigate potential source of PCE in vicinity of Monitoring Well GN9S at Wergin Construction Company.
WE-SE36-16 WE-SE37-16 WE-SE38-16	VOCs, AB\N, grain size, natural organic content	Analyze unsaturated zone soils in vicinity of soil gas detection areas (PCE) at Marathon Pres.
WE-SDSB-01	VOCs	Soil blank for VOCs.

.

13076.28 CSR/kam/CSR [kam-600-500]

•

### SURFACE WATER SAMPLE LOCATIONS WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

<u>Station</u>	<u>Date</u>	Location
•SW01 & SED01	12-09-87	East bank of the Wisconsin River, west of East Wausau Avenue;
•SW02 & SED02	12-09-87	East bank of the Wisconsin River, approximately 700 feet south of East Wausau Avenue;
•SW03 & SED03	12-09-87	West bank of the Wisconsin River east of the southeast corner of the Marathon Electric assembly building;
•SW04 & SED04	12-09-87	West bank of the Wisconsin river, due east of monitoring wells C4S and C4D;
•SW05 & SED05	12-09-87	North side of Bos Creek ponded area adjacent to Monitoring Well R2S, R2D;
•SW06 & SED06	12-09-87	Mouth of Bos Creek, approximately 40 feet south of boat launch at Schofield Park;
•SW07 & SED07	12-09-87	Bos Creek at Burns Street, upstream of well CW6 discharge;

13076.28 CSR/kam/CSR [kam-600-50e]

•

### VERTICAL GRADIENTS GROUNDWATER FLOW WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

	'		Vertical	
Well No	<u>est</u>	<u>Date</u>	Gradient	Direction
		West Well	Field	
C4S, C4	4D	01-08-88	2.6 E-04	Down
C2S, R4	4D	01-08-88	3.1 E-04	Down
W53, W	53A	12-10-88	2.3 E-04	Down
R1S, R1	1D	01-08-88	2.2 E-03	Down
R2S, R2	2D	01-08-88	6.1 E-03	Down
R3S, R3	SD	01-08-88	8.4 E-03	Down
W52, W5	52A	01-08-88	4.1 E-03	Down
W55, W5	55A	01-08-88	3.2 E-03	Down
W9, W57	7	01-08-88	1.9 E-03	Down
GM4S, G	GM4D	01-08-88	2.8 E-04	Up
W3A, W3	3B	01-08-88	4.6 E-04	Down
W4A, W4	4C	01-08-88	0	
			Vertical	
<u>Well Ne</u>	<u>est</u>	Date	Gradient	<b>Direction</b>
		East Well	Field	
E21, E2	21A	01-07-88	4.5 E-04	Up
TCT44	F30	01_07_88	8 7 E_04	- <del>-</del>
		01-0/-00	0./ L-U4	υp
E29A, (	GM5D	01-07-88	6.7 E-03	Up
E25A, E	25	01-07-88	3.0 E-04	Up

WC3B, WC3 01-07-88 6.4 E-04 Up WC7A, MW9A 01-07-88 9.9 E-04 Up E24, E24A 01-07-88 7.2 E-04 Up . WW1, E20 01-07-88 5.9 E-04 Up E26, E26A 01-07-88 6.4 E-04 Down

13076.28 CSR/kam/KJD [kam-600-50p]

### SUMMARY OF HYDRAULIC CONDUCTIVITY TESTS WAUSAU WATER SUPPLY NPL SITE

<u>Well #</u>	Method	Drilling (cm/sec)	Hydraulic Conductivity <u>Difference</u>	Average	Percent <u>Error</u>
C4S C4D	HSA RB/DM No Case	0.137 x 10-1 0.173 x 10-3			
R3S R3D	HSA RRA	0.680 x 10-1 0.858 x 10-2			
W55A	. HSA	0.189 x 10-2			
W55 W55 Rep	RB/DM RB/DM	0.699 x 10-2 0.692 x 10-2	7.0 x 10 <sup>-4</sup>	6.99 x 10-2	1%
E24A E24	HSA RB/DM	0.290 x 10-1 0.252 x 10-1			
C2S	HSA	0.430 x 10-1			
E20 E20 Rep	RB/DM No Case RB/DM No Case	0.170 x 10-2 0.208 x 10-2	3.8 x 10 <sup>-4</sup>	1.94 x 10-2	20%
E22	RB/DM	0.812 x 10-1			
E25	RB/DM	0.302 x 10-1			
E30	RB/DM No Case	0.144 x 10-2			
MW9A	RB/DM	0.456 x 10-1			·
R2D	RRA/Casing	0.657 x 10-2			
W51A	HSA	0.103 x 10-1			
W56	RB/DM No Case	0.159 x 10-2			
W50 W50 Rep	RB/DM RB/DM	0.413 x 10-1 0.475 x 10-1	6.2 x 10 <sup>-3</sup>	0.444 × 10 <sup>-1</sup>	14%
Notès		<i>و</i> ا ا	• ¥		

# Notes

RB/DM No Case - Rotary boring, drilling mud used to support borehole RB/DM - Rotary boring, drilling mud with casing advanced HSA - Hollow stem auger RRA - Reverse air rotary

13076.28 CSR/kam/KJS [kam-600-50q]

.

# HENRY'S LAW CONSTANTS FOR SOME COMMON INDUSTRIAL SOLVENTS AT 25 C AS DETERMINED BY THE METHOD DESCRIBED IN MACKAY AND SHIU (1981) AFTER MARRIN AND THOMPSON (1987)

	Henry's Law Constant*	
trans-1,2-dichloroethylene	0.67	
Methylene chloride	0.26	
1,1,1-trichloroethane (TCA)	2.80	
Trichloroethylene (TCE)	1.18	
Carbon tetrachloride	1.59	
Tetrachloroethylene (PCE)	2.30	
Chloroform	0.38	
1,1,2-trichlorotrifluoroethane (F-113)	15.00	
n-hexane	170.00	
Toluene	0.67	
* Henry's law constants are given in units of	of kPa.M <sup>3</sup> /mol	

13076.28 CSR/kam/CSR [kam-600-50f]

.

### COMPARISON OF CONTRACT LABORATORY VS. FIELD GC RESULTS WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

.

	WARZYN	CLP
<u>Locations</u>	Total Chlorinated Ethenes ug/L	Total Chlorinated Ethenes ug/L
E21-132 Dup	1,98	3
E21-132	1,98	2
E24-40	1,43	3.8
E25-120	0	0.7
E25-154	0	0
E30-100	Ō	Õ
E32-Comp	6.51	7.6
E32-14	963.5	1450
E33-14	380.17	470
E34-14	73.5	60.6
E35-18	8200	5700
E36-16	20.88	22
E38-18	0	30
W52-100	30	34.7
W53-125	2038	1979
W54-85	54.8	80
W53-75	1532.3	1335.9
W55-60	1.36	0
W55-70	0	0
W55-80	0	0
W57-21	0	0
W55 Complete	4320	3200
SW09	152	82
SW10	87.1	70
W56-50	. 0	1
CW4	15.22	18.2
W55A	29.98	32.4
SB01	2.58	3
SB02	0	0
SB03	0	5

Refer to Drawing 13076-All for graphic comparison of field GC vs. Contract Lab Analyses.

.

13076.28 MCB/kam/CSR [kam-600-50g]

.

.

•

### CROSS INDEX OF EXISTING WELL DESIGNATIONS WAUSAU WATER SUPPLY NPL SITE WAUSAU, WISCONSIN

Well Identification Code Appearing On Log	Well Identification Code Appearing <u>In This Report</u>	Well Identification Code Appearing On Log	Well Identification Code Appearing <u>In This Report</u>
	WEST_ST	UDY AREA	
R1D	Same	WMW-1A	MW1A
R2D	Same	WMW-2A	MW2A
R3D	Same	WMW-3A	MW3A
R4D	Same	WMW-3B	MW3B
City Well #6	CW6	WMW-4A	MW4A
City Well #7	CW7	WMW-4B	MW4B
City Well #9	CW9	WMW-4C	MW4C
15	C1S	WMW-5	MW5
B-2S	C2S	WMW-6	MW6
B-3S	C3S	WMW-7	MW7
B-4S	C4S	WMW-9	MW9
4D	C4D	GM-1S	GM1S
B-6D	C6S	GM-2S	GM2S
B-7S	C7S	GM-3S	GM3S
		GM-4S	GM4S
		GM-4D	GM4D

# EAST STUDY AREA

.B1	WC1	MW11 (EPA 11)	MW11
B2	WC2	MW12 (EPA 12)	MW12
B3	WC3	MW13 (EPA 13)	MW13
B3A	WC3A	MW14 (EPA 14)	MW14
B3B	WC3B	TCT40	Same
		•	

TABLE 13 (Continued)

Well Identification	Well Identification	Well Identification	Well Identification
Code Appearing	Code Appearing	Code Appearing	Code Appearing
<u>In This Report</u>		In This Report	
B3C	WC3C	TCT41	Same
<b>B4</b>	WC4	TCT42	Same
B4B	WC4B	TCT42	Same
B5	WC5	TCT44	Same
B5A	WC5A	FVD1	Same
B6	WC6	FVD2	Same
B6A	WC6A	FVD5	Same
B7	WC7	FVD7	Same
B7A	WC7A	GM5D	Same
MW1	WW1	GM6D	Same
MW2	WW2	GM7D	Same
MW3	WW3	GM8D	Same
MW4	WW4	GM9S	Same
MW5 "	WW5	Wergin	Same
MW6	WW6	City Well #3	CW3
MW7	WW7 .	City Well #4	CW4
MW7A (EPA 7A)	MW7A		
MW8	Same		
WGS9	Same		
MW9A	Same		
WGS10	Same		
MW10A (EPA 10A	) MW10A		

13076.28 CSR/kam/CSR [kam-600-50h]

MW10B (EPA 10B)

MW10B

.

· · •





# APPENDIX A

. . . . .

# FIELD METHODS FOR EXPLORATION AND SOIL SAMPLING

•. •

.

### FIELD METHODS for EXPLORATION AND SAMPLING SOILS

### A. Boring Procedures Between Samples

The bore hole is extended downward, between samples, by a continuous flight auger, driven and washed-out casing, or rotary boring with drilling mud or water.

### B. Standard Penetration Test and Split-Barrel Sampling of Soils (ASTM\* Designation: D 1586)

This method consists of driving a 2" outside diameter split barrel sampler using a 140 pound weight falling freely through a distance of 30 inches. The sampler is first seated 6" into the material to be sampled and then driven 12". The number of blows required to drive the sampler the final 12" is recorded on the log of borings and known as the Standard Penetration Resistance. Recovered samples are first classified as to texture by the driller. Later, in the laboratory the driller's classification is reviewed by a soils engineer who examines each sample.

#### <u>C. Thin-walled Tube Sampling of Soils (ASTM\* Designation: D 1587)</u>

This method consists of forcing a 2" or 3" outside diameter thin wall tube by hydraulic or other means into soils, usually cohesive types. Relatively undisturbed samples are recovered.

### D. Soil Investigation and Sampling by Auger Borings (ASTM\* Designation: D 1452)

This method consists of augering a hole and removing representative soil samples from the auger flight or bucket at 5'0" intervals or with each change in the substrata. Relatively disturbed samples are obtained and its use is therefore limited to situations where it is satisfactory to determine approximate subsurface profile.

### E. Diamond Core Drilling for Site Investigation (ASTM\* Designation: D 2113)

This method consists of advancing a hole in hard strata by rotating downward a single tube or double tube core barrel equipped with a cutting bit. Diamond, tungsten carbide, or other cutting agents may be used for the bit. Wash water is used to remove the cuttings. Normally a 2" 0.D. by 1 3/8" I.D. coring bit is used unless otherwise noted. The rock or hard material recovered within the core barrel is examined in the field and laboratory. Cores are stored in partitioned boxes and the length of recovered material is expressed as a percentage of the actual distance penetrated.

\*American Society for Testing and Materials, Philadelphia, Pennsylvania

# LOG OF TEST BORING



**General Notes** 

# **Descriptive Soil Classification**

### **GRAIN SIZE TERMINOLOGY**

Soil Fraction	Particle Size	U.S. Standard Sieve Size
Boulders	Larger than 12"	Larger than 12"
Cobbles	3" to 12"	3" to 12"
Gravel: Coarse	34" to 3"	3⁄4" to 3"
Fine	4.76 mm to ¾″	#4 to 3⁄4"
Sand: Coarse	2.00 mm to 4.76 mm	#10 to #4
Medium	0.42 mm to 2.00 mm	#40 to #10
Fine	0.074 mm to 0.42 mm	#200 to #40
Silt	0.005 mm to 0.074 mm	Smaller than #200
Clay	Smaller than 0.005 mm	Smaller than #200

Plasticity characteristics differentiate between silt and clay.

#### GENERAL TERMINOLOGY

Physical Characteristics Color, moisture, grain shape, fineness, etc. Major Constituents Clay, silt, sand, gravel Structure Laminated, varved, fibrous, stratified, cemented, fissured, etc. Geologic Origin Glacial, alluvial, eolian, residual, etc.

### **RELATIVE PROPORTIONS** OF COHESIONLESS SOILS

Proportional			Defining Range By												
Term								l	Pe	rC	er	Ita	ag	e	of Weight
Trace	•		•											•	0%- 5%
Little	•		•			•	•••			•					5%-12%
Some	•		•		 •	•									12%-35%
And .	•		•			•		•		•				•	35%-50%

### ORGANIC CONTENT BY COMBUSTION METHOD

Soil Description	Loss on Ignition
Non Organic	Less than 4%
Organic Silt/Clay	4-12%
Sedimentary Peat	12-50%
Fibrous and Woody Peat	. More than 50%

### **RELATIVE DENSITY**

.....

term t		value
Very Loose		0-4
Loose		4-10
Medium Dense		10-30
Dense		30-50
Very Dense	0	ver 50

#### CONSISTENCY

Term	q <sub>u</sub> -tons/sq. ft.
Very Soft	0.0 to 0.25
Soft	0.25 to 0.50
Medium	0.50 to 1.0
Stiff	1.0 to 2.0
Very Stiff	2.0 to 4.0
Hard	Over 4.0

### PLASTICITY

Term	Plastic Index
None to Slight	0-4
Slight	5-7
Medium	8-22
High to Very High	Over 22

The penetration resistance, N, is the summation of the number of blows required to effect two successive 6" pentrations of the 2" split-barrel sampler. The sampler is driven with a 140 lb. weight falling 30" and is seated to a depth of 6" before commencing the standard penetration test.

# Symbols

### DRILLING AND SAMPLING

CS-Continuous Sampling RC-Rock Coring: Size AW, BW, NW, 2" W **ROD-Rock Quality Designator RB**-Rock Bit FT-Fish Tail DC—Drove Casing C-Casing: Size 21/2", NW, 4", HW CW-Clear Water **DM**—Drilling Mud HSA-Hollow Stem Auger FA-Flight Auger **HA**—Hand Auger COA-Clean-Out Auger SS-2" Diameter Split-Barrel Sample 2ST-2" Diameter Thin-Walled Tube Sample 3ST-3" Diameter Thin-Walled Tube Sample PT-3" Diameter Piston Tube Sample AS-Auger Sample WS-Wash Sample PTS—Peat Sample **PS**—Pitcher Sample NR-No Recovery S-Sounding PMT-Borehole Pressuremeter Test VS—Vane Shear Test WPT-Water Pressure Test

### LABORATORY TESTS

q.-Penetrometer Reading, tons/sq. ft. q.-Unconfined Strength, tons/sq. ft. W-Moisture Content, % LL-Liquid Limit, % PL-Plastic Limit, % SL-Shrinkage Limit, % LI-Loss on Ignition, % D-Dry Unit Weight, Ibs./cu. ft. pH-Measure of Soil Alkalinity or Acidity FS-Free Swell, %

### WATER LEVEL MEASUREMENT

▽-Water Level at time shown NW-No Water Encountered WD-While Drilling BCR-Before Casing Removal ACR-After Casing Removal CW-Caved and Wet CM-Caved and Moist

Note: Water level measurements shown on the boring logs represent conditions at the time indicated and may not reflect static levels, especially in cohesive soils.



# UNIFIED SOIL CLASSIFICATION SYSTEM

#### **COARSE-GRAINED SOILS**

(More than half of material is larger than No. 200 seive size.)

	Clean Gra	vets (Little or no fines)
GRAVELS	GW	Well-graded gravels, gravel-sand mix- tures, little or no fines
More than half of coarse	GP	Poorly graded gravels, gravel-sand mix- tures, little or no fines
than No. 4	Gravels w	vith Fines (Appreciable amount of fines)
sieve size	GMu	Silty gravels, gravel-sand-silt mixtures
	GC	Clayey gravels, gravel-sand-clay mixtures
	Clean Sa	nds (Little or no fines)
	SW	Well-graded sands, gravelly sands, little or no fines
SANDS More than half of coarse	SP	Poorly graded sands, gravelly sands, little or no fines
fraction smaller than No. 4	Sands wi	th Fines (Appreciable amount of fines)
sieve size	SM u	Silty sands, sand-silt mixtures
	SC	Clayey sands, sand-clay mixtures

### **FINE-GRAINED SOILS**

(More than half of material is smaller than No. 200 sieve.)

SILTS	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity
AND CLAYS Liquid limit less than 50%	CL	Inorganic clays of low to medium plastici- ty, gravelly clays, sandy clays, silty clays, lean clays
	OL	Organic silts and organic silty clays of low plasticity
SILTS	мн	Inorganic silts, micaceous or diatoma- ceous fine sandy or silty soils, elastic silts
AND CLAYS Liquid limit greater than 50%	СН	Inorganic clays of high plasticity, fat clays
	ОН	Organic clays of medium to high plasticity, organic silts
HIGHLY ORGANIC SOILS	PT	Peat and other highly organic soils

### LABORATORY CLASSIFICATION CRITERIA

GW	$C_u = \frac{D_{so}}{D_{10}}$ greater than 4; $C_c =$	$\frac{(D_{10})^2}{D_{10}XD_{60}}$ between 1 and 3				
GP	Not meeting all gradation rec	uirements for GW				
GM	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are				
GC	Atterberg limits above "A" line with P.I. greater than 7	use of dual symbols				
sw	$C_u = \frac{D_{60}}{D_{10}}$ greater than 6; $C_c =$	$\frac{(D_{10})^2}{D_{10}XD_{60}}$ between 1 and 3				
SP	Not meeting all gradation rec	quirements for SW				
SM	Atterberg limits below "A" line or P.I. less than 4	Limits plotting in hatched zone with P.I. between 4 and 7 are borderline cases				
SC	Atterberg limits above "A" line with P.I. greater than 7					

#### PLASTICITY CHART



For classification of fine-grained soils and fine fraction of coarsegrained soils.

Atterberg Limits plotting in hatched area are borderline classifications requiring use of dual symbols.

Equation of A-line: PI = 0.73 (LL · 20)

# APPENDIX B BORING LOGS



WARZYN PERFORMED BORING LOGS

W			Y N		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva o	E ition 1307	- <b>20</b> 119 6.25	97.2
ENG	INEE	RINC	G INC.	F SCI	Location Wausau, Wisconsin	Sheet	1	of	2	
	SA	MPI	LE		VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES
Recove	ery " R=%	Moist	N Der	oth	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC
					Medium Dense to Very Dense Brown Fine to Coarse SAND, Little to Some Fine Gravel and Silt (SP)					<u>. wate</u>
1		Μ	34	5-				0.0		
2 .	12	M	113					0.0		
				10-						
3	12	W	<u>⊻</u> 54					0.0		-
				15-						
	E	W								
	0	¥¥		20-				0.0		51.9
5	6	W	13-	25-				0.0		
				70						
6	6	w	24					0.0		11.3
				35-						
				40						
While Upon Time Depth	Drill Com After to W	ing pletic Dril /ater	<u>vvAIE</u> <u>¥</u> 13.0 on of Dri ling	illin		Start Crew 0 Drillin 0-4 5'	<b>NER</b> 10/23/ Chief J g Meth	AL N 87 E W R od 3	IO I Ind10, ig I 1/4"	ES /27/8 D-50 HSA

W			Y N	,	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No e Eleva o	E ition 1307	- <b>20</b> 119 6.25	7.2	
ENG	INEE		G INC		Location Wausau, Wisconsin	Sheet         2         of         2           08)         273-0440				 	
$\geq$	SA	MPI	E	ONE SC	TENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	<u>50</u>		OPF	RT	IFS	
Recov	ery "	Moist	ure		VISUAL CLASSIFICATION	qu	Field		Mono-	Field	
No.		4	N	Depth		TSF	Soil	nnu		Wate	
				- - - - - - - - - - - - - - - - - - -	Medium Dense to Very Dense, Brown Fine to Coarse SAND, Little to Some Fine Gravel and Silt (SP)						
7	6	W	60	- -				0.0		NTD	
				- 50-							
8	3	W	42	- 55- - 55- - 60-	Grades Fine to Medium SAND, Little Silt,			0.0			
				- 65- - 70- - 75-	Trace Fine Graver near 64 (SF)						
9		W	54	-  - 80				0.0		ND	
				- 00 	End Boring at 80.5'						

. .

		Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. Surface Elevation Job No. 130				95.2
ENGINE	ERINO	G INC	c.	Location Wausau, Wisconsin	Sheet	et <u>1</u> of <u>4</u>			
<u> </u>	MD		-ONE SC	IENCE COURT + P.O. BOX 5385, MADISON, WIS. 53705 + TEL.(60	08) 273-044 <b>60</b>			DT	
Recovery "	Moist	ure		VISUAL CLASSIFICATION		Field		Mono-	Field
No. T	•	N	Depth -	Earth Drilled to 29'	TSF	Soil_			Wate
			- - - - - - - - - - - - - - - - - - -	FILL: Granite Cuttings Dense Brown Fine to Coarse SAND, Trace to Little Fine Gravel (SP) Visual Description based on Cuttings and Drilling Action					
1A 6	w	78					0.0		
1B 18	w	76	- - 30-				0.0		
			-	Contract Lab Soil Sample WE-SE21-31-01					
			- - - - - - - - - - - - - - - - - - -	Earth Drilled to 89'					
	<u> </u>	WA	TER	LEVEL OBSERVATIONS	GE	NER	L AL N	ΙΟΤ	ES
While Dri Upon Cor Time Afte Depth to Depth to	lling npletio er Dri Water Cave	<u>¥</u> 1 on of lling in	4.0 Drillin	ng ¥	Start Crew Drillin	11/11/ Chief M g Meth	/87 E /IK R nod RE	Endl 1 Lig B/DM	/14/8 0-13

.

	LOG OF TEST BORING	Boring	g No	E	-21	
	roject wausau, wi NPL Site RI/FS	Surfac	ce Eleva Io	ation 1307	119 76.25	25.Z
NGINEERING INC	ocation Wausau, Wisconsin	Sheet	Sheet of			
	CE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.((	508) 273-0440				
SAMPLE	VISUAL CLASSIFICATION	SO	IL PR	ROPE	ERT	IES
covery " Moisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Field VOC
	ine to Coarse SAND with Trace to Little ravel Based on Drilling Action and Cuttings arth Drilled to 89'		Soll			<u>Vate</u>



	YN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring Surfac Job N Sheet	g No e Eleva o	E ation 1307 of	- <b>21</b> 119 6.25	)5.2		
GINEERIN	NG INC.		(08) 2 <b>77</b> 0//	Sheet					
SAME		TENCE COURT • P.U. BUX 5365, MAUISUN, WIS. 55/05 • TEL.(							
very " Moi	sture	VISUAL CLASSIFICATION	qu	Field		Mono-	Fie		
TT ¥ ↓	N Depth	and Remarks	( )P.P.	VOC Soil	XNu	tox	VO Uat		
		Probable GRAVEL, Basd on Drilling Action		3011			_ Has		
		and Cuttings					1.		
		Drilling Action and Drilling Mud Color							
		Change							
	E								
		End Boring at 133'							
							ļ		
	- 140-						Ì		
	ΙE								
						ļ			
	- 145-					1			
	ΙE								
	- 150-								
	I E								
	E 155-								
					1				
					1				
	- 165								
	170-								

ł

	ZYN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	; No e Eleva o.	E- ition 1307	- <b>21/</b> 119 6.25	5.5
ENGINEER	RING INC.	Location Wausau, Wisconsin	Sheet	1	of	1	
SAN	<u>ONE S</u> /PLE	VISUAL CLASSIELCATION	508) 273-044 SO	IL PR	OPE	RT	IES
Recovery " R=%	loisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel
5. T ¥	V Depth	Earth Drilled to 22.0'. Visual description	TSF	_Soil			_Wate
		based on cuttings.					
		Reddish Brown SAND & GRAVEL with Chips of Granite (FILL)					
		·					
		Dense, Brown Fine to Coarse SAND, Trace to					
		Little Fine Gravel (SP) Visual Description based on Cuttings and Drilling Action					
		End Boring at 22'					
		· ·		i			
	- 35-						
hile Drilli		LEVEL OBSERVATIONS	Start	11/12/	<u>чь IN</u> 97 б		<u>53</u>
Jpon Comp	letion of Drilli	ng 🛓	Crew	Chief N	IK R	igCN	IE 7
Depth to Wa	Drilling		Drillin	g Meth	od <u>I</u>	ISA (	0-22
Depth to Ca	ve in						••••

W A R Z Y N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location	Boring Surfac Job N	Boring No. <b>E-22</b> Surface Elevation 119 Job No. 13076.25 Sheet 1 of 1				
ENGINEERING INC.	Location wausau, wisconsin	Sneet	<b>.</b>	01	<b>.</b>	······	
	SCIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL. (608	<u>3) 273-044</u>			-07		
Recovery " Moisture	VISUAL CLASSIFICATION	30	Field	UPE	Mono-	IE3 I Field	
	and Remarks	( )P.P. TSF	VOC	HNu	tox	VOC	
	Earth Drilled to 22.0' Refer to Boring Log E-22 for Soil Classification from 0-22.0' 5- 0- 5- 5- 5- 5- 5- 5- 5- 5- 5- 5- 5- 5- 5-						
WATI	R LEVEL OBSERVATIONS	GF	NFR			FS	
While Drilling Upon Completion of Dr Time After Drilling Depth to Water		Start Crew O Drillin	11/13/ Chief M g Meth	87 E 1K R od J	Indi 1 Lig CM	/13/8 /1E 75 0-22'	

WARZYN				LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. <b>E-22</b> Surface Elevation 1196.1					
ENGINEERING INC.				Location Wausau, Wisconsin	Sheet	Sheet         1         of         3				
				IENCE COURT • P.O. BOX 5385, MADISON, WIS. 53705 • TEL.(608						
Recovery " Moisture				VISUAL CLASSIFICATION and Remarks	qu Field Mono-F ()P.P. VOC HNU tox				Field	
NO.    ¥	+		Depth	FILL: Foundry Sand	TSF	Soil_			Water	
			-							
1 18	M	25	-	Medium Danse to Very Danse, Brown Fine to			0.0			
			- 5 -	Coarse SAND, Little to Some Fine Gravel,						
ť				Trace Silt (SP)	1	•				
2 18	M	30	-				0.0			
			- 10							
		F	-							
3 18	W	68	- 15-				0.0			
		F	-							
			_							
4 12	W	22	- 20-				0.0		12.2	
		þ	-							
5 12	м	23	_				0.0			
			- 25-				0.0			
		E	-							
			-							
		Ē	- 30-							
		Ē	-							
6 12	W	16	- 75				0.0		ND	
·    ·		F								
		E	-							
		Ē	- - 40-							
WATER LEVEL OBSERVATIONS						GENERAL NOTES				
While Drilling ¥         Upon Completion of Drilling ↓         Time After Drilling ↓         Depth to Water ↓						Start 10/12/87 End10/13/87 Crew Chief JW Rig D-50 Drilling Method FA 0-5'; RB/DM 5-95'				


		YN		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No. e Eleva o.	E ition 1307	- <b>22</b> 119 6.25	96.1
ENGINE		; INC.	NE SC	Location Wausau, Wisconsin	Sheet	3	of		
SA	MPL	.E			SO	IL PR	ROPERTIES		
Recovery " R=% No. T	Moist	N D	epth	and Remarks	qu ()P.P. TSF	Field VOC Soil	HNu	Mono- tox	Fie VOI Wate
			90	Medium Dense to Very Dense Brown Fine to Coarse SAND, Little to Some Fine Gravel, Trace Silt (SP)					
10 12	w		95				0.0		1
			100	End Boring at 96.5'					

		Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS		Boring Surfac Job N	g No. e Eleva	E- ation 1307	- <b>23/</b> 119 6.25	<b>A</b> 98.2
ENGINE	ERING	G INC		Location Wausau, Wisconsin		Sheet	1	of	1	
SA	MPL	.E		VISUAL CLASSIFICATION	SOIL PROPER					
	Moist	ure	Depth	and Remarks		qu ()P.P.	VOC	HNu	tox	V0
				Loose, Black Organic SILT (OL)		TSF	Soil			Wat
			-							
1 18	Μ	16		Stiff Reddish Brown Fine Sandy CLAY (CL)		(1.25)		0.2		
		_		Very Dense, Brown Medium to Coarse SAND, Little Fine Gravel, Trace Silt (SP)						
2 18	M	73	-							
			- 10 					0.2		
			-							
3 8	M/W	36	- ₩ 15-					0.2		
			-							
4 10	W	22	-					0.2		
			20 					0.2		41
			-	End Boring at 21.4'						
			- - 25-							
		-	-							
			-							
			-							
			- 35							
			-							
	Ĩ		- 							
	I.	WA	TER	LEVEL OBSERVATIONS		GE	NER/		<b>O</b> T	ES
While Dril Upon Con Time Afte	ling pletio r Dril	$\frac{1}{2}$ 14 on of ling	4.7 Drillin	ng ¥	Start         10/30/87         End10           Crew Chief         LE         RigCM           Drilling         Method         4				/30/ 1E 7 HS	

WAF	R Z Y	N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva	E- tion	<b>24</b> 120	9.0
			Location Wausau, Wisconsin	Job N Sheet	o 1 ·	1307 of	<u>6.25</u> 1	••••••
ENGINE	RING I	INC. ONE SC	I CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	)8) 273-044	.0			
SA	MPLE		VISUAL CLASSIFICATION	VISUAL CLASSIFICATION SOIL PRO				IES
Recovery "	Moisture		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Field VOC
No. T 🖌	*	N Depth	FILL: Sand and Gravel	TSF	Soil	0.4		Water
		-						
1 10								
1 12	M	30 <u></u> 5				0.4		
		- -						
2 0		E	Medium to Very Dense Press Fire to Current					
3 4	I	91-	SAND, Little to Some Fine Gravel, Trace Silt		<u> </u>	0.3		
		E <sup>-10-</sup>	(SP)		<u> </u>			
		E						I
4 0	M	47				0.3	·	·
					<u> </u>			
5 10	M	26						<u> </u>
		20-						
		E						
6 0	w	2217						
0 0		23 		ļ		0.4		
		-						
		- 30-						400.2
7 16	W	12 75				0.5		
			End Poring at 25'					
		-	End boring at 55					
					į			
	14							
White D-"	$\frac{\mathbf{V}}{\mathbf{V}}$		LEVEL UBSERVATIONS	<u> </u>				<u>ES</u>
Upon Con Time Afte	ung <u></u> pletion r Drillir	of Drilling	ng ¥	Start Crew Drillin	10/13/ Chief 1 g Meth	87 E LE R od <u>4</u>	nd10, ig Cl 1/4"	/13/8 ME 4: HSA

WAF	? Z `	ΥN	LOG OF TES	ST BORING	Boring	2 No.	Ε	-24	
			Project Wausau, W	I NPL Site RI/FS	Surfac	e Eleva	tion	120	98.5
			L operation Work		Job N	01	1307	6.25	
ENGINEE	RING	G INC.		au, wisconsin	Sheet	<b>H</b>	01		
<u> </u>	MDI		CIENCE COURT · P.O. BOX 5385, M	ADISON, WIS. 53705 • TEL.(6	08) 273-044			т	
Recovery "	Moist	ure	VISUAL CLAS	SIFICATION		Field		Mono-	IES Field
. R=%	4	N Dep	- and Re	marks	()P.P. TSF	VOC Soil	HNu	tox	VOC Water
			Refer to Boring Log E-24 Description and Classifica	A for Soil tion from 0-35.0'					
		. ا. ا. ا. ا. ا. ا.							
		<u>Mulalala</u>							
		ب ا ب ا ب ا ب ا	Medium Dense to Very D	ense, Brown Fine to					
		E	Coarse SAND, Little to So	ome Fine Gravel,					
1	w	32-	Trace Silt (SP)				00		1 43
		Ē					0.0		1.45
1 11	1	WATI	LEVEL OBSERVAT	IONS	GF	NFR	71 V	ОТ	FS
While Drill Jpon Com Fime Afte Depth to V Depth to C	ling ipletic r Dril Vater Cave i	<u>¥ 24.0</u> on of Dr lling n			Start Crew 0 Drillin 0-70'; 70-85	10/14/ Chief J g Meth 3 7/8"	87 E W R od 5 7 RB/1	Ind10 Lig 7/ <b>8</b> " DM	/19/8 D-50 RB/DI

W	AF	R Z Y	YN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva	E	- <b>24</b> 120	8.5			
				Location Wausau Wisconsin	Job No. 13076.25 Sheet 2 of 3							
ENG	INEE	RINC			511000	<i>#</i>		<i>S</i>				
	SA	MPI	F	1012HC2 COOK 7 F13: DOX 5335, MAD130N, W13: 55105 - 122.(000	SO		OP	=RT	IFS			
Recove	ery_"	Moist	ure		qu	Field		Mono	Field			
No. T	<b>⊼</b> -∞	•	N Depth	and Remarks	()P.P. TSF	VOC Soil	HNu	tox	VOC Water			
				Contract Lab Water Sample WE-GE24-40-01								
2	12		- 45	Coarse SAND, Little to Some Fine Gravel, Trace Silt (SP)								
2	12	••	/8- 				0.0					
									1.25			
		2										
3	12	w	46- 60-	-								
			- 65- - - -									
4	9	w							PMDT			
									BriDL			
			- 75-									
			- 80- 									
			- 85-									

. . .

		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No.         E-24           Surface Elevation         1208.5           Job No.         13076.25								
NGINEERING	INC.	Location Wausau, Wisconsin	Sheet <u>3</u> of <u>3</u>								
	ONE SC	IENCE COURT . P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(	608) 273-04	08) 273-0440							
SAMPL	E	VISUAL CLASSIFICATION	SOIL PROPERTIES								
ecovery " Moistu R=%	Ire	and Remarks	qu ()PP	Field	UN:	Mono-	Fie				
	N Depth		ISF	Soil	ninu.		Wate				
	-	End Boring at 85.7'									
	E										
	<u>-</u> 90-	*Medium Dense to Very Dense, Brown Fine									
	-	Trace Silt (SP)									
	E										
	E										
	- 95										
	E .										
	-										
	E 100-										
	Ē										
	E 105										
	Ē										
	<b>F</b>										
	E 110-										
	E I										
						Ì					
	- 115- -										
	E										
	- 120 -										
	E										
						ĺ					
	- 125-										
	 				[						
	ΕI					Í					
	E										
	- 130-										
	1 1										

. . • · ·

			LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva	E ation	- <b>25</b> 121	1.7	
ENGINEI	ERING IN	NC.	Location Wausau, Wisconsin	Job N Sheet	o1	1307 0f	6.25 4		
		ONE SC	CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(6	08) 273-044					
SA Recovery "	Moisture		VISUAL CLASSIFICATION		Field		Mono-	IES Field	
No. T ↓	↓ N	Depth	and Remarks	()P.P. ISF	VOC Soil	HNu	tox	VOC Water	
			Medium Dense to Very Dense, Brown Medium to Coarse SAND, Little Fine Gravel (SP)						
1 18	M 7	2		· · · · · · · · · · · · · · · · · · ·		0.2			
		5- 				0.2			
2 10	M 15							, 	
2 10		-10				0.2			
							ŕ		
3 12	M 14	4				0.6			
4 8	M 8	0	Grades to Trace Fine Gravel near 19'			03			
		20							
5 10	W 8								
		25	Grades to Little Fine Gravel near 25'			0.6		·	
			· ·					l	
6 0	7	1 	No Sample Recovery					BMD	
7 6	W 3	6 				0.4			
	W	<u>⊢ 40-</u> ATFR	LEVEL OBSERVATIONS	GF				FS	
While Dril Upon Con Time Afte	ling ¥ pletion o r Drilling	25.0 of Drillin		Start Crew Drillin	10/12/ Chief 1 g Meth	_ Start <u>10/12/87</u> Endl _ Crew Chief <u>LL</u> RigC Drilling Method <b>RB/D</b>			





W	A F	R Z	YN	7	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring	g No ce Eleva	E ation	- <b>25</b>	1.7			
						Job N	o.	1307	76.25				
ENGI	NEE	RING	g ing	с.	Location Wausau, Wisconsin	Sheet	4	of	4	•••••			
$\geq$	SV	MD		- ONE SC	TIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60								
Recover	Γ <u>Υ</u> "	Moist	ure	·	VISUAL CLASSIFICATION	qu Field Mono-							
No. T	R=%	↓ ↓	N	Depth	and Remarks	()P.P. TSF	VOC Soil	HNU	tox	VOC Wate			
					Probable 12" Gravel Layer near 130' Based on Drilling Action and Cuttings								
17	0		70							BM			
				135 	No Sample Recovery					DFU			
				E									
				- 140-									
				E	Very Dense, Reddish Brown Clayey GRAVEL								
18	1	W	130		Action)				<u> </u>				
	-			- 145-				<u> </u>					
				E									
					· · · · ·								
				-	WE-GE25-01								
	_			E									
9	1	Μ	192	- - 155-				0.2		BM			
					End Boring at 154'								
				Ē	Probable Bedrock at 154', based on split spoon								
					color change.								
				165 									
				170									
				- 175-									

WAI	RZYN	J	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring	g No e Eleva	E- ation	<b>25</b> / 121	<b>4</b> 1.7
			Location Wausau. Wisconsin	Job N Sheet	o1	1307 of	6.25 1	
	ERING IN	NC.	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	08) <u>273</u> -044	40			
SA	MPLE		VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES
Recovery "	Moisture		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel
		-   -   -   -   -   -   -   -   -   -	Earth Drilled to 37.5' Refer to Boring Log E-25 for Description and Classification from 0-37.5'					
			End Boring at 27.5'					
While Dril Upon Con Time Afte Depth to V	lling ¥ npletion o er Drilling Water	<b>A I EK</b> 27.9 f Drillir <u>1/4 1</u> _27.3		GENERAL NOTE Start 10/22/87 End10/2 Crew Chief LL RigCM Drilling Method 4 1/4" 0-37.5'				ES /22/8 1E 75 HS/

W	AF	R Z	Y N	-	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva	E	- <b>26</b>	6.7
ENG	INE	ERIN	G IN	с.	Location Wausau, Wisconsin	Job N Sheet	o1	1307 	6.25 3	
$\geq$				-ONE SC	TIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	08) 273-044	40		· · · ·	
	SA	MP	LE		VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recov	ery." R=%	Moist		-	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Field VOC
NO.	<u> </u>	<b>*</b>	N	рерти -	Farth Drilled to 33.5' Refer to Boring Log	TSF	Soil			Wate
	ĺ			-	E-26A for Soil Description and Classification					
				Ē	from 0-33.5'			]		
				E						
				⊢ 5-						
				E						
				<b>F</b>						
			1	E						
				E 10-						
				- "						
		<u>ب</u>	1 1	-						
ļ				<u> </u>						
				E 15-	· · · · · · · · · · · · · · · · · · ·					
				<u>-</u> .						
				-						
Ì				- 20-						
				-						
				-						
				-						•
				25						
				-						
				-						
				-			1			
1				- 30-						
				-						
				_						
1		w	22	-						
	ļļ	•••		- 35-	Medium Dense, Brown Fine GRAVEL, Little		_			ND
					Medium Sand (GP)					
				_						
				-				i		
[				<u>ــــــــــــــــــــــــــــــــــــ</u>						
<u>I</u> .			W/A		LEVEL OBSERVATIONS					
W/1- :1 -		1:					INCRA			<u>5</u>
Unon		nng Inletio	<u>늘</u> on of	Drillir		Start	11/9/8	17 E	nd 11	/9/87
Time	Afte	r Dri	lling		*0 =	Drillin	g Meth	od 37	.ıg∪‼ //8" 1	1E / 5
Depth	n to V	Vater				0-96'				
Depth	n to C	Cave i	in							

	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	; No e Eleva o	DO Ition 1307	<b>T 2</b> 119 6.25	M 6.8		
GINEERING INC.	Location Wausau, Wisconsin	Sheet3 of3						
SAMPLE	VISUAL CLASSIFICATION	SOIL PROPERTIES						
Very " Moisture R=%	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel		
v v v v v ocpui 90- 90- 95- 100- 100- 100- 100- 100- 110-	Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987		Soil			Wat		



.W			YN		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	; No e Eleva 0	DO tion 1307	<b>T</b> 3 120 6.25	M 7.9	
ENG	INEE		G INC.		Location Wausau, Wisconsin	Sheet	2	of			
>	SA	MPI	.E	DNE SC	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	SOIL PROPERT					
Recov	very " R=% च	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel	
8	14	W		- - -	Firm, Brown Fine to Coarse SAND, Trace Gravel (SP)		Soil			Wat	
9	12	w	26	- 45 - -							
10	12	W	32-	- 50							
				- 55 - - - 60	End Boring at 52' Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987						
			بلابل بابابا بابا	- - - 65							
			باباباباباباباب	· 70 · · · 75							
				80							





	R Z	YN	-	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau Wissersia	Boring Surfac Job N	g No e Eleva o	DO ation 1307	T 4 118 6.25	Γ 4Μ 1187.8 5.25 3			
	ERINO	g ing	C.   - ONE SC	TENCE COURT - D.O. ROY 5385 MAD 1504 U15 53705 - TEL 44	.   Sneet		01 .	<b></b>				
SA	MP	LE		VISUAL CLASSIFICATION	UAL CLASSIFICATION SOIL PROPERT				IES			
Recovery " R=% No. [T]	Moist	ure N	Depth	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC			
				Dense, Brown Fine to Medium SAND (SP)	TSF	Soil			Wat			
15 24	W	31	- 90- 			· · · · ·						
			- - - - - 95-									
			1.1.1.									
16 24	w	65	100 100									
			- 105 - 105 - 110 - 110 - 1115 - 1115 - 120 - 125 - 125	Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987								

WAR			LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring Surfac Job N Sheet	g No e Eleva o	DO ition 1307	T 5 118 6.25	M 7.8	
ENGINE	RING INC	. I ONE SC	TENCE COURT - P.O. BOX 5385 MADISON WIS 53705 - TEL (60	B) 273-044		01	<b>#</b>		
SA	MPLE		VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	ES	
Recovery " R=%	Moisture	and Remarks		qu ()P.P.	Field VOC	Field Mono- VOC HNU tox	Mono- tox	Field	
1 24	W 1		WATER						
		- 5	Brownish Gray Organic SILT (OL)						
2 24	W 2-	-	Gray and Black Alternating Layers of Fine Silty SAND and PEAT, Trace Wood (SM-PT)						
3 24	W 8	- - 10	Firm, Gray SAND & GRAVEL, Trace Silt,						
4 18	W 20-	-	Some Organics (SP)						
		- 15 - 20 - 20 - 25 - 30 - 35 - 35  - 40	Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987						
I I	WA	TER	LEVEL OBSERVATIONS	GE	NERA	AL N	ΟΤΈ	S	
While Dril Upon Com Time Afte Depth to V	While Drilling        ↓         Ipon Completion of Drilling        ↓         ime After Drilling       ↓         imeth to Water       ↓					14 Er M Ri od	nd 9/1 ig	18/84 VII	



		YN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	No. e Eleva	E ation 1307	- <b>26</b> 119 6.25	6.7		
ENGINE	ERINO	GINC.	Location Wausau, Wisconsin	Sheet <u>3</u> of <u>3</u>						
SA	MPL	.E		SOIL PROPERTIES						
Recovery " R=%	Moist	ure N Depth	and Remarks	qu ()P.P. TSE	Field VOC Soil	HNu	Mono- tox	Fiel VOC		
		- - - - - - - - - - - - - - - - - - -	Very Dense Brown Fine to Coarse SAND, Trace to Little Fine Gravel, Trace Silt (SP)							
5	W									

			Y N		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring Surfac Job N Sheet	g No. e Eleva o. 1	E- ition 1307 of	- <b>26/</b> 119 6.25 1	<b>4</b> 96.6
$\geq$			0	NE SC	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(608	3) 273-044	) 273-0440			
/	SA	MPl	.Е		VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recove	ery " R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNU	Mono- tox	Fiel VOC
NO. 1	•			epth	Medium Dense to Very Dense, Brown Fine to Coarse SAND, Little to Some Gravel (SP)	TSF	<u>Soil</u>			Wate
1		М	34-	5						
2		М	53- -	10	Collected Contract Lab Soil Sample from 11.5 to 14' WE-SE26A-14-01					
3		W	24- -	15—						
4		w		20	Loose Brown Fine GRAVEL, Little Medium					
				25	Sand (GP) End Boring at 23'		1			
				35						
[										EC
While Upon Time Depth	Drill Com Afte to V	ling pletic r Dril Vater	∑ on of D lling	Drillin		Start Crew Drillin 0-23'	11/6/9 Chief 1 Ig Meth	87 E PD F od 4	End 11 RigCN 1/4"	LS /6/8 /IE 7: ' HS/

WAI		N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No.         E-27           Surface Elevation         1196.3           Job No.         13076.25						
ENGINEI	ERING I	NC.	Location Wausau, Wisconsin	Sheet   373-044	1	of .	4			
SA	MPLE		VISUAL CLASSIFICATION	SO	IL PR	OPE		IES		
Recovery :: R=%		l Depth	and Remarks	()P.P.	VOC	HNu	tox			
		$ \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$	Earth Drilled to 89' Approximately 15' of Granitic Fill Based on Drilling Action and Cuttings (FILL) Fine to Coarse SAND with Some Gravel (Based on Drilling Action and Cuttings) (SP)							
	WATER		LEVEL OBSERVATIONS	GF	NER	AL N	ЮТ	ES		
While Dri Upon Con Time After Depth to	lling ¥ npletion er Drillin Water	12.0 of Drillin g		_ Start 11/30/87 Endl1 _ Crew Chief JW Rig _ Drilling Method <b>RB</b> / 0-139.5'				/30/ D-50 DM		

WARZYN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No.         E-27           Surface Elevation         1196.3           Job No.         13076.25						
NGINEERING INC.	Location Wausau, Wisconsin	Sheet		of	4			
ONE	SCIENCE COURT • P.O. BOX 5385, MADISON, WIS. 53705 • TEL.(	608) 273-044	0			$\equiv$		
SAMPLE	VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES		
R=%	and Remarks	qu ()P.P.	VOC	HNu	tox	VO		
	Earth Drilled to 89' Fine to Coarse SAND with Some Gravel (Based on Drilling Action and Cuttings)							



			LOG OF TEST BORING	Boring	g No	E	-27				
			Project Wausau, WI NPL Site RI/FS	Surfac   Job N	e Eleva 0.	tion 1307	119 6.25	96.3			
GINEE	RING	INC.	Location Wausau, Wisconsin	Sheet	4	of	4				
<u>ج</u>			SCIENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(6								
	Moist	. <b>L</b> ire	VISUAL CLASSIFICATION		Field		Mono-	Fiel			
Ţ ↓	_ <b>↓</b> _[	N Dept	h and Remarks	()P.P. TSF	VOC Soil	HNu	tox	VO Wat			
			GRAVEL (GP) Drove Stone								
		- 13	Drilling Mud Color Change to Dark Baddish								
			Brown at 135' Probable Weathered Bedrock								
		Ē 14						532			
			End Boring at 139.5'								
		Ē	· ·								
		- 14 -	·								
		-			-						
		- 15									
		Ē									
		- 15 -	· · · · · · · · · · · · · · · · · · ·								
		Ē									
		-									
		<u> </u>									
		E									
		-									
		- E''									
		Ē									
	·										
11 1			רי יק								

W A I	RZYI ERING IN	NC.	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring Surfac Job N Sheet	g No. ce Eleva o. 1	E- ation 1307 of	28/ 121 6.25 1	2.1
SA	MPLE	UNE SU	VICLES CLARCES ACTION	SO		OPE	RT	IES
Recovery "	Moisture		and Remarks		Field		Mono-	Field
No. T	V N	Depth -	8" TOPSOIL	TSF	Soil	0.3		
		Ē	Medium Dense to Danse Provin Fine to Coarse					
1 14	M 4		SAND, Little to Some Fine Gravel, Little Silt					
-			(SP)			0.4		
		Ē						
2 12	M 2	4						
						0.3		
3 0		7				 		
			No Sample Recovery			0.3		
		E						
4 5	M							
		20-				0.3		
		Ē						
5 5	M· 4	5						
		25-				0.3		
		<b>≚</b> . -					2	
		- 30-						
		-						
6 3	W 1	7						
<b>P</b>						0.3		<u> </u>
			End Boring at 37'					
		- 40-						
	<u> </u>	ATER	LEVEL OBSERVATIONS	GE	NER	<u>al N</u>		ES
While Dri Upon Con Time Afte Depth to	lling <u>≚</u> npletion c er Drilling Water	27.8 of Drillin 3	ng ¥	Start Crew Drillir 0-37'	10/13/ Chief I ng Meth	87 E LE R lod 4	nd10 igCN 1/4"	/13/8 1E 45 HSA

		N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surface Job No	No. e Eleva	<b>E</b> - ation 1307	<b>29A</b> 120 6.25	0.8
ENGINEI	ERING I	NC.	Location Wausau, Wisconsin	Sheet	1	of	1	
SA	MPLE	ONE SC	VISUAL CLASSIFICATION	SOI	L PR	OPE	RTI	ES
Recovery " R=%	Moisture	Depth	and Remarks	qu ()P.P.	Field VOC	HNU	Mono- tox	Field VOC
			Loose, Brown Organic SILT (OL) (Topsoil) FILL: Sand, Fine Gravel and Clay					_mare
1 6	М	7- 7- 						
2 6	M		Very Dense to Medium Dense, Brown Medium to Coarse SAND, Little to Some Fine to Coarse Gravel (SP)					
~ 0	171							
3 2	M/W 10	6"	Split Spoon Refusal due to Probable 12" Coarse Gravel Layer near 15.0'					
4 4	W 4	17¥ 						
5	W 2	21 21 						
			End Boring at 29'					
		- - - - - - - - - - - - - - - - - - -						
	W	ATER	LEVEL OBSERVATIONS	GE	NER/	AL N	ΟΤΙ	ES
While Dril Upon Con Time Afte Depth to V	lling <u>¥</u> apletion o er Drillin; Water	19.1 of Drillin g	ng ¥	Start Crew C Drilling 0-29'	10/23/ Chief 1 g Meth	87 Ei LE R iod 4	nd10/ igCM 1/4"	23/1 E 7: HS

W		₹Z`	Y N.		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No ce Eleva co.	E ation 1307	- <b>30</b> 120 6.25	)2.1
ENG	INEE		G INC	.	Location Wausau, Wisconsin	Sheet	1	of	4	
$\geq$	SΔ	MPI	F	-UNE SC	TENCE COURT - P.O. BUX 5365, MAUISON, WIS. 53705 - TEL.(60	<u>8) 2/3-04</u>			:PT	IFS
Recove		Moist	ure		VISUAL CLASSIFICATION		Field		Mono-	Fie
No. T	R=% ↓	ł	N	Depth	and Remarks	()P.P. TSF	VOC Soil	HNu	tox	V( Wat
					Sand, Gravel and Fragments of Granite (FILL)					
1	18	М	40	-				0.0	1	
				- 5-	Dense to Very Dense Fine to Coarse SAND with GRAVEL (SP-GP)			0.0		
2	4	M	100-	-						
<b>-</b>			<del>/6</del> "	- 10-				0.0		
				-						
3	12	Μ	99	-				0.0		
				- 15-						
				-						
4		м	32	-						
	<u> </u>	141	52	<b>⊈</b> 20	Madium to Vary Dance Brown Fire to			0.0		
				-	Medium to Very Dense, Brown Fine to Medium SAND, Trace to Little Fine Gravel, Trace Silt (SP)					
5	12	M/W	53	-				0.0		ВМ
				- 25- -						
				-						
				-				-		
				- 30-						
				-						
				-						
				-						
				- 35-						
			F	_			1			
		w		-						
U 1	12	•••	12	- 40-				0.0		NI
<u>I_</u>	WATER LEVEL OBSERVATIONS						NER		ЮТ	ES
While Upon Time	Drill Com Afte	ling pletic r Dril	$\overline{\underline{2}}$ 20 on of lling	).0 Drillir		Start Crew Drillin	10/28/ Chief J ng Meth	87 E IW R	ig FA	 /30/ D-5( 0-4'

ENGINE		Y N		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring Surfac Job N Sheet	g No. e Eleva o. 2	E ution 1307 	- <b>30</b> 120 6.25 4	2.1
		ONE	e sc	IENCE COURT . P.O. BOX 5385, MADISON, WIS. 53705 . TEL.(6	08) 273-044	0			$\equiv$
Bacavary		. <b>L</b>		VISUAL CLASSIFICATION	SO		OPE	:RI	ES
Recovery R=X	Moist	N Dep	oth	and Remarks	()P.P. TSF	VOC Soil	HNU	tox	VOC Wate
7 8 8 6	W		45 50 55 60 70 75	Medium to Very Dense, Brown Fine to Coarse SAND, Trace to Little Fine Gravel, Trace Silt (SP) Medium Dense to Very Dense Brown Fine to Medium SAND, Trace Fine Gravel, Trace Silt (SP)			0.0		N
9 8	w		80	·			0.0		N



N		R Z	Y N	-	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Borin Surfa	g No ce Eleva lo.	E ation 1307	- <b>30</b> 120 76.25	)2.1
ENC	GINEI	ERIN	G IN	c.	Location Wausau, Wisconsin	Sheet	4	of	4	
$\geq$	SA	MP	LE	- ONE SC	VISUAL CLASSIELCATION	508) 273-04 SC	40 <u></u> 0IL PR	OP	ERT	IES
Reco	very " R=%	Moist		Donth	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC
<u>.</u>	<u>'                                    </u>	*	/18"	- -	Very Dense, SAND & GRAVEL (SP-GP)	TSF	Soil			Wate
15	0	w	150					10		6.6
			/12"					1.0		0.0
				- 135-	End Boring at 134.0'					
	ļ									
				- - 140						
				E						
				-						
				- 145- -						
				-						
				- 150-						
				<u> </u>						
				- 155-						
				-						
				-						
				160 						
				-						
				-						
				- 165-						
				-						
				Ξ						
				-						
				- 170-						
				-						
				-						
				- 175-						

• •

W A R Z	YN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. <b>E-31</b> Surface Elevation 1201.6 Job No. 13076 25				
ENGINEERIN	NG INC.	Location Wausau, Wisconsin	Sheet	1	of		
SAM		VISUAL CLASSIFICATION	SO	<u></u> IL PR	OPE	ERT	IES
Recovery " Moi R=%	sture	and Remarks	qu ()P P	Field	HNU	Mono-	Fiel
No. T 🖌 🕴	N Depth		ISF	Soil			Wate
1 M		FILL. Sand and Graver					
2 M	10-						
3 M	100 						
4 M	60 20-						
5 W	86 25-	Contract Lab Soil Sample obtained at 25', WE-SE31-25					
		Medium Dense to Very Dense, Brown Medium to Coarse SAND, Little to Some Gravel, Trace Silt (SP)					ſ
6 W	21						
	40-						
While Drilling Upon Complet Time After Dr	GENERAL NOTES Start 11/2/87 End 11/3/8 Crew Chief LE RigCME 75 Drilling Method3 7/8" RB/D						



W A I	R Z Y	Ń N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No.         E-31           Surface Elevation         1201.6           Job No.         13076.25           Sheet         3         of					
ENGINE	ERING	INC.	Location Wausau, Wisconsin						
			VISUAL CLASSIEICATION						
Recovery " R=%	Moistu	re N Depth	and Remarks	qu ( )P.P.	Field VOC	HNu to	no-Field x VOC		
10	W	145 90-	Medium Dense to Very Dense, Brown Medium to Coarse SAND, Little to Some Gravel, Trace Silt (SP)				ND		
		-   -   -   -   -   -   -			1				
11	w	80					ND_		
		- - - - - - - -	Medium Dense to Very Dense, Brown Fine to Medium SAND, Trace Gravel (SP)						
12	W	92 					ND		
		- - - - - - - - - - - - - - - - - -							
13	W	86 120-					ND		
		- - - - - - - - - - - - - - -							
14	W	97	Very Dense GRAVEL with Sand (GP)				ND		

-

W	AF	R Z	YN	-	LOG OF TEST BORING Boring No. E-31						
					Project Wausau, WI NPL Site RI/FS	Surface Elevation <u>1201.6</u> Job No. <u>13076.25</u>					
ENG	INE	ERINO	G IN	с.	Location Wausau, Wisconsin	Sheet	4	of	4		
$\geq$				- ONE SC	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(60	8) 273-044	.0				
Recov					VISUAL CLASSIFICATION	SOIL PROPERTIES					
10.	-`ƙ=% ī]↓	J	N	Depth	and Remarks	()P.P. TSF	VOC Soil	HNU	tox	VOC Wate	
				<u>.</u>							
	1										
15		W	100	<b>_</b> •	Probable Bedrock at 135' (Based on Drilling					4	
			<del>  /2"</del>		Action and Split Spoon Refusal)						
Í					End Boring at 136'						
				- 140-							
				- 145-							
				-   -							
				-							
				E							
				- 155-							
				E							
				- 160-							
				-							
				E							
				L 165							
	.			<u> </u>							
				El							
				E							
			ł	- 170 -			i				
				- 175							
W		RZY	YN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	3 No e Eleva o	E ation 1307	- <b>32</b> /6.25			
-------------------------------	---	-------	---	--	---------------------------	----------------------	---	----------------------	------	--	---------------------------------------
ENG	INE	RINC	GINC.	Location Wausau, Wisconsin							
	SA	MPL	.E	VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES		
Recov	ery " R=%	Moist	ure	and Remarks	qu ()P.P.	Field	HNU	Mono- tox	Fiel		
			N     Depth       -     -	Earth Drilled to 14', Visual Description based on Cuttings FILL: Reddish Brown Sand and Gravel Contract Lab Soil Sample obtained from 10-14'; WE-SE32-14-01 Contract Lab Groundwater Sample obtained at 14' WE-GE32-14-01 End Boring at 14'		Soil			963.		
1	1						<u> </u> ^   ^		EC.		
While Upor Time Dept	ile Drilling on Completine After Di pth to Wate		vvAIEK LEVEL C         e Drilling ¥         a Completion of Drilling ↓         After Drilling ↓         h to Water ↓				GENERAL NO Start 11/12/87 End1 Crew Chief MK RigC Drilling Method 4 1/4 0-14'				<u>E3</u> /12/3 ME 7: '' HS.

.

	τ Ζ Υ	N	LOG OF TEST BORING	Boring	g No	E	-33	
			Project Wausau, WI NPL Site RI/FS	Surfac   Job N	e Eleva 0.	ition 1307	6.25	
▼ ENGINEE	RING I	NC.	Location Wausau, Wisconsin	Sheet	1	of	1	
<u> </u>		ONE SC	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(6	508) 273-044	0			=
SA	MPLE		VISUAL CLASSIFICATION	SO		OPE		IES
R=%		N Depth	and Remarks	( )P.P.	VOC	HNu	tox	VOC
			Earth Drilled to 14'. Visual Description based on Cuttings		5011			Hate
			FILL: Reddish Brown Sand and Gravel					
		- 5-						
		- 10- -	Contract Lab Soil Sample obtained at 10' to 14' WE-SE33-14-01					
			Groundwater Sample obtained at 14' WE-GE33-14-01					380.0
			End Boring at 14'					
		- - - 20-						
		- - 25-						
		- - 35-						
		- - 40-						
	N	<b>ATER</b>	LEVEL OBSERVATIONS	GE	NER	AL N	IOT	ES
While Dril Upon Con Fime Afte Depth to V	ling <u>¥</u> pletion r Drillin Water	of Drillir	ng ¥	Start Crew Drillin 0-14'	11/12/ Chief M g Meth	87 E 4K F 10d 4	Endl 1 RigCN 1/4"	/12/8 AE 75 ' HSA

	7		Surfac	e Eleva	tion		
	INC.	Location Wausau, Wisconsin	Job N Sheet	o1	<u>1307</u> 	6.25 1	
	ONE S	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(6	08) 273-044	.0			
MPL	.E	VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES
Moistu	ire N. I. Dooth	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel
		Earth Drilled to 14'. Visual Description based on Cuttings	TSF	<u>Soil</u>			Wate
	E	FILL: Reddish Brown Sand and Gravel					
	- 5-						
	Ē						
	- 10-	Contract Lab Soil Sample obtained from					
	Ē	10-14', WE-SE33-14-01					
		WE-GE34-14-01					73
	- 15-	End Boring at 14'				•	
	E ·						
	<u> </u>						1
	-						
	- 25-						
	Ē						
	- 30 -						
	- 35-						
		LEVEL OBSERVATIONS					
$\frac{VATER LEVEL OBSERVATIONS}{Ile Drilling}$				11/12/ Chief <u>N</u> g Meth	<u>87</u> E 1K R 0d 4	ndl1/ igCN 1/4"	<u>=3</u> /12/ IE 7 HS
	ling 5 ppletio r Drill Vater Cave in	N Depth N Depth - 5 - 5 - 10 - 10-	N       Depth       and Remarks         Image: Second state of the sec	Noiscure       and Remarks       Q P.P. () P.P. ISP         Image: Noiscure       Image: Noiscure <td>N       Depth       and Remarks       (1)</td> <td>Noisture     and Remarks     (1)       ↓     N     Depth     and Remarks     (1)       ↓     N     Depth     Earth Drilled to 14'. Visual Description based on Cuttings     (1)       FILL: Reddish Brown Sand and Gravel     FILL: Reddish Brown Sand and Gravel     (1)     (1)       ↓     0     Contract Lab Soil Sample obtained from 10-14', WE-SE33-14-01 Groundwater Sample obtained at 14'     (1)       ↓     WE-GE34-14-01     (1)     (1)       ↓     15     End Boring at 14'       ↓     20-       ↓     20-       ↓     20-       ↓     (1)   <td>No bepth       and Remarks       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       FILL: Reddish Brown Sand and Gravel       Fill.       (P)       (P)       (P)       (P)         ↓       □       10-       Contract Lab Soil Sample obtained from 10-14', WE-SE33-14-01       (P)       (P)</td></td>	N       Depth       and Remarks       (1)	Noisture     and Remarks     (1)       ↓     N     Depth     and Remarks     (1)       ↓     N     Depth     Earth Drilled to 14'. Visual Description based on Cuttings     (1)       FILL: Reddish Brown Sand and Gravel     FILL: Reddish Brown Sand and Gravel     (1)     (1)       ↓     0     Contract Lab Soil Sample obtained from 10-14', WE-SE33-14-01 Groundwater Sample obtained at 14'     (1)       ↓     WE-GE34-14-01     (1)     (1)       ↓     15     End Boring at 14'       ↓     20-       ↓     20-       ↓     20-       ↓     (1) <td>No bepth       and Remarks       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       FILL: Reddish Brown Sand and Gravel       Fill.       (P)       (P)       (P)       (P)         ↓       □       10-       Contract Lab Soil Sample obtained from 10-14', WE-SE33-14-01       (P)       (P)</td>	No bepth       and Remarks       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       N       bepth       Earth Drilled to 14'. Visual Description based on Cuttings       (P)       Pick       We for         ↓       FILL: Reddish Brown Sand and Gravel       Fill.       (P)       (P)       (P)       (P)         ↓       □       10-       Contract Lab Soil Sample obtained from 10-14', WE-SE33-14-01       (P)       (P)

•

WARZYN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No ce Eleva o	E ation 1307	- <b>35</b>	
ENGINEERING INC.	Location Wausau, Wisconsin	Sheet	1	of	1	
	CIENCE COURT • P.O. BOX 5385, MADISON, WIS. 53705 • TEL.(6	08) 273-044	40			=
SAMPLE	VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recovery " Moisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC
	Earth Drilled to 20'. Visual Description based on Cuttings Brown Sand, Gravel and Cobbles (FILL) Contract Lab Soil Sample taken from 13.0 to 16.0', WE-SE35-16-01 Contract Lab Groundwater Sample obtained at 18', WE-GE35-18-01 End Boring at 20'	TSF	Soil			<u>Wate</u> 8200.
While Drilling Upon Completion of Drillin Time After Drilling		GE Start Crew Drillin 0-20'	<b>NER</b> 11/12/ Chief M ng Meth	<b>AL N</b> 87 E 1K R 10d 4	IOT ndl 1 ig CN 1/4"	ES /12/8 /12 /5 / HSA

W A	R Z Y I	N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring	g No e Eleva	E ation	-36	
			Location Wansan Wisconsin	Job N	0 1	1307	6.25 1	
ENGINE	ERING II	NC.   	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(6)	08) 273-044	<del>.</del>			
SA	MPLE		VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recovery "	Moisture		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel
			Earth Drilled to 17.5'. Visual Description based on Cuttings. Brown Sand and Gravel Contract Lab Soil Sample obtained from 10-13', WE-SE36-13-01 Contract Lab Groundwater Sample obtained at 16', WE-GE36-16-01 End Boring at 17.5'	TSF	<u>Soll</u>			20.
	<u> </u>	ATER	LEVEL OBSERVATIONS	GE	NER		ΙΟΤ	ES
While Dri Upon Con Time Afte Depth to	lling ¥ npletion o er Drilling Water	of Drillir g	ng ¥					/12/3 AE 7: ' HS/

WARZYN	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	; No e Eleva 0	E ation 1307	- <b>37</b> 119 6.25	8,3
ENGINEERING INC.	Location Wausau, Wisconsin	Sheet	1	of	1	
ONE	SCIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(	608) 273-044	.0			=
SAMPLE	VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recovery " Moisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC
	Earth Drilled to 26.0°. Visual Description based on Cuttings Brown SAND and GRAVEL Contract Lab Soil Sample obtained from 14-16', WE-SE37-16-01 End Boring at 26'					
40	-					
WATE While Drilling ¥ Upon Completion of Drill Time After Drilling Depth to Water		GE Start Crew ( Drillin 0-26'	NER/ 11/12/ Chief M g Meth	ALN 87 E 41K R aod 4	IOT Indi 1 ig CM 1/4"	ES /12/8 1E 75 HSA

A W	RZYN		LOG OF TEST BORING	Boring	g No	E	-38	
			Project Wausau, WI NPL Site RI/FS	Surfac	e Eleva 0.	tion 1307	6.25	
ENGINE	ERING IN	NC.	Location Wausau, Wisconsin	Sheet	1	of	1	
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		-ONE SC	IENCE COURT . P.O. BOX 5385, MADISON, WIS. 53705 . TEL.(60	08) 273-044 SO			DT	
Recovery "	Moisture		VISUAL CLASSIFICATION		Field		Mono-	Field
			Earth Drilled to 18.0'. Visual Description Based on Cuttings Brown SAND and GRAVEL Contract Lab Soil Sample obtained from 14-16', WE-SE38-16-01 Contract Lab Groundwater Sample obtained at 18', WE-GE38-18-01 End Boring at 18'	TSF	Soil			BMD
While Dri Upon Cor Time Afte	Water Water Water Water	- 35- - 35- - 40- ATER		, Start Crew Drillin	<b>NER</b> 11/13/ Chief M g Meth	<b>AL N</b> 87 E 11K R 10d 4	IOT ndl1 ligCN 1/4"	ES /13/8 /E 75 ' HSA

		Y N	,	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No e Eleva o	M ation 1307	<b>/-5(</b> 121 /6.25	)  3,3
ENGINE	<b>▼</b> ERING	INC	•	Location Wausau, Wisconsin	Sheet	1	of	3	
<u> </u>	RZYN       LOG OF TEST BORIN         Project       Wausau, WI NPL Site         Location       Wausau, Wisconsi         ONE SCIENCE COURT - P.O. BOX 5385, MaDISON, WIS. 5         MPLE       VISUAL CLASSIFICAT and Remarks         M 75       5         M 75       5         M 31       10         M 31       10         M 31       10         M 31       10         M 50       15         Grades to Coarse Sand near 15'         M 53       20         M 67       25         M 67       25         Grades to Coarse Sand near 15'         Grades More Coarse and More Dense         W 22       35         Grades More Coarse and More Dense         W 22       35         Grades More Coarse and More Dense         W 22       35         Hedium Dense       10 <th>CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(6</th> <th>08) 273-044</th> <th></th> <th></th> <th>DT</th> <th></th>	CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(6	08) 273-044			DT			
Recovery "	Moistu	ure		VISUAL CLASSIFICATION		Field		Mono-	Field
No. T	<u>  ↓ [</u>	N	Depth		()P.P. ISF	VOC Soil	HNU	tox	VOC Water
		Ē	-						
		- 75		FILL: Sand, Gravel and Clay				ļ	
1 12	IVI	E		Medium Dones to Very Dones Brown Medium					 
			- - - -	to Coarse SAND, Little to Some Fine Gravel (SP)					
2 8	M	31	- 10				1.2	1	
			- 10-						
			-						
3 8	M	50	- 15				0.0	1	
				Grades to Coarse Sand near 15'					
		F	-						
4 4	М	53-	- 20-				0.0		
		Ę	_						
		F	-						
5 4	M/W	67	_ Z 25_				0.0		
			- - - 30	Medium Dense, Brown, Fine to Coarse SAND, Trace Silt (SP)					
			_	Grades More Coarse and More Dense					
6 5	W	22							50.8
·			- 55-						
		Ē	_						
		Ę	-						
L	ι <u> </u> ,	WΔ.		LEVEL OBSERVATIONS					FC
While Dri Upon Con Time Afte	lling pletio r Drill	<u>¥ 25</u> n of i ling	.0 Drillir		Start Crew Drillin	10/26/ Chief I g Meth	87 E E R od R	igCN B/DN	/27/8 1E 750 1 0-85



	Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No. e Eleva o.	<b>W</b> ation 1307	<b>/ - 50</b> 121 6.25	3.3
ENGINEERING INC.	Location Wausau, Wisconsin	Sheet	3	of	3	
	CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(4	608) 273-044	.0 0.	0.00		$\equiv$
SAMPLE	VISUAL CLASSIFICATION	SO		OPE		IES
R=% N Depth	and Remarks	()P.P. TSE	VOC	HNu	tox	VOC
	End Boring at 85'	TSF	Soil			Water

. . .

A W	RZ	YN		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No. e Eleva	W ation 1307	- <b>51</b> 122 6.25	<b>A</b> !2.2
ENGINE	ERING	F INC.		Location Wausau, Wisconsin	Sheet	1	of		
S	AMPI	.E		VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
Recovery R=2	K Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fie VO
NO. 1 ¥			- -	Dark Brown Organic SILT (Topsoil) (OL) Loose to Medium Dense, Brown Fine to Coarse SAND, Little to Some Gravel, Trace	TSF	Soil			Wat
1 14	M	22	5	Silt (SP)			0.3		
2 9	M	9	10				0.0		
3 8	M	7	15						
4 12	M		20-						
5 0									
			25				0.1		
			30						
6 10	w								
			35			. <u></u>	0.0		
			40	LEVEL OBSERVATIONS	GE	NFR			FC
While Dr Upon Co Time Aft	illing mpletio ter Dril	¥ 34.2 on of Di ling	rilling		Start Crew Drillin	10/15/ Chief I g Meth	87 E E R od 4	nd10 ligCN 1/4"	/15/ 1E 4 / HS

	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No. e Eleva	W- ation 13076	51A 1222.2 25
ENGINEERING INC.	Location Wausau, Wisconsin	Sheet		of	
SAMPLE	VICLAL CLACCICATION	508) 273-044 SO	IL PR	OPE	RTIES
Recovery " Moisture R=% I N Depth	and Remarks	qu ()P.P.	Field VOC	HNU 1	ono-Fiel
7 20 W 26	Loose to Medium Dense, Brown Fine to Coarse SAND, Little to Some Gravel, Trace Silt (SP)		Soil	0.0	Wat
	End Boring at 45'				

W	A F		Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Borin Surfac	g No ce Elev	V ation 130'	V-5 12 76.25	<b>2</b> 16.5	
ENG	INEE		G INC	C.	Location Wausau, Wisconsin	in Sheet of					
	SA	MPL	.E		VISUAL CLASSIFICATION	SC	DIL PR	ROP	ERT	IES	
Recove	ery " , R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNU	tox	Fie VC	
NO. 1	*		N		Gray to Brown Sandy SILT (Topsoil)	TSF	Soil			Wat	
				-							
	12	м	21	-	Medium to Very Dense, Brown Medium to			-			
	12		- 21	- 5-	Coarse SAND, Trace Gravel (SP)			0.0	+		
				-							
				-							
2	12	M	39	10					+		
									+	+	
3	12	м	30						<u> </u>	<u> </u>	
				15 				0.0	-	<u> </u>	
4	4	M	83		Very Dense, Brown Fine to Coarse SAND and	ļ		<u> </u>			
				20	GRAVEL (SP-GP)			0.0			
				-							
				-	Dense to Very Dense, Brown Fine to Coarse						
<b>&gt;</b>	6	M	72	 25	SAND, Trace to Little Fine Gravel, Trace Silt			0.0			
				_	(SP)						
				-							
6A	6	M	23	-							
6P	12			- 30- -				0.0	<u> </u>	ļ	
פט	12			-	Contract Lab Soil Sample obtained at 32.0'.			0.0			
6C	8				WE-SW52-32-01			0.0		1	
·	<b>∮</b> →			- 35-				0.0	+		
				-							
7	8	M	31	-				0.0	+		
				- 40-	· · · · · · · · · · · · · · · · · · ·						
			WA	TER	LEVEL OBSERVATIONS	GE	<b>NER</b>		TOV	ES	
While Upon Time	Vhile Drilling Jpon Completion of Drilling Gime After Drilling					Start Crew Drillin	11/2/ Chief	87 ] MP ]	Endl 1 Rig <b>C</b> 4 1/4	/10 ante " HS	
Upon Time Depth Depth	pon Completion of Drilling					Crew Drillin 0-5', 5-152	Chief ng Metl 5 7/8"	MP I hod 4 RB/I	Rig C 4 1/4 DM	an "	



W	A R	Z	Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No ce Eleva	N ation	<b>/-5</b> 2 12	<b>2</b> 16.5
ENGI	NEE	RINO	G INC		Location Wausau, Wisconsin	Sheet	3	of	<u>9.45</u>	······
	SA	MPI	LE	- UNE 30	VISIAL CLASSIEICATION	SO		OPE	ERT	IES
Recover	y " R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNU	Mono- tox	Field
12	6	• • •	79		Medium to Very Dense, Brown Fine to Coarse		Soit			Wate
				- 90- 	SAND, Little Silt (SP)			0.0		BMI
13	6	W	103	- - - - - - - - - - - - - - - - - - -	Water sample taken for Contract Lab at 100', WE-GW52-100		30.0	0.2		30.
14	6	W	165	- - - - 110-	Very Dense, Brown Fine to Coarse SAND, Trace to Little Fine Gravel (SP)		71.8	0.0		71.{
15	12	117	150	- - - - - - - - - - - - - - - - - - -						
15		w	150	- - - - - - - - - - - - - - - - - - -				0.2		653.

NGINEERING INC.	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring No.         W-52           Surface Elevation         1216.5           Job No.         13076.25           Sheet         4         of							
ONE SC	TIENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(608	273-0440							
SAMPLE	VISUAL CLASSIFICATION	SO	IL PROPER			IES			
Covery " Moisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC			
	Earth drilled from 131.0' to 152.0', Fine to Coarse Sand, Based on Cuttings and Drilling Action  Probable GRAVEL Layer from 143' to 150' Based on Drilling Action  Probable SAND Layer Based on Drilling Action End Boring at 152.0'	ISF	30.4						

· .

1

. •

	R Z Y I	N	LOG OF TEST BORING	Boring	g No	W	-52/	4
			Project Wausau, WI NPL Site RI/FS	Surfac	e Eleva	ation	121	6.8
			Location Wausau Wisconsin	Job N	0 1	<u>1307</u> of	6.25 1	•••••
	ERING I	NC.	IENCE COURT . P.O. ROX 5385. MAD ISON WIS. 53705 . TEL (6	08) 273-044			·····	
SA	MPLE					OPE	RT	ES
ecovery "	Moisture		VISUAL CLASSIFICATION	qu	Field		Mono-	Field
. Ţ ¥	V N	Depth		TSF	VOC Soil	HNU	τοχ	VOC Wate
		E	Earth Drilled to 36.0', Refer to Boring Log					
		F	0 to 36'					
		E						
Í		- 5-						
		-						
		Ē						
		E 12						
		- "						
		E						
		E I						
		F						
		Eï						
		- 20-						
		E						
		Ē						
		25-						
		E						
		E						
		F_						
		E						
		- 35-						
		ΕI	End Boring at 36'					
		ΕI	-					
		- 40-						
	W	ATER	LEVEL OBSERVATIONS	GE	GENERAL NOTES			
hile Dril	ling 🗵			Start 11/12/87 End11/12				12/8
pon Con	pletion of	of Drillir	ng ¥	Crew Chief MK RigCME			E 75	
ime Afte	r Drilling Voto-	3		Drillin	g Meth	od <u>4</u>	1/4"	HS/
cpin 10 \$1	valer			0-36'				

V			Y N	7	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No. e Eleva o.	W ation 1307	- <b>53</b> 121 76.25	<b>A</b> 17.6
ENG	INE	ERINO	G IN	с.	Location Wausau, Wisconsin	Sheet	1	of	2	
$\geq$	SΔ	MPI	F	ONE S	CIENCE COURT + P.O. BOX 5385, MADISON, WIS. 53705 + TEL.(	508) 273-044 SO			=RT	
Recov	very "	Moist	ure		VISUAL CLASSIFICATION	qu	Field		Mono-	Fie
No.	<u>, î</u>	4	N	Depth	- And Remarks	( )P.P. TSF	VOC Soil	HNU	tox	VO Wat
				E						
1.	6	М	7		FILL: Concrete, Bricks, Miscellaneous Rubble					
2	1	M	110							
	<b> </b>			E 10-				 		
			~~~							
5	3	M	57							
					Dense to Very Dense, Brown Medium to Coarse SAND, Little Fine Gravel, Trace Silt					
4	12	М	32							
				- 20- - -	Contract Lab Soil Sample obtained at 20', WE-SW53A-20-01					
5	18	M/W	50							
				- 25- -						
				- ⊒_30-						
6	18	w	96							
<u> </u>	•			- 35- -						
					Contract Lab Soil Sample obtained at 40'.					49
7	24	w	205	<u> </u>	WE-SW53A-40-01					
			WA	TER	LEVEL OBSERVATIONS	GE	NER/	AL N	ΙΟΤ	ES
While Upor Time Dent	Dril Con Afte	ling pletic r Dril Vater	<mark>≚ 3</mark> on of ling	0.9 Drilli	ng ¥	Start Crew 0 Drillin	11/2/9 Chief J g Meth	87 E IW R Iod 4	Ind 11 Lig 1 1/4"	/2/1 D-50 ' HS

ł

	Project Wausau, WI NPL Site RI/FS	Surfac	g No. :e Eleva 0	<b>VV</b> ition 1307	- <b>53</b> 121 6.25	A .7.6			
ENGINEERING INC.	Location Wausau, Wisconsin	Sheet		of	2				
SAMPLE		SO	SOIL PROPERTIES						
	and Remarks	()P.P. 	VOC Soil	HNu	tox	VOC Wate			
	End Boring at 41.3' 50- 55- 60- 65- 70- 75- 80-								

• .

W A	R	Z_`	YN		LOG OF TEST BORING	Boring	g No	N	/-53	8
					Project Wausau, WI NPL Site RI/FS	Surfac	e Eleva	tion	121	7.5
	FED			~	Location Wausau, Wisconsin	JOD N Sheet	o <b>1</b>	0f	0,45 4	
GIN			J 1190	-ONE SC	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(	608) 273-044	.0			
S	AN	1PL	.E		VISUAL CLASSIFICATION	SO	IL PR	OPE	ERT	IES
overy	=% M	oisti	ure		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Field
<u> </u>	<u></u>	*	<u>N</u>	Depth -	Earth Drilled to 43.5'	TSF	Soil			Wate
					Refer to Boring Lot W-53A for Soil					
			:	E	Description and Classification from 0-43.5'.					
				E						
				F 5-						
				E						
				-						
				F						
				E 1						
				- "						
				<b>-</b>						
				E-						
				F						
				- 15-						
				E						
				20-						
				-						
				E						
				- 25-						
				_						
		Í		-						
1				-						
										22
				- 35-						55.
ł				ΕI						
				<u> </u>						
				-						
				- 40						
			WA	TER	LEVEL OBSERVATIONS	GENERAL NOTES				ES
D	rillir	ıg -	<u>¥</u> _3	0.0						/2/8
n Co	ompl	letio	n of	Drillin	ng ¥	Crew	Chief J	WR	tig	D-50
e Af	ter ]	Dril	ling			_ Drillin	g Meth	od 5_7	7/8" ]	RB/C
th to	) wa	ter				0-171.5'				

1

ļ







W	AF		Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No. e Eleva o.	N tion 1307	<b>/-5</b> 4 121 (6.25	l 16.9
ENG	INE		G ING	с.	Location Wausau, Wisconsin	Sheet	1	of	3	
>	SA	MP	LE	-ONE SC	CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(608	<u>3) 273-044</u> SO		OP	ERT	IES
Recov	ery " R=%	Moist			and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC
NO.	•	*			6" Bituminous Asphalt	TSF	Soil			Wate
1	14	M	47		FILL: Foundry Sand, Slag, Concrete, Bricks and Miscellaneous Rubble					
2	1	М	20	- 5- -				0.4		
3	12	М	16		Sample and Duplicate WE-SW54-5-01,			0.4		
	2	λÆ	6	- 10 - -	We-SW54-5-91 Loose, Brown Silty Fine to Medium SAND, Little Fine Gravel (SM)					
	3	111	0							
5	12	М	61		Dense to Very Dense, Brown Fine to Coarse SAND, Trace to Little Fine Gravel, Trace Silt (SP)			0.2		
6	12	М	66	- 20- - -	Contract Lab Soil Sample WE-SW54-20-01			0.2		
7	8	M	42	- 25-	Lost approximately 150 gal of drilling mud from 17 to 34'			0.2		
				) 						
8	6	W	77	-   ∑⊒ 30	Contract Lab soil sample WE-SW54-30-01					
-										396
				- 35- - - -						
				- - 40-						
	L		WA	TER	LEVEL OBSERVATIONS	GE	NER		IOT	ES
While Upon Time Deptl	Dril Con Afte h to V	ling pletic r Dril Vater	<mark>∑ 3</mark> on of lling	0.0 Drilli	ng ¥	Start Crew Drillin 5 7/8	11/11/ Chief J g Meth RB/D	87 E IW F Iod M 5-1	End <b>1 1</b> Rig HSA 87.5'	/12/1 D-50 0-5'



WARZY	<u>N</u>	LOG OF TEST BORING	Boring	3 No	W	-54				
		Project Wausau, WI NPL Site RI/FS	Surface Elevation         1216.9           Job No.         13076.25							
	INC	Location Wausau, Wisconsin	Sheet	3	of	3				
	ONE SC	IENCE COURT . P.O. BOX 5385, MAD ISON, WIS. 53705 . TEL.(6	L.(608) 273-0440							
SAMPL	E	VISUAL CLASSIEICATION	SOIL PROPERTIES							
ecovery " Moistu R=%	ire	and Remarks	qu ( )8 P	Field	- NN	lono-	Fiel			
-	N Depth		TSF	Soil	nnu		Wate			
	<u> </u>	Little Fine Gravel. Trace Silt (SP)								
	-	Contract Lab Groundwater Sample obtained								
	E	from 85', WE-GE54-85-01								
	F 90-									
	E	End Doring at 97.5'								
		End bornig at 87.5								
	E									
	E 95_									
						Ì				
	Ē									
	E					ł				
		· · · ·								
	E 105-									
	<u>-</u>	· · ·								
1 1 1	E I									
	- 110 -									
	EI									
	F									
	E l									
	- 115-									
	ΕI									
	-									
	<u> </u>									
	- 120-									
	E I									
	E I									
	- 125-									
	-									
	F									
	ΕI									
	- 130									
	1 1									

W	A F	₹Z	Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No e Elev: o.	W ation 1307	- <b>55</b> / 121 6.25	<b>A</b> 8.0
ENG	INEE	RINO	G INC		Location Wausau, Wisconsin	Sheet	1	of	2	
$\geq$	SA	MPI	LE	ONE SO	VISUAL CLASSIELCATION	<u>18) 273-044</u> SO	IL PR		RT	IES
Recove	۲¥ " R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	KNu	Mono- tox	Field VOC
NO. T	<u>+</u>			Depth -	Dark Brown Silty TOPSOIL	TSF	Soil			Water
				-	Loose to Medium Dense, Brown Fine to Coarse SAND, Trace to Little Fine Gravel, Little Silt (SP)					
1	12	M	29		Little Sitt (Sr)					
	-			-						
2	4	M	26	-				1		<u></u>
				10   						
3	0		54	-						
				— 15— - - - -	No Sample Recovery					
4	12	M	19	- - - 20-						
				- - - -						
5	14	М	22							
				- 25- - -						
6	14	М	11							
				30 						
7	12	w	8	Z						
	 			- 35- -	Contract Lab Soil Samples obtained from 35', WE-SW55A-35-01					
				-						
				- 40- TEP			NED			
While Upon Time Depth	Drill Com Afte: to V	ling pletic r Dril /ater	$\frac{\mathbf{VVA}}{\mathbf{V}}$			Start Crew 0 Drillin	10/15/ Chief ] g Meth	<b>4L N</b> (87 E LB R lod 4	nd10 ig Cl 1/4"	ES (15/8 ME 4: HSA

N			YN	-	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS		Boring Surfac Job N	; No e Eleva o	W ition 1307	- <b>55</b> 121 6.25	A 8.0
ENC	GINE	ERING	G INC	C.	Location Wausau, Wisconsin		Sheet		of		
_	SA	MP	LE	- UNE SC	VISUAL CLASSIFICATION	(80	273-044 SO	IL PR	OPE	ERT	IES
Reco No.	very " R=% ∏↓	Moist ↓	ure N	Depth	and Remarks		qu ( )P.P. ISF	Field VOC Soil	HNu	Mono- tox	Fiel VOC Wate
8	18	W	34		Loose to Medium Dense Brown Fine to Coarse SAND, Trace to Little Fine Gravel, Little Silt (SP)						30.
	- 			- 45-	End Boring at 43'						
				- - - - - -							
				- - - - - - - - - - - - - - - - - - -							
				- 65 							
				- - - - - - -							•
	•			- - - - - 75-							
				80    							
				- 85-							

•

WAI ENGINEI	RZYN	<b>-</b>	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin		Boring Surfac Job N Sheet	g No e Eleva o1	M ation 1307 of	<b>/ - 55</b> 121 (6.25 4	5
		- ONE SC	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL	.(608	273-044			-07	
SA Recovery "	Moisture		VISUAL CLASSIFICATION			IL PR		KI	IES Fiel
R=% No.  T  ↓		Depth	and Remarks		( )P.P.	VOC	HNu	tox	VOC
			Earth Drilled to 48.5', Refer to Boring Log W-55A for Description and Classification from 0 to 48.5'						
		- 40-							
k.l	WA	TER	LEVEL OBSERVATIONS	.1	GENERAL NOTE				ES
While Dril Upon Con Time After Depth to V	lling ¥ npletion of er Drilling Water Cave in	Drillin			Start Crew Drillin 0-11';	Start 10/19/87 End10/2 Crew Chief DZ Rig CMI Drilling Method 4 1/4" H 0-11'; RB/DM 11-128.5'			





ENGINEER	ING INC.	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring No. W-55 Surface Elevation 1217. Job No. 13076.25 Sheet 4 of 4								
$\geq$	ONE SC	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.	<u>608) 273-04</u>	40			=				
SAN	IPLE	VISUAL CLASSIFICATION	SO	SOIL PROPERTIES							
Recovery " M	bisture	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC				
No. T 🖌	N Depth	End Poring at 120.02	TSF	Soil			Wate				
		End Boring at 150.0									
	ΙE										
	I E										
			:								
	L 145-			-							
	- 150-										
						]					
						1					
	- 155-										
	E										
	165-										
	- 170-				1						
		· ·									
	- 175-										
11 1						r I					

WARZYN						LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No.         W-56A           Surface Elevation         1198.8           Job No.         13076.25				
ENG	INE		G IN	С.	50	Location Wausau, Wisconsin	Sheet	1	of	1	
SAMPLE						VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES
Recov	/ery " R=% T ↓	Moist	ure N	Dep	th	and Remarks	qu ()P.P. ISF	Field VOC Soil	HNu	Mono- tox	Field VOC Water
1	8	М	5	لىلىلىلىلىل	5	Dark Brown Organic SILT (Topsoil) (OL) Loose, Dark Brown Fine to Medium SAND, Little Silt, Trace to Little Fine Gravel (SP-SM)			0.1		
- 2	5	W	20			Medium Dense to Dense, Dark Brown Fine to Coarse SAND and GRAVEL (SP)					
		**		¥∎ 1	0				0.1		
3	6	W	27		5-	Grades Little to Some Fine Gravel near 13.5'			0.1		
				ليايل							
4	4	W	13	2	20				0.1		
				2 2 2 3 3 4 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	!5  0  5	End Boring at 20'					
			14/4		0-						
While Upon Time Deptl Deptl	WATER LEVEL OBSERVATIONS         While Drilling ¥ 9.5         Upon Completion of Drilling ¥         Time After Drilling         Depth to Water         Depth to Cave in						GENERAL NOTES Start 10/15/87 End10/15/87 Crew Chief LE RigCME 450 Drilling Method 4 1/4" HSA 0-20'				

WARZYN					LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. W-56 Surface Elevation 1198.9						
					Logation Wangan Wingangin	Job No. 13076.25						
ENGI	NEE	RINC	g in	C.	Location wausau, wisconsin	.   Sneet	<b>I</b>	01	<u>4</u>			
	SAR	MPI	F	UNE	SCIENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(6							
Recover	ecovery " Moisture				VISUAL CLASSIFICATION	qu Field Mono Fiel						
No. T	K=‰ ↓	ţ	N	Dept	and Kemarks	()P.P. TSF	VOC Soil	HNu	tox	VOC Wate		
				ערין גן גן גן גן גן גן אוערין גן	Earth Drilled to 23.0', Refer to Boring Log W-56A for Soil Description and Classification from 0 to 20'							
1	13	w	39	- lululy	Dense to Very Dense, Brown Fine to Coarse SAND, Trace Fine Gravel (SP)					-		
								0.0				
2	6	W	51	- - - - - - - - - - - - - - - - - - -				0.0		5.4		
3	15	W	100					00				
			10/0							FC		
WATER LEVEL OBSERVATIONS         While Drilling ¥ 9.0         Upon Completion of Drilling ¥         Time After Drilling         Depth to Water         Depth to Cave in						Start 10/19/87 End10/20/8 Crew Chief JW Rig D-50 Drilling Method5 7/8" RB/DI 0-65.5'						



A W	RZ	Y N	,	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. W-57 Surface Elevation 1202.1							
					Job N	ío.	1307	6.25				
ENGINE	ERING	G INC	2.	Location Wausau, Wisconsin	Sheet	1	of	2				
<u> </u>		F	-ONE SO	CIENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(608	<u>273-04</u>							
Recovery_	Moist	ure		VISUAL CLASSIFICATION	qu Field Mono- Field							
No. T		N	Depth	and Remarks	( )P.P. 	VOC Soil	HNu	tox	VOC Water			
			ılılı	Trace to Little Fine Gravel (SP)								
1 12	M	62	1.1									
			- 5- -				0.0					
			-	Contract Lab Soil Sample WE-SW57-10-01								
$\frac{2}{3}$ $\frac{6}{4}$	M	111	- 10-				1.0					
4 12	M	109					3.5					
			- -									
			- <u>1</u> 5-	Loose, Brown Fine to Coarse SAND, Trace to Little Fine Gravel (SP)								
5 6	W	10	三 - - 20-				1.5		ND			
			- - -	Contract Lab Groundwater Sample taken at 21', WE-GW57-21-01								
6 6	w	11	- - -				1.8					
			25 									
7 2	w	2	- - - 70-				1.8		ND			
			- 30- - -									
			- 75									
8 4	w	2	-				1.1		BMDL			
		WΔ			GF	NFR			FS			
While Drilling ¥ 18.5         Upon Completion of Drilling ¥         Time After Drilling         Depth to Water						Start 10/21/87 End10/21/87 Crew Chief JW Rig D-50 Drilling Method RB/DM 0-77.5'						


B.2 DEPARTMENT OF TRANSPORTATION BORING LOGS

-

Í

1

W		R Z	Y N	•	LOG OF TEST BORING           Project         Wausau, WI NPL Site RI/FS	Boring Surfac	g No ce Eleva	<b>D(</b> ation	DT : 118	<b>1</b> 8.1		
	$\checkmark$						Job No. 13076.25					
ENG	INE	ERING	G INC	Ξ.	Location Wausau, Wisconsin	Sheet <u>1</u> of <u>2</u>						
$\geq$				-ONE S	CIENCE COURT . P.O. BOX 5385, MADISON, WIS. 53705 . TEL.(6	08) 273-04	40		. ··			
	SA	MP	LE		VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	IES		
Recov	ery " R=%	Moist	ture		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fi V		
NO.		¥	N	Depth _	Air	TSF	Soil			¥.		
				-	WATER							
				_								
					· · · · · · · · · · · · · · · · · · ·							
1	4	W	0	- 5	Very Loose Gray Organic SILT. (OL) Laver			<u> </u>				
	┞╌──┤			_	of Wood							
					Loose Gray Silty SAND (SM) with Trace							
2	10	W	4	10- 	Gravel and Layer of Peat (PT)							
					Dense, Gray Silty SAND, Little Gravel (SM)	·		<u> i</u>				
					]							
3	12	W	30	_ ''								
				-			•					
. [				-	· ·							
				- - 20-	4							
4	0		30	_								
				-								
				-	Firm, Brown Fine to Coarse SAND, Trace of							
5	6	W	22	- 25-	Gravel (SP)							
	·		[	-								
		ļ		-								
[				-								
6	8	W	15	- 30-	1							
·····	┞──┤		├Ē	-		J				<u> </u>		
				-								
7	6 ·	W	34	35- - 	Grading to Fine to Medium Sand (SM) at 35'							
				-	Dense Brown/Gray Weathard Create							
				-	Conse, Brown/Gray weathered Granite							
				 40	1							
	L I		WΔ		LEVEL OBSERVATIONS		NED			20		
While	D-:11	inc	$\nabla$							<u>=3</u>		
Upon	Com	pletic	= on of	Drilli	ng	Start Crew	<u>9/4/8</u> Chief	4 E: K R	nd <u>9/</u> ig	<u>5/8</u> 6		
Time	After	r Dril	lling			Drillin	g Meth	od	-6			
Depth	to W	ater										

•

·

.

					Project Wausau, WI NPL Site RI/FS	Boring No. <b>DUI 1</b> Surface Elevation 1188.1 Job No. 13076.25						
ENG	ENGINEERING INC.			: 1	Location Wausau, Wisconsin		Sheet 2 of 2					
$\geq$				ONE SC	IENCE COURT . P.O. BOX 5385, MADISON, WIS. 53705 . TEL.(6	(608) 273-0440						
SAMPLE			LE		VISUAL CLASSIFICATION	SO	IL PR	OPE	RT	ES		
Recov	rery" R=% ₹	Moist I	ure	0 + h	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fie VO		
8	18	W	35	- -	Dense, Brown/Gray Weathered Granite	TSF	Soil			Wat		
9	6	W	95 <del>/6.5</del> "	- - - - - - - - - - - - - - - - - - -	Very Dense, Brown Weathered Granite NQ Core 46.0 to 49.5' RQD 66%		 					
				- - - 50	End Boring at 49.5'							
				- - - - - - - - - - - - - - - - - - -	Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987							
				- 60- 								
				- 65- - -								
		¢		70								
				- 75- -								
				- - 85-								

Y

	A F	₹ Z `	Y N		LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No ce Eleva	DO ation	<b>T 1</b>	M 1.8			
ENGINEERING INC.					Location Wausau, Wisconsin		JOB No.         130/6.25           Sheet         1         of         3						
$\geq$	2 4			ONE SC	IENCE COURT · P.O. BOX 5385, MADISON, WIS. 53705 · TEL.(6	08) 273-044	40		-07				
Recover	<b>3</b> A y "	Moist			VISUAL CLASSIFICATION		QU Field Mono-1 Fi						
No. T	R=% ∳	ł		Depth	and Remarks	()P.P. TSF	VOC Soil	HNu	tox	VC Vat			
			E	_	Brown TOPSOIL				1				
				-	Very Loose, Dark Brown SILT (ML)								
1	10	Μ	10	- 5				1					
				-	Firm, Brown SAND & GRAVEL, Trace SILT (SP)								
2	24	W		- 10				<u> </u>	<b> </b>				
				- - -	Firm, Gray Fine to Medium SAND, Trace Gravel (SP)								
3	12	w		- 15-					<u> </u>				
-				.									
				•	Loose, Brown Fine to Coarse SAND Trace					1			
4	14	W	7	· 20	Gravel (SP)								
5	12	W	15	25	Gravel (SP)								
				. 30									
6	12	W					-						
7	12	w		35-									
				40-									
11_			WAT	TER	LEVEL OBSERVATIONS	GF	NFR			FS			
While I Upon ( Time A	Drill Com	ing pletic Dril	∑ on of I ling _	Drillin		Start Crew Drillin	9/4/8 Chief g Meth	4 E R	nd <u>9</u>	/4/8			

W			Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac Job N	g No e Eleva o	DO ation 1307	<b>T 1</b> 119 6.25	M 91.8		
ENG	INE	RING	g ing		Location Wausau, Wisconsin	Sheet         2         of         3           08) 273-0440						
$\geq$	SA	MP	LE	- UNE SU	VISUAL CLASSIFICATION							
Recov	/ery " R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fiel VOC		
NO. Q		<u>+</u>	N 15	Depth		TSF	Soil			Wate		
0	12		13		Firm, Brown Fine to Coarse SAND, Trace Gravel (SP)							
9	16	Ŵ	11	- 45-								
				-								
				- - - 50								
10	18	W	19									
				_	· · · · · · · · · · · · · · · · · · ·							
11	19	w	21	- 55-	Firm, Brown Fine SAND, Trace Silt (SP)							
				- - 60-	Firm, Brown Fine to Coarse SAND (SP)							
12	18	W	21	-								
				-								
13	14	w	47	- - 65-								
				-	Dense, Brown Fine to Medium SAND, Trace Gravel, Little Silt (SP-SM)							
				-  70								
14	18	W	15	-								
				-			i					
15	18	W	30	- - 75-	Dense, Brown Medium SAND (SP)							
	┞			-								
				- - 80-								
16	18	W	33		Dense, Brown Fine to Medium Sand (SP)							
				-								
				- 85-								

ł

1

WARZYN					LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS Location Wausau, Wisconsin	Boring No.DOT 1MSurface Elevation1191.8Job No.13076.25Sheet3Of3						
ENC				NE SC	IENCE COURT . P.O. BOX 5385, MAD ISON, WIS. 53705 . TEL.(6	508) 273-044	.0					
	SAMPLE				VISUAL CLASSIFICATION	SOIL PROPERTIES						
Reco	/ery " R=%	Moist	ure		and Remarks	qu ()P.P.	Field VOC	HNU	Mono- tox	Fiel VOC		
				- <u>90</u>	Dense, Brown Fine to Medium SAND (SP)							
17	10	W		95-								
18	18	W	24	100-								
				105-	End Boring at 102.5' Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987							
				115—								
			بابليليل	120-								
				130-								

•

-

ij

V		R Z	Y N	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring No. DOT 2 Surface Elevation 1187.8 Job No. 13076.25						
ENG	INE	ERIN	G INC.	Location Wausau, Wisconsin	Sheet	Sheet 1 of 2					
$\geq$	SA	MP	ONE	VISUAL CLASSIEICATION	508) 273-044 SO	IL PR	OPE	ERT	IES		
Recov	ery "	Moist	ure		qu	Field		Mono	Fiel		
No.	<u>ī</u> ] <b>↓</b> _		N Dept	and Remarks	()P.P. TSF	VOC Soil	HNU	tox	VO Vate		
	1			Air							
1	8	w	8						<u> </u>		
2	4	W									
3	8	W	8- 25	-							
		· · · · ·									
				Firm, Gray Medium to Coarse SAND, Trace of Gravel, Trace of Silt (SP)					ł		
4	18	W	12- 30								
					┣						
									1		
5	16·	W	19 35	7							
			-								
			Ŀ,								
While Upor Time	Dril Com Afte	ling ipletic r Dril	vvAIC ∑ on of Drill lling		Start Crew O Drillin	9/6/8 9/6/8 2 Meth	4 E K R lod	io I ind <u>9</u> ig	<u>5</u> 6		

W			Y N	•	LOG OF TEST BORING Project Wausau, WI NPL Site RI/FS	Boring Surfac	g No e Eleva	D ition 1307	OT 118	<b>2</b> 7.8		
ENG	INEE	RING	G INC	C.	Location Wausau, Wisconsin	Sheet 2 of 2						
SAMPLE Recovery "   Moisture				- ONE SC	VISUAL CLASSIFICATION		SOIL PROPERTIES					
No. T	``k=%   }	1		Depth	and Remarks	( )P.P.	VOC	HNu	tox	VOC		
6	12	Ŵ	11		Firm, Gray Mediumto Coarse SAND, Trace of Gravel, Trace of Silt (SP)					W.d.L		
7	3	W	12	45- 								
8	18	W	31	- - - - -	Dense, Brown Fine to Coarse SAND, Trace Silt, Little Gravel (SP)							
9	18	w	31	- - - - 55-			· .					
	10		51		Dense, Brown Medium to Coarse SAND, Trace of Gravel and Silt (SP)							
10	13	W	80 - /7"	60 - - -	Very Dense, Brown SAND & GRAVEL, Much Silt (GM)							
11	0	-	80 - /2"	- - - 65-	Dense, Brown/Gray Weathered Granite End Boring at 65'							
				- - - - - - - - - -	Note: Soil samples were obtained by Wisconsin Dept. of Transportation in September, 1984. Soil descriptions were checked against samples by Warzyn Engineering November, 1987		·					
	•			- - - - - - -								
				- - - - - - -								
		:		- 85-								

.

W	AR	ΖY	N		LOG OF TEST BORING	Boring	g No	DO	)T 2	M
					Project Wausau, WI NPL Site RI/FS	Surfac	e Eleva	ition 1307	<u>119</u> 6 25	6.8
ENGI	ENGINEERING INC.				Location Wausau, Wisconsin	Sheet	1	of	3	
$\geq$			(	DNE SC	IENCE COURT - P.O. BOX 5385, MADISON, WIS. 53705 - TEL.(60	8) 273-044	•0			
	SAN	IPL	E		VISUAL CLASSIFICATION	SO	IL PR	OP	ERT	IES
Recover	χ "   Μα ξ=%   ⊥	oistu ∫ Γ		enth	and Remarks	qu ()P.P.	Field VOC	HNu	Mono- tox	Fie
	×	<u> </u>	-	, epcil	Firm Brown SAND, Some Gravel (SP)	TSF	Soil			Wat
				- 5						
1	14	w	22	15	Firm Gray Fine to Coarse SAND, Trace Gravel (SP)					
2	16	w	12-	20—						
3	12	W	8-	25	Loose, Brown Fine to Coarse SAND (SP)					
		V	15	30	Firm, Brown Fine to Coarse SAND, Trace Gravel (SP)					
5	12 . 1	w		35						
			F							
	_1_			<u>+0-</u>	LEVEL OBSERVATIONS		NED			
While Drilling     ∠       Upon Completion of Drillin       Time After Drilling			Z n of C ing	<u>L</u> R		Start Crew ( Drillin	9/6/8 Chief g Meth	4 E M R od	nd 9	ES /6/8 VII

. .

.



## APPENDIX C WELL CONSTRUCTION DETAILS

·

.









8	NO. 13076	.25	
R	ING/WELL NO. E-22	) 	
T	E10/14/	87	
I	EF/UNITJW	I/D-50	
	SCREEN TYPE	Stainless Stee	el <u>.</u>
	SLOTTED LENGTH	5.0'	ft.
	SLOT SIZE 0.01	0"	
	SCREEN DIAMETER	2.0	in.
	SOLID PIPE TYPE	Galvanize	ed
	SOLID PIPE LENGTH	88.7	ft.
	JOINT TYPE SLIP/GL	UED THREADED	>
	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
	TYPE OF BACKFILL A	ROUND SCREEN	
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit	ROUND SCREEN Elint_Sand (IF INSTALLED) e_Pellets	
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite	Slurr
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR	ROUND SCREEN Flint Sand (IF INSTALLED) e_Pellets Bentonite EMIE OM SURFACE	Slurr
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B	ROUND SCREEN Flint Sand (IF INSTALLED) e_Pellets Bentonite EMIE COM SURFACE AL (IF INSTALLE entonite	Slurr D)
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B PROTECTIVE CASING	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite EMIE OM SURFACE AL (IF INSTALLE entonite YES NO	Slurr D)
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B PROTECTIVE CASING LOCKING	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite EMIE COM SURFACE AL (IF INSTALLE entonite YES NO YES NO	Slurr D)
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B PROTECTIVE CASING LOCKING CONCRETE SEAL	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite EMIE OM SURFACE AL (IF INSTALLE entonite YES NO YES NO	Slurr D)
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B PROTECTIVE CASING LOCKING CONCRETE SEAL DRILLING METHOD	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite EMIE OM SURFACE AL (IF INSTALLE entonite YES NO YES NO RB/DM	Slurr D)
	TYPE OF BACKFILL A No. 30 TYPE OF LOWER SEAL Bentonit TYPE OF BACKFILL HOW INSTALLED TR FR TYPE OF SURFACE SE Granular B PROTECTIVE CASING LOCKING CONCRETE SEAL DRILLING METHOD ADDITIVES USED (IF None	ROUND SCREEN Flint_Sand (IF INSTALLED) e_Pellets Bentonite EMIE OM SURFACE AL (IF INSTALLE entonite YES NO YES NO YES NO RB/DM ANY)	Slurr D)

\*ALL DEPTHS MEASURED FROM GROUND SURFACE.

.

DATE

















MON	ITORING WELL CONSTRUCTION INFORMATION
JOB	NO. 13076.25
BOR	ING/WELL NO. E-27
DAT	E 12/12/87
CHI	EF/UNIT PD/D-50
1.	SCREEN TYPE <u>Stainless</u>
	SLOTTED LENGTH 5.0 ft.
	SLOT SIZEO.010"
	SCREEN DIAMETER 2.0 in.
2.	SOLID PIPE TYPEGalvanized
	SOLID PIPE LENGTH 131 ft.
	JOINT TYPE SLIP/GLUED THREADED
3.	TYPE OF BACKFILL AROUND SCREEN #30 Flint Sand
4.	TYPE OF LOWER SEAL (IF INSTALLED) Bentonite Pellets
5.	TYPE OF BACKFILL Bentonite Slurry
	HOW INSTALLED FROM SURFACE
б.	TYPE OF SURFACE SEAL (IF INSTALLED) Granular Bentonite
7.	PROTECTIVE CASING YES NO
	LOCKING YES NO
8.	CONCRETE SEAL
9.	DRILLING METHOD RB/DM
10.	ADDITIVES USED (IF ANY) None
11.	TYPE OF BACKFILL #30 Flint Sand
WATE	ER LEVEL DATE



Ĵ

\*ALL DEPTHS MEASURED FROM GROUND SURFACE.



ENGINEERING INC

. .

MON	ITORING WELL CONSTRUCTION INFORMATION
JOB	NO. <u>13076.25</u>
BORI	ING/WELL NO. <u>E-28A</u>
DATE	10/13/87
CHIE	F/UNITLE/CME 45
1.	SCREEN TYPE Stainless Steel
	SLOTTED LENGTH 9.5 ft.
	SLOT SIZE0.010"
	SCREEN DIAMETER 2.0 in.
2.	SOLID PIPE TYPE <u>Galvanized</u>
	SOLID PIPE LENGTH 27 ft.
	JOINT TYPE SLIP/GLOED THREADED
3.	TYPE OF BACKFILL AROUND SCREEN No. 30 Flint Sand
4.	TYPE OF LOWER SEAL (IF INSTALLED) Bentonite Pellets
5.	TYPE OF BACKFILL Bentonite Slurry
	HOW INSTALLED - TREMIE
δ.	TYPE OF SURFACE SEAL (IF INSTALLED) Bentonite Pellets/Concrete
7.	PROTECTIVE CASING YES NO
	LOCKING YES NO
8.	CONCRETE SEAL YES NO
9.	DRILLING METHOD HSA
0.	ADDITIVES USED (IF ANY)
1.	TYPE OF BACKFILL None
WAT	ER LEVEL

\*ALL DEPTHS MEASURED FROM GROUND SURFACE.



ENGINEERING INC

MON	ITORING WELL CONSTRUCTION INFORMATION
JOB	NO. <u>13076.25</u>
BOR	ING/WELL NO. <u>E-29A</u>
DAT	E10/23/87
СНІ	EF/UNITLE/CME 750
1.	SCREEN TYPE Stainless Steel
	SLOTTED LENGTH 10 ft.
	SLOT SIZE 0.010"
	SCREEN DIAMETER 2.0 in.
2.	SOLID PIPE TYPE <u>Galvanized</u>
	SOLID PIPE LENGTH 18.1 ft.
	JOINT TYPE SLIP/GLUED THREADED
3.	TYPE OF BACKFILL AROUND SCREEN No. 30 Flint Sand
4.	TYPE OF LOWER SEAL (IF INSTALLED) Bentonite Pellets
5.	TYPE OF BACKFILL Bentonite Slurry
	HOW INSTALLED - TREMIE
б.	TYPE OF SURFACE SEAL (IF INSTALLED) Granular & Pellet Bentonit
7.	PROTECTIVE CASING YES NO
	LOCKING YES NO
8.	CONCRETE SEAL
9.	DRILLING METHOD
10.	ADDITIVES USED (IF ANY) None
11.	TYPE OF BACKFILL None
WAT	ER LEVEL 19.12 DATE 10/23/87

• •

\*ALL DEPTHS MEASURED FROM GROUND SURFACE.






















ENGINEERING INC

.

. . .

MON	ITORING WELL CONSTRUCTION INFORMATION
JOB	NO. <u>13076.25</u>
BOR	ING/WELL NO
DAT	E 10/5/87
СНІ	EF/UNIT LE/CME-45C
1.	SCREEN TYPE Stainless
	SLOTTED LENGTH 9.5 ft.
	SLOT SIZE 0.010"
	SCREEN DIAMETER 2.0 in.
2.	SOLID PIPE TYPEGalvanized
	SOLID PIPE LENGTH <u>32.4</u> ft.
	JOINT TYPE SLIP/GLUED THREADED
3.	TYPE OF BACKFILL AROUND SCREEN No. 30 Flint Sand
4.	TYPE OF LOWER SEAL (IF INSTALLED) Bentonite Pellets
5.	TYPE OF BACKFILL Bentonite Slurry
	HOW INSTALLED - TREMIE
б.	TYPE OF SURFACE SEAL (IF INSTALLED) Bentonite Pellets
7.	PROTECTIVE CASING YES NO
	LOCKING YES NO
8.	CONCRETE SEAL
9.	DRILLING METHOD HSA
10.	ADDITIVES USED (IF ANY)
11.	TYPE OF BACKFILL -
WAT	ER LEVEL DATE

\*ALL DEPTHS MEASURED FROM GROUND SURFACE.











APPENDIX D SOIL GAS INVESTIGATION RESULTS

. .

• • •

WAUSAU MPL RI/FS

.

.. · ·

.

..

۰.

TARGET SOIL GAS ANALYSES

:

.

DETECTION	TOLUENE ag/L	1,1 DCE ng/L	1,2-DCE ng/L	1CE ng/L	PCE ag/L	BENZENE ng/L	ETH-DENJENE ng/L	MECL2 ng/L	I,1DCA ng/L	CHCL3 ng/L	1,2DCA ag/L	1,1,1TCA ng/L	BRCL2CH ng/L	CLBR2CH ng/L	BROMOFORM ng/L	TOTAL CHLOR Ethenes	TOTAL
LINII (ng/L	.) 1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	2000	2000	1000	1000
LOCATIONS																	
10-13-87 S61 S62 S63 S64 S65 S81	*****	******		************				*******	******		*****	*****					*******
10-14-87 566 567		******	*****	*****		-			******								
568 559 569 DUP 5510 5611																	******
S612 S613 S614 S515 S614				******		) <u>1</u> 4 4 6 4 6 4 4 6 4 6 4 6 4 6 4 6 4 6 4	******		********		********	********	*******		*********	*****	
5617 5618 5619 5620 582			••••••	*****			*******			******	*******		f\$*******	********		************	
10-15-87 5621 5622 5623				BMDL	BMDL BMDL BMDL			*********		*****	*******	*********	*********	*******	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	BHDL BHDL BHDL BHDL BHDL	BMDL BMDL BMDL
S624 S625 S626 S627 S628					BNOL BNOL BNOL BNOL BNOL BNOL	*****	*******	*******		*******		********		********		BMDL BMDL BMDL BMDL BMDL BMDL BMDL	BMDL BMDL BMDL BMDL BMDL BMDL BMDL
583 (1) 5629 5630 5631 5632					BMDL	•••••	*****			*****		*****		********		вала в на	BMDL
S633 S633 S634 S635 S635 S635		*******		BNDL	********	**********			********		******		*****		*****	BNDL	BHDL
10-16-87				**************	*********	**********	************	*********	********		*********	**********	*********		*********	**********	*******
SG21REPEAT SG21REPEAT SG2SREPEAT SG37 SG37 SG37 SG4		********		*****			*****		*******				••••		*****		*******

### WAUSAU NPL RI/FS

### TARGET SOIL GAS ANALYSES

DETECTION	TOL VENE ng/L	1,1 DCE ng/L	1,2-DCE ng/L	TCE ng/L	PCE ng/L	BENZENE E ng/L	TH-BENZENE ng/L	NECL 2 ng/L	1,1DCA ng/L	CHEL3 ng/L	1,2DCA ng/L	1,1,1TCA ng/L	BRCL2CH ng/L	CLBR2CH ng/L	BRCHOFORM ng/L	TOTAL CHLOR ETHENES	TOTAL
LINII ING/LI	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	2000	2000	1000	1000
S638	*******	********															
5639 5640 5641				*****		BADL Badl	******		*****	**********	********	**********	**********	*********			BMDL BMDL
5642 5643						8MDL											RHDI
5644 5645 5646 5647 5548				*******		-	********		******	********		**********			*******	******	*****
*************** \$649				***********	******	********		*******	********		*********		********		*******	******	********
10-19-87				<b></b>								BUD					
S651	~ 			BRDL													
S652 S653					*******		*********		********		**********	**********	**********	*********	********	**********	*******
S654 S655															•		
1484+194+++++++	******	********	********	**********		********	*********				********		**********		*******	*****	
10-20-87 5657	OVERAWSE ESTI	NATER VALUE	250	244000	4020000												
SB05	S658-S663 NER GROSS PCE CON	E RERUN DUE TAMINATION	TO CARRY OVER	CONTAMINATIO	N FROM S657							2580				4324000	4324000
***********	*********	********	***********		**********	*********	*******	***********		**********	*****	********	**********	********	*********	*************	*******
5658REP 5659REP 5640REP																	
\$\$\$\$\$\$\$\$\$\$\$\$\$\$	***********	*********	***********	**********		*********	*********	**********	*********		*********	• • • • • • • • • • • • • • •	********			************	********
SG63REP SG63DUPREP						BHDL											BMDL
2004 ###################################	*******	********		**********	5300	*******	*******	*******		***********						5300	5300
SB66 S667					BUDL											BNDL	BADL
5806 5668					BMDL											8MDL	BADL
5669	***********	*********	***********	**********	*********	******	**********	*********	*******	********	*******	**********	********	********	********	***********	*******
5670 5671 5672	1244																1244
5673 ************				********	BMDL											BNDL	BNDL
5674 5674DUP			•		2340 3000					**********	********	***********	**********		********	2340	2340
5807++					BHOL											BHDL	SUDO
**************************************		*********			**********	*********		********	********	*********					********	***********	
S676 S677				RMDL	BNDL							BMD4.				BMDL BMDL	BMDL BMDL
S677DUP				BNDL	1324								BHDL Bhdl			1294 1324	1294 1324

: : •

: ;

. :

•

. . .

..

. .

:

WAUSAU NPL RI/FS

٠

TARGET SOIL GAS AWALYSES

DETECTION	TOLUENE ng/L	L,1 DCE ng/L	1,2-DCE ng/L	TCE ag/L	PCE ng/L	BENZENE E ng/L	TH-BENZENE ng/L	MECL2 ng/L	1,1DCA ng/L	CHCL3	1,20CA ng/L	1,1,1TCA ng/L	BRCL2CH ng/L	CLBR2CH og/L	BRONOFORM ng/L	TOTAL CHLOR ETHENES ng/L	TOTAL VOCS no/L
LOCATIONS S678	1000	. 1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	- 1000	1000	2000	2000	1000	1000
S679 S680 S681 S682 S683		********	*********	**********	BNDL BNDL	********	*********				********	******	********		*****	BMDL BMDL	BMDL BMDL
5684 5685 5808			***********	********		-	***********		*********		********	***********	******		******	*****	*******
10-23-87 \$586 \$687 \$668	*********	BHDL			BHDL BHDL 1606				****	*******	*******	*******				00000000000000000000000000000000000000	BNDL 1404
5690 5690 5691	********				*******	**********		*********	*********	******	*********			*******	*****	****	******
5692 5693 5693DUP 5694 *************	********				6320 4600 3940 5280	*****						BMDL				6320 4600 3940 5280	6320 4600 3940 5280
5695 5696 5809 5697 5698 *************					12960 8440 BNDL BNDL BNDL BNDL										*********	12960 8440 5MDL 9MDL 9MDL	12960 8440 BMDL BMDL BMDL
5699 10-26-87 56100 56101				1004	2660 BMDL									*****		2660 BNDL 1004	2660 BMDL 1004
56102 56103				BNDL		*********	********	**********		**********				********		BNDL	8MDL
10-27-87 56104 ***************		********	******	*******	********	********	**********						********	*****			*******
56105 56106 56107 56107DUP 5610				SMOL	BADL											82000 BNDL	820CO BADL
S6108 S6109		*******	******	*********	********	*********	**********	**********			**********		*********				*******
10-28-87 S6110 ***********************************	******	********	******		********		*********		********		********	******		*********	*******		
66112 66113 SE113DUP S6114	5260 6120																6120
S6115 S811 S6116 S6117			*****	BNDL				**********	*****		********	*********	********		********	BMDL	BMDL

. . .

..

;

÷.

### WAUSAU NPL RI/FS

### TARGET SOIL GAS ANALYSES

DETECTION	TOLUENE ng/L	i,i DCE ng/L	1,2-DCE ng/L	TCE ng/L	PCE ng/L	BENZENE ng/L	ETH-BENJENE ng/L 1000	MECL2 ng/L 1000	1,10CA ng/L 1000	CHCL3 ng/L 1000	1,2DCA ng/L 1000	1,1,11CA mg/L 1000	BRCL2CH ng/L 1000	CLBR2CH ng/L 2000	BROMOFORM ng/L 2000	TOTAL CHLOR ETKENES ng/L 1000	TOTAL VOCS ng/L 1000
LIMIT (ng/L) LOCATIONS S611B	1000				B060											B060	6060
*************** S6119 S6120 S6121 S6122 66123	2060	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1320	5800 4880 2260	BNDL BNDL									****		BNDL BNDL 7120 4880 2260	BMDL BMDL 9180 4880 2260
10-29-87 56124 55125 56126	******	*******	BNDL	12640 63600 BMDL	BMDL BMDL	-										12640 63600 BMDL	12640 63609 BNDL
S6127 S6128 S8 S6129 S6129 S6129 S6129 NiDa	*****		***********	BMDL BMDL 11000 3900	37600 8240 8801 39600 24200		*********									37600 8240 BMDL 50600 28100	37600 6240 BNDL 50600 28100
\$6130 \$6131		******			BMDL BMDL	******		**********		*****	********	***********				BMDL BMDL	BADL Badl
11-10-87 \$5132			*********				********				********	**********		*********			
SS133 S6134 S6135 S6136 S6136 SS137				BMDL		3580						BMDL	****	*****	***********	BMDL.	3580 BKDL BMDL
56138 56139 56140 56141 56142				BNDL 65800 11000	BMDL BNDL BMDL							(BMDL				BNDL BNDL 65800 11000	BMDL BMDL 65800 11000
S6143 S6143DUP				BADL				**********					*****			BNDL	BADL
11-11-87 56144 *************				***********	***********			*********		**********		BNDL			**********		BADL
5614400P 56145 56146 56147					8NDL											8MDL.	BHDL
56148 56149 56150 56151	COULD NOT DR	IVE SOIL BAS	PROBE	**********			***********		***********	***********						**************	
NDTES • S616, S616, S BNDL BELON NIN ++ SB07 RAN US • DILUTED 1:50	SG19 CONTAINE Inum Reportab Ing Bomb From	D UNIDENTIFI Le detection S657	ED COMPOUND P Limit	EAK IN PID CH	ROMATOGRAM				NAV								

BULLIED 1150 5521,5622,5623,5624,5625,5626,5627,5628,583 CONTAIN PEE CARRY OVER FROM WATER SAMPLE AWALYZED EARLIER ON SAME DAY

. :

٠. ,

# APPENDIX E

•

.

## RESULTS OF ROUND 1 SAMPLE DESCRIPTIONS AND GENERAL WATER QUALITY PARAMETER ANALYSES

,

# WAUSAU NPL WEST SIDE ROUND 1 (SEPT. - OCT. 1987)

.

•

· .

W-11 #		Conductivty	<b>.</b> .		
<u>weil #</u>	<u>рн</u>	<u>at 25°</u>	<u>Odor</u>	Color	Turbidity
C2S	6.25	388	None	Clear	None
C4D	5.84	342	None	Clear	Slight
W1A	9.64	227	None	Clear	Slight
W3A	6.95	140	None	Clear	None
W3B	7.27	146	None	Clear	None
W4A	5.88	347	None	Clear	Slight
W4B	6.43	238	None	Clear	None
W4C	6.17	227	None	Clear	None
W7	6.70	350	None	Clear	None
W9	6.15	285	None	Clear	None
R1S	6.30	271	None	Clear	None
R1D	5.85	283	None	Clear	Slight
R1D dup	5.90	283	None	Clear	Slight
R2S	6.54	171	None	Lt. brown	None
R2D	6.38	277	None	Lt. brown	Slight
R3S	6.26	200	None	Clear	None
R3D	6.46	257	None	Clear	None
R4D	6.05	338	None	Lt. brown	Moderate
GM1S	6.16	157	None	Lt. brown	Slight
GM1S dup	6.23	157	None	Lt. brown	Slight
GM4S	6.12	173	None	Lt. brown	Moderate
GM4D	6.81	185	None	Clear	None
GM4D dup	6.79	188	None	Clear	None
PDTW	6.52	230	None	Clear	None
Pumping We	<u>ells</u>				
CW6	6.80	166	None	Clear	None
CW7	7.00	144	None	Clear	None
CW9	6.73	166	None	Clear	None

. -

# WAUSAU NPL EAST WELLS ROUND 1 (SEPT. - OCT. 1987)

.

.

• •

<u>Well #</u>	рH	Conductivty <u>at 25°</u>	<u>Odor</u>	<u>Color</u>	<u>Turbidity</u>
WC1			No sample w	vas obstructed a	at 5'
WC2	6.84	220	None	Brown	Moderate
WC3	6.85	301	None	Clear	None
WC3A	7.17	113	Sulfur	Clear	None
WC3B	7.17	159	None	Lt. brown	Slight
WC3C	6.76	116	Sulfur	Clear	None
WC4	6.70	152	Metallic	Clear	Slight
WC4 dup	6.74	155	Metallic	Clear	Slight
WC4A	6.67	170	Musty	Brown	Moderate
WC5	6.79	154	None	Clear	None
WC5A	6.46	197	None	Lt. brown	Slight
WC6	7.02	136	None	Lt. brown	Slight
WC6A	6.89	210	Chemical	Brown	Moderate
WC7	6.95	158	None	Clear	None
WC7A	7.26	223	Sulfur	Brown	Very
MW7A	6.95	171	None	Clear	None
MW10A	6.42	483	None	Clear	Slight
MW10B	7.03	318	None	Clear	None
MW10B dup	7.04	318	None	Clear	None
MW11	6.23	280	None	Clear	None
MW13	6.68	570	None	Clear	None
WW5	5.96	500	None	Lt. brown	Moderate
WW6	6.81	166	None	Lt. gray	Slight
WW7	6.34	320	None	Clear	None
WW7 dup	6.43	320	None	Clear	None
FVD1	6 <b>.</b> 23	210	Fuel oil	Clear	Sliaht

.

## WAUSAU NPL EAST WELLS ROUND 1 (SEPT. - OCT. 1987) (Continued)

•

.

• •

<u>Well #</u>	рН	Conductivty at 25°	<u>Odor</u>	<u>Color</u>	<u>Turbidity</u>
FVD2	6.16	210	Fuel oil	Dk. brown	Very
FVD5	6.17	256	Fuel oil	Clear	None
FVD7	5.98	246	Musty	Lt. brown	Slight
FVD7 dup	5.98	246			
GM5D	6.47	340	None	Clear	Slight
GM6D	6.72	267	None	Clear	Slight
GM7D	6.52	407	None	Clear	None
GM8D	6.92	145	None	Clear	Moderate
GM9S	6.28	392	None	Clear	None
Pumping We	<u>ells</u>				
CW3	6.80	225	None	Clear	None
CW4			None	Clear	None
Wergin	6.88	151	None	Rusty	Moderate
<u>Blanks</u>					
SB01	6.23	<10	None	Clear	None
SB02	6.93	<10	None	Clear	None
SB03	7.00	<10	None	Clear	None
SB04	6.00	<10	None	Clear	None
SB05	6.95	<10	None	Clear	None
SB06	7.60	<10	None	Clear	None

SGW2/kam/CSR [kam-400-50c]

•



PROJECT: WAUSAU NPL	CK'D: CAWI APP'D: CSR
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: コーパーS 8
C#: 13076.30	PAGE 1 OF 10
INORGANIC RESULTS	

COMODUND (MC/I)	WE-66M4S-01	WE-66M40-01	WE-GPDTW-01	WE-6W7-01	WE-6W38-01	WE-6W3A-01	WE-6W1A-01
LUMPUVND (MG/L)	09/29/8/	09/29/8/	09/29/8/	09/29/8/	09/29/8/	09729787	09/29/8/
	38232228332 ,	38222222223				3222222222	
CALCIUM	10.32	22.58	23.22	25.74	14.94	16.22	47.29
POTASSIUM	0.48 J	0.46 J	0.57 J	4.86 J	0.44 J	1.14 J	1.40 J
MAGNESIUM	3.32	7.97	9.85	8.06	5.76	2.88	1.25
SODIUM	3.32	3.23	5.97	18.95	3.65	3.63	3.36
IRON	0.13 B	0.05 B	0.18 B	0.09 B	0.08 B	0.09 B	0.05 B
CHLORIDE	4.20	3.60	3.10	79.00	6.00	5.60	5.50
TOTAL ORGANIC CARBON	2.50 J	2.00	2.00 UJ	2.00 UJ	4.40 J	6.00 J	2.00 UJ
TOTAL KJELDAHL NITROGEN	0.10	0.20	0.10 U	0.10	0.20	0.70	0.10
SULFATE	7.70	5.00 U	13.00	21.00	13.00	5.00 U	5.00
ALKALINITY	40.00	92.00	106.00	34.00	54.00 <sup>.</sup>	64.00	71.00
NITRATE + NITRITE NITROGEN	0.10 U	0.10 U	1.00	1.70	0.10 U	0.10 U	0.10 U
AMMONIA NITROGEN	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U	0.40	0.10 U

U = ANALYZED. BUT NOT DETECTED.

J = ESTIMATED VALUE.

B = COMPOUND ALSO DETECTED IN BLANK.



PROJECT: WAUSAU NPL	CK'D: CAW APP'D: CSR
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2-16-88
C#: 13076.30	PAGEZ OF 10
INORGANIC RESULTS	THUC - U

	WE-66M1S-01	WE-6W4B-01	₩E-6₩4A-01	WE-6W4A-01	₩E-SB01-01	WE-6C40-01	WE-66M1S-91
COMPOUND (MG/L)	09/29/87	09/29/87	09/29/87	09/29/87	09/29/87	09/29/87	09/29/87
		38888822222		=======	2222233233		
A1 A118	40 C4	00 70	17 OF	74 00	4 OF	74 75	
LALVION	13.31	20.39	13.93	31.28	0.25	31./3	14.0/
POTASSIUM	5.14 J	2.25 J	1.57 J	0.77 J	0.01 J	1.14 J	5.11 J
MAGNESIUM	3.97	5.70	3.33	11.48	0.04	8.19	3.73
SODIUM	3.16	11.99	16.31	11.26	0.28	9.37	3.14
IRON	0.05 B	0.18 B	0.07 B	0.29 B	0.05 B	0.05 B	0.05 B
CHLORIDE	5.30	36.00	48.00	51.00	0.50 U	33.00	5.40
TOTAL ORGANIC CARBON	2.00 UJ	2.00 UJ	2.00 UJ	2.00 UJ	2.00 UJ	2.00 UJ	2.00 UJ
TOTAL KJELDAHL NITROGEN	0.20	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U	0.20
SULFATE	13.00	15.00	10.00	14.00	5.00 U	30.00	14.00
ALKALINITY	40.00	39.00	28.00	88.00	2.30	45.00	39.00
NITRATE + NITRITE NITROGEN	2.50	0.70	0.70	0.20	0.10 U	9.20	2.50
AMMONIA NITROGEN	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U

. .

١

U = ANALYZED. BUT NOT DETECTED.



PROJECT: WAUSAU NPL	CK'D: CAW APP'D: CSR
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2.16-88
C#: 13076.30	PAGES OF 10
INORGANIC RESULTS	

COMPOUND (MG/L)	WE-GR1D-01 09/30/87	WE-6R1S-01 09/30/87	HE-66M5D-01 09/30/87	WE-66M6D-01 09/30/87	WE-66M9S-01 09/30/87	WE-GHW11-01 09/30/87	WE-SB03-01 09/30/87
**************	101100000						
CALCIUM	23.78	19.72	34.73	26.32	20.05	28.19	0.22
POTASSIUN	1.18 J	6.78 J	0.73 J	0.67 J	4.75 J	3.08 J	0.01 UJ
MAGNESIUM	7.45	6.22	13.98	10.57	3.94	7.25	0.03
SODIUM	10.15	13.54	6.82	5.74	46.29	14.61	0.22
IRON	0.05 B	0.05 B	0.10 B	0.06 B	0.05 B	5.23 B	0.05 B
CHLORIDE	25.00	69.00	79.00	54.00	68.00	69.00	0.50 V
TOTAL ORGANIC CARBON	2.00 UJ	2.00 UJ	2.00 UJ	2.00 UJ	2.10 J	2.00 UJ	2.00 UJ
TOTAL KJELDAHL NITROGEN	0.10 J	0.30 J	0.20 J	0.10 UJ	0.30 J	0.30 J	0.10 UJ
SULFATE	29.00	30.00	31.00	23.00	31.00	27.00	5.00 U
ALKALINITY	39.00	47.00	50.00	43.00	45.00	27.00	2.40
NITRATE + NITRITE NITROGEN	6.80	4.20	1.20	0.70	1.90	1.00	0.10 U
AMMONIA NITROGEN	0.10 U	0.10 U	0.10 U	0.10 U	0.10 U	0.10	0.10 U

•

U = ANALYZED, BUT NOT DETECTED.

٠



.

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT: WAUSAU NPL	CK'D: OAW APP'D: CSC
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2-1 <b>6</b> -88
C#: 13076.30	PAGE 4 DE 10
INORGANIC RESULTS	

.

	WE-6W9-01	₩E-6R30-01	WE-6R3S-01	WE-66M8D-01	WE-66M70-01	WE-6WW7-01	WE-6CW3-01
COMPOUND (HG/L)	09/30/87	09/30/87	09/30/87	09/30/87	09/30/87	09/30/87	09/30/87
		35288388228					
CALCIUM	16.37	22.06	16.31	13.97	46.29	33.56	20.97
POTASSIUM	1.48 J	0.69 J	2.38 J	0.48 J	0.72 J	2.10 J	1.29 J
MAGNESIUM	6.73	9.18	4.58	4.82	19.60	6.30	5.87
SODIUM	15.08	7.06	9.68	3.43	6.93	13.00	8.42
IRON	15.04 B	0.10 B	2.09 B	0.18 B	0.14 B	0.05 B	1.58 8
CHLORIDE	56.00	33.00	26.00	39.00	49.00	67.00	23.00
TOTAL ORGANIC CARBON	2.00 U.	I 2.00 UJ	5.80 J	4.50 J	2.00 UJ	2.00 J	3.30 J
TOTAL KJELDAHL NITROGEN	0.30 J	0.20 J	0.60 J	0.20 J	0.10 J	0.20 J	0.70 J
SULFATE	21.00	24.00	11.00	5.70	53.00	14.00	13.00
ALKALINITY	27.00	36.00	55.00	65.00	126.00	62.00	71.00
NITRATE + NITRITE NITROGEN	0.10 U	0.80	0.10 U	0.10 U	. 0 <b>.1</b> 0 V	0.20	0.60
AMMONIA NITROGEN	0.10	0.10 U	0.10 U	0.10 .	0.10	0.10 U	0.40

•

U = ANALYZED. BUT NOT DETECTED.

٠



.

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT:HAUSAU NPLCK'D:CAW APP'D:CSRLOCATION:HAUSAU, HISCONSINDATE ISSUED:2-16-88C#:13076.30PAGE 5 OF 10INORGANIC RESULTSPAGE 5 OF 10

COHPOUND (HG/L)	WE-GR1D-91 09/30/87	WE-SB02-01 09/30/87	WE-6CW6-10 09/30/87	WE-GCW7-01 09/30/87	WE-6CW9-10 09/30/87	WE-GMW7A-01 09/30/87	WE-6MW13-01 10/01/87
	1222233322					2222222222	2222222222
CALCIUM	23.36	0.21	16.00	14.44	16.04	20.40	47.09
POTASSIUM	1.24 J	0.01 VJ	0.90 J	0.68 J	0.68 J	0.54 J	4.57
MAGNESIUM	7.43	0.03	5.49	4.91	5.53	6.33	10.44
SODIUM	10.59	0.22	5.35	3.75	6.88	3.48	27.44
I RON	0.05 B	0.05 B	1.04 B	0.47 B	0.28 8	0.06 B	9.06
CHLORIDE	41.00	0.50 U	29.00	6.60	8.70	6.90	127.00
TOTAL ORGANIC CARBON	2.00 UJ	2.00 UJ	2.60 J	3.00 J	2.00 UJ	2.00 UJ	2.10
TOTAL KJELDAHL NITROGEN	0.10 J	0.10 UJ	0.30 J	0.30	0.10	0.10	2.30
SULFATE	28.00	5.00 U	7.70	8.00	14.00	11.00	26.00
ALKALINITY	39.00	2.00 U	59.00	59.00	60.00	74.00	87.00
NITRATE + NITRITE NITROGEN	6.40	0.10 U	0.20	0.10 U	0.70	0.10 U	0.10 U
AMMONIA NITROGEN	0.10 U	0.10 U	0.10 U	0.10	0.10 U	0.10 U	2.00

•

U = ANALYZED, BUT NOT DETECTED.

J = ESTIMATED VALUE.

•

B = COMPOUND ALSO DETECTED IN BLANK.



PROJECT: WAUSAU NPL	CK'D: DAW APP'D: C.S.R
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2-16-88
C#: 13076.30	PAGE GOF 10
INORGANIC RESULTS	

	WE-6MW13-01	WE-6WW7-91	WE-GHW10A-01	WE-6MW108-01	WE-6C2S-01	WE-6R4D-01	WE-6R2S-01
COMPOUND (MG/L)	10/01/87	09/30/87	10/01/87	10/01/87	10/01/87	10/01/87	10/01/87
							*********
	<i>1</i> 7 A0	70 04	AO 8A	70.04	78 24	27 07	45 70
UNLVIVN DOTAGOTUH	4/.07	32.74	47.04	JV.71	JO.20	20107	12.17
PUTASSIUM	4.3/ J	Z.14 J	J.61 J	1.44 J	1.30 J	1.48 J	2.16 J
MAGNESIUM	10.44	6.26	10.60	8.61	9.34	14.27	4.82
SODIUM	27.44	13.33	12.88	3.66	14.55	11.58	5.40
IRON	9.06 B	0.08 B	1.79 8	7.77 8	0.09 B	0.07 B	0.21 B
CHLORIDE	127.00	59.00	93.00	46.00	60.00	64.00	15.00
TOTAL ORGANIC CARBON	2.10 J	2.00 UJ	2.00 VJ	5.00 J	2.00 UJ	2.00 UJ	2.00 UJ
TOTAL KJELDAHL NITROGEN	2.30	0.20	0.20	1.00	0.20	0.30	0.20
SULFATE	26.00	15.00	24.00	16.00	22.00	33.00	8.70
ALKALINITY	87.00	64.00	84.00	97.00	48.00	41.00	53.00
NITRATE + NITRITE NITROGEN	0.10 U	0.20	0.80	0.10 U	11.00	2.80	0.20
AMMONIA NITROGEN	2.00	0.10 U	0.10 U	0.80	0.10 U	0.10 U	0.10

.

1.

.

U = ANALYZED, BUT NOT DETECTED. J = ESTIMATED.VALUE. B = COMPOUND ALSO DETECTED IN BLANK. •



PROJECT: WAUSAU NPL	CK'D: CAN APP'D: CSR
LOCATION: WAUSAV, WISCONSIN	DATE ISSUED: 2-16-58
C#: 13076.30	DAGE TOF 10
INORGANIC RESULTS	FRUE CO.

.

	WE-6R2D-01	WE-6FVD2-01	WE-6FVD1-01	WE-6MV05-01	WE-6MW108-01	WE-SB04-01	WE-GFV07-01
COMPOUND (MG/L)	10/01/87	10/01/87	10/01/87	10/01/87	10/01/87	10/01/87	10/01/87
	=========	111111111111		*********			
CAI 07118	<b>37 8</b> 6	10 00	40 44	04 70	71 15	A 99	07 00
CALCIVA	23.00	19.02	10.44	21.37	31.63	0.22	27.02
PUTASSIUM	0.85 J	2.21 J	1.97 J	1.99 J	1.44 J	0.01 UJ	3.44 J
MAGNESIUM	11.22	3.09	3.69	3.28	8.77	0.04	4.46
SODIUM	6.34	5.37	5.13	5.60	3.63	0.30	9.36
IRON	0.06 B	23.07 B	15.41 B	26.58 B	7.70 B	0.07 B	0.06 B
CHLORIDE	47.00	15.00	16.00	29.00	44.00	0.50 U	11.00
TOTAL ORGANIC CARBON	2.00 UJ	20.00 J	4.10 J	5.60 J	5.00 J	2.00 UJ	3.80 J
TOTAL KJELDAHL NITROGEN	0.10 U	5.10	0.80	0.60	1.10	0.10 U	0.50
SULFATE	33.00	17.00	14.00	23.00	16.00	5.00 U	45.00
ALKALINITY	48.00	46.00	73.00	77.00	96.00	2.00 U	58.00
NITRATE + NITRITE NITROGEN	0.10 V	0.10	0.10	0.10 U	0.10 U	0.10 U	1.40
AMMONIA NITROGEN	0.10 U	0.70	0.30	0.40	0.80	0.10 U	0.10 U

U = ANALYZED. BUT.NOT DETECTED. J = ESTIMATED VALUE.

B = COMPOUND ALSO DETECTED IN BLANK.

يەت ئىر كەر يەت



•

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

.

PROJECT: WAUSAU NPL	CK'D: BAW APP'D: CSR
LOCATION: WAUSAU, WISCONSIN	که کار د : DATE ISSVED: مار د Si
C#: 13076.30	PAGE & DF 10
INORGANIC RESULTS	

•

	WE-6FVD7-91	#E-S805-01	#E-G##6-01	WE-GWERG-01	WE-6WW5-01	₩E-6₩C4-01	HE-GHC4A-01
COMPOUND (M6/L)	10/01/87	10/01/87	10/01/87	10/01/87	10/06/87	10/06/87	10/06/87
=========	===========	=======					
CALCIUM	26.66	0.23	16.19	16.77	32.40	14.07	13.93
POTASSIUM	3.45 J	0.01 UJ	1.65 J	0.73 J	1.59 J	0.77 J	1.04 J
MAGNESIUM	4.43	0.03	3.87	4.56	9.03	3.36	5.16
SODIUN	9.18	0.28	3.80	3.16	42.46	4.44	7.93
IRON	0.06 B	0.05 B	0.55 B	0.25 B	0.05 8	8.36 B	7.91 B
CHLORIDE	8.90	0.50 U	5.40	6.40	127.00	10.00	13.00
TOTAL ORGANIC CARBON	4.00 J	2.00 UJ	6.90 J	7.90 J	2.00 UJ	6.60 J	5.00 J
TOTAL KJELDAHL NITROGEN	0.30	0.10 U	0.90	1.00	0.50	1.30	0.50
SULFATE	45.00	5.00 U	8.20	6.70	31.00	11.00	12.00
ALKALINITY	57.00	2.40	67.00	73.00	32.00	61.00	61.00
NITRATE + NITRITE NITROGEN	1.30	0.10 U	0.10 U	0.10 U	6.10	0.10 U	0.10 U
AMMONIA NITROGEN	0.10 U	0.10 U	0.60	0.20	0.10 U	1.00	0.20

U = ANALYZED, BUT NOT DETECTED.



..

PROJECT: WAUSAU NPL	CK'D: CAW APP'D: CSR
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: ג -16-8-8
C#: 13076.30	PAGES DELO
INORGANIC RESULTS	

,

COMPOUND (MG/L)	WE-6WC7-01	WE-6WC7A-01	WE-GWC3C-01	HE-6HC3-01	WE-6WC3A-01	WE-6WC2-01	WE-6WC5-01
				=======		=======	
CALCIUM	14.65	32.01	11.33	35.13	11.43	10.13	15.47
POTASSIUM	0.87 J	1.24 J	0.79 J	0.82 J	0.91 J	1.24 J	1.19 J
MAGNESIUM	4.35	4.57	2.80	13.68	2.45	2.78	3.16
SODIUM	3.86	8.26	3.56	12.23	3.15	9.00	4.03
IRON	9.43 B	3.04 B	5.88 B	0.17 B	6.14 B	18.87 8	3.96 8
CHLORIDE	11.00	17.00	4.70	46.00	4.00	12.00	6.40
TOTAL ORGANIC CARBON	7.00 J	8.50 J	6.00 J	2.00 UJ	6.60 J	12.00 J	7.20 J
TOTAL KJELDAHL NITROGEN	1.60	2.10	1.10	0.10	1.10	1.90	1.20
SULFATE	11.00	5.00 U	11.00	35.00	9.40	6.30	6.80
ALKALINITY	61.00	136.00	46.00	106.00	52.00	61.00	6 <b>9.</b> 00
NITRATE + NITRITE NITROGEN	0.10 U	0.10 U	0.10 U	0.50	0.10 U	0.20	0.10 U
AMMONIA NITROGEN	1.00	1.10	0.80	0.10 U	0.90	1.00	1.20

U = ANALYZED. BUT NOT DETECTED.



١

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

.

PROJECT: WAUSAU NPL	CK'D: GAW APP'D: CSR
LOCATION: WAUSAV, WISCONSIN	DATE ISSUED: 2-16-88
C#: 13076.30	PAGE 10 DE 10
INORGANIC RESULTS	

	WE-GWC5A-01	WE-6WC3B-01	WE-6WC6-01	WE-GWC6A-01	WE-6WC4-91	WE-SB06-01
COMPOUND (MG/L)	10/07/87	10/07/87	10/07/87	10/07/87	10/07/87	10/07/87
2222222332268222				************		
CALCIUM	12.76	10.39	10.09	16.04	14.14	0.19
POTASSIUN	1.02 J	0.91 J	0.70 J	1.89 J	0.78 J	0.01 UJ
MAGNESIUM	4.57	2.44	1.97	3.23	3.38	0.03
SODIUM	4.72	4.40	3.57	7.76	4.38	0.17
IRON	16.02 B	9.02 B	7.66 8	16.72 B	8.60 B	0.11 B
CHLORIDE	9.20	6.60	5.90	9.70	10.00	0.50 V
TOTAL ORGANIC CARBON	9.50 J	10.00 J	9.40 J	12.00 J	6.00 J	2.00 UJ
TOTAL KJELDAHL NITROGEN	1.50	1.90	1.20	1.10	1.20	0.10 U
SULFATE	15.00	13.00	13.00	13.00	11.00	5.00 U
ALKALINITY	62.00	48.00	43.00	72.00	60.00	2.00 U
NITRATE + NITRITE NITROGEN	0.10	0.10	0.10 U	0.10 U	0.10 U	0.10 U
AMMONIA NITROGEN	0.90	0.90	1.00	0.60	1.10	0.10 U

U = ANALYZED, BUT NOT DETECTED.

J = ESTIMATED VALUE. B = COMPOUND.ALSO DETECTED IN BLANK.

## APPENDIX F

.

. .

# RESULTS OF ROUND 1 VOLATILE ORGANIC COMPOUND ANALYSES



.

.

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

. .

~

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS		CK'D:CA DATE IS PAGE I	CK'D:CAW APP'D: CSR DATE ISSUED: 1-20-80 PAGE I OF 13							
COMPOUND	REPORTABLE Detection Limit (VG/L)	WE-66M4D-01 09/29/87	WE-GPDTW-01 09/29/87	WE-GW7-01 09/29/87	WE-6W3B-01 09/29/87	WE-6W3A-01 09/29/87	₩E-6₩1A-01 09/29/87	WE-66M1S-01 09/29/87		
CHLOROMETHANE BROMOMETHANE VINYL CHLORIDE CHLOROETHANE METHYLENE CHLORIDE ACETONE CARBON DISULFIDE 1, 1-DICHLOROETHENE 1, 1-DICHLOROETHENE TRANS-1, 2-DICHLOROETHENE CHLOROFORM 1, 2-DICHLOROETHANE 2-BUTANONE 1, 1, 1-TRICHLOROETHANE 2-BUTANONE 1, 1, 1-TRICHLOROETHANE CARBON TETRACHLORIDE VINYL ACETATE BROMODICHLOROMETHANE 1, 2-DICHLOROPROPANE TRANS-1, 3-DICHLOROPROPENE TRICHLOROETHENE DIBROMOCHLOROMETHANE 1, 1, 2-TRICHLOROETHANE 8ENZENE cis-1, 3-DICHLOROPROPENE 2-CHLOROETHYLVINYLETHER BROMOFORM 4-METHYL-2-PENTANONE 2-HEXANONE TETRACHLOROETHENE TOLUENE CHLOROBENZENE ETHYLBENZENE STYRENE	$\begin{array}{c} 10.0\\ 10.0\\ 10.0\\ 10.0\\ 1.5\\ 1.0\\ 7.5\\ 3.0\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5$			••••••••••••••••••••••••••••••••••••••	UJ 8	UJ 5	UJ 6	UJ 4		
ACROLEIN ACRYLONITRILE	2.5 150.0 150.0									



PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C&: 13076.23 ORGANIC RESULTS		CK'D: <i>C</i> Date IS Page 2	CK' D: CAW APP' D: CSR DATE ISSUED: 1-28-88 PAGE 2 OF 13-								
COMPOUND	REPORTABLE Detection Limit (UG/L)	WE-6W4B-01 09/29/87	WE-6W4C-01 09/29/87	¥E-6¥4A-10 09/29/87	WE-SB01-01 09/29/87	WE-GC4D-01 09/29/87	HE-66M1S-91 09/29/87	WE-TB01-01 09/29/87			
CHLOROMETHANE BROMOMETHANE VINYL CHLORIDE CHLOROETHANE METHYLENE CHLORIDE	10.0 10.0 10.0 1.5 1.0	2		2	UJ 4	UJ 1	UJ 1	UJ 3			
ACETONE CARBON DISULFIDE 1, 1-DICHLOROETHENE 1, 1-DICHLOROETHANE TRANS-1, 2-DICHLOROETHENE	7.5 3.0 1.5 1.5 1.5	UJ 9	NT 3	₩J- <u>8</u>		9					
CHLOROFORM 1, 2-DICHLOROETHANE 2-BUTANONE 1, 1, 1-TRICHLOROETHANE CARBON TETRACHLORIDE VINYL ACETATE DEPENDENCE ORDETHANE	1.5 1.5 50.0 1.5 1.5 15.0				J 1			7			
1, 2-DICHLOROPROPANE TRANS-1, 3-DICHLOROPROPANE TRICHLOROETHENE DIBROMOCHLOROMETHANE 1, 1, 2-TRICHLOROETHANE BENZENE	1.5 1.5 1.5 1.5 1.5 1.5 1.5	J 1				34					
CIS-1, J-DICHLOROPROPENE 2-CHLOROETHYLVINYLETHER BROMOFORM 4-METHYL-2-PENTANONE 2-HEXANONE TETRACHLOROETHENE TETRACHLOROETHENE	2.0 1.5 3.0 50.0 3.0	-		. ,	.,	.,					
CHLOROBENZENE CHLOROBENZENE STYRENE TOTAL XYLENES ACROLEIN ACRYLONITRILE	1.5 1.5 1.0 2.5 150.0 150.0	د	J 1	J 1	J 1			2			



PROJECT: WAUSAU NPL (K'D: CAW APP'D: CSIZ LOCATION: WAUSAU, WISCONSIN DATE ISSUED: 1-28-88 C#: 13076.23 PAGE 3 OF 13 ORGANIC RESULTS REPORTABLE DETECTION LIMIT WE-GRID-01 WE-GRIS-01 WE-GGM5D-01 WE-GGM6D-01 WE-GGM9S-01(2) WE-GMW11-01 COMPOUND (UG/L)09/30/87 09/30/87 09/30/87 09/30/87 09/30/87 09/30/87 332322222222 =========== -----CHLOROMETHANE 10.0 BROMOMETHANE 10.0 VINYL CHLORIDE 10.0 CHLOROETHANE 1.5 UJ 2 UJ 3 METHYLENE CHLORIDE 1.0 UJ 2 WJ 1 UJ 200 UJ 3 ACETONE 7.5 J 7 J 6 CARBON DISULFIDE 3.0 1, 1-DICHLOROETHENE 1.5 1, 1-DICHLOROETHANE 1.5 TRANS-1, 2-DICHLOROETHENE 1.5 J1 **CHLOROFORM** 1.5 1, 2-DICHLOROETHANE 1.5 2-BUTANONE 50.0 1, 1, 1-TRICHLOROETHANE 1.5 CARBON TETRACHLORIDE 1.5 VINYL ACETATE 15.0 BROMODICHLOROMETHANE 1.5 1, 2-DICHLOROPROPANE 1.5 TRANS-1, 3-DICHLOROPROPENE 1.0 TRICHLOROETHENE 1.5 10 2 J 1 DIBROMOCHLOROMETHANE 1.5 1, 1, 2-TRICHLOROETHANE 1.5 BENZENE 1.5 cis-1, 3-DICHLOROPROPENE 2.0 2-CHLOROETHYLVINYLETHER 1.5 BROMOFORM 1.5 4-METHYL-2-PENTANONE 3.0 2-HEXANONE 50.0 TETRACHLOROETHENE 3.0 J 2440 16 TOLVENE 1.5 4 5 CHLOROBENZENE 1.5 ETHYLBENZENE 1.5 STYRENE 1.0 TOTAL XYLENES 2.5 ACROLEIN 150.0 ACRYLONITRILE 150.0



.

PROJECT: WAUSAU NPL LOCATION: HAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS

· .

CK'D: CAW APP'D: CSR DATE ISSUED: 1-28-88 PAGE 4 OF 13

COMPOUND	REPORTABLE Detection Limit (UG/L)	WE-SB03-01 09/30/87	₩E-6₩9-01 09/30/87	WE-GR3D-01 09/30/87	₩E-GR3S-01 09/30/87	WE-66M8D-01 09/30/87	WE-66M7D-01 09/30/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0						
CHLOROETHANE	1.5						
METHYLENE CHLORIDE	1.0	VJ 2	VJ 2	UJ 2	VJ 1	UJ 1	UJ 2
ACETONE	7.5						
CARBON DISULFIDE	3.0						
1, 1-DICHLURUEIHENE	1.5						
	1.5				~		•
CULODOCODM	1.7	<b>A</b> 1			Z		2
4 2_010URN *	1.0	10					
2-BUITANONE	1.J 50 0						
	15						
CARBON TETRACHI ORIDE	1.5						
VINVL ACETATE	15.0						
BROMODICHLOROMETHANE	1.5						
1, 2-DICHLOROPROPANE	1.5						
TRANS-1, 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5			7	J 33		5
DIBROMOCHLOROMETHANE	1.5						
1, 1, 2-TRICHLOROETHANE	1.5						
BENZENE	1.5						
	2.0						
	1.7						
DAUNUFUAN A-METNVI -2-DENTANOME	1.) 7 û						
2-HEYANONE	50.0						
	3.0	2					2
	1.5	2					£
CHLOROBENZENE	1.5	-					
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5						
ACROLEIN	150.0						
ACRYLONITRILE	150.0						



PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C0: 13076.23 Organic Results

.

CK'D: VAND APP'D: CSR DATE ISSUED: 1-28-85 PASE 5 OF 13

COMPOUND	REPORTABLE Detection Limit (UG/L)	WE-6WW7-01 09/30/87	WE-6CW3-01 09/30/87	WE-GR1D-91 09/30/87	WE-SB02-01 09/30/87	WE-6CW6-10 09/30/87	WE-GCW7-01 09/30/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0						
CHLOROETHANE	1.5						
METHYLENE CHLORIDE	1.0	UJ 4	UJ 6	VJ 5	UJ 2	VJ 2	VJ 3
ACETONE	7.5		J 16		UJ 6		UJ 9
CARBON DISULFIDE	3.0						
1, 1-DICHLOROETHENE	1.5						
1. 1-DICHLOROETHANE	1.5						
TRANS-1, 2-DICHLOROETHENE	1.5	3	6				
CHLOROFORM	1.5			J 1	J 25		
1. 2-DICHLOROETHANE	1.5						
2-BUTANONE	50.0						
1, 1, 1-TRICHLOROETHANE	1.5						
	1.5						
	15.0						
	1.5						
	1.3						
TAICH ODOCTUCNE	1.0	E	1 (0			• • • •	
	1.)	2	J 67			j 116	
	1.0						
IT IT ZTINICHLURUCINANC DENTENE	1.3						
CIRCULAR CONCENT	2.0						
2_/UI ADACTUVI VINVI CTUCD	4 5						
2 CHEDROCHTTEVINTEETHER RRAMAEARM	1.5						
4-HETHVI -7-PENTANONE	7.0						
2-HEYANONE	50.0						
	3.0	55	10				
	1.5		4	3	I f	2	
CHI OROBEN7ENE	1.5		,	0	<b>U</b> 1	-	
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5						
ACROLEIN	150.0						
ACRYLONITRILE	150.0						
HVHILVHIIHILL	19444						



.

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C≇: 13076.23 ORGANIC RESULTS CK'D: CAN APP'D: CSA DATE ISSUED: 1-28-88 PAGE 6 OF 13

COMPOUND	REPORTABLE Detection Limit (VG/L)	WE-6CW9-01 09/30/87	WE-TB02-01 09/30/87	WE-6HW13-01 10/01/87	WE-6WW7-91 09/30/87	WE-GMW10A-01 10/01/87	WE-6MW10B-01 10/01/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0						
CHLOROETHANE	1.5						
METHYLENE CHLORIDE	1.0	UJ 4	UJ 2	UJ 1	UJ 2	VJ 4	UJ 4
ACETONE	7.5	VJ 13		UJ 4	UJ 20		
CARBON DISULFIDE	3.0						
1. 1-DICHLURUEIHENE	1.5						
1. 1-DICHLURUEIHANE	1.5				-		<i></i>
INANG-1, Z-VICHLUKUEIHENE	1.3		T 00		3		70
UNLURUFURN 4 - 2-51000 0000 TUANE	1.0		J 20				
2-DITANONE	1.J . 50 0						•
	45		ł				
	1.5						
VINVI ACFTATE	15.0						
BROMODICHI OROMETHANE	1.5		11				
1, 2-DICHLOROPROPANE	1.5		• •				
TRANS-1, 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5			J 1	6		10
DIBROMOCHLOROMETHANE	1.5						
1. 1, 2-TRICHLOROETHANE	1.5						
BENZENE	1.5						
cis-1, 3-DICHLOROPROPENE	2.0						
2-CHLOROETHYLVINYLETHER	1.5						
BROMOFORM	1.5						
4-METHYL-2-PENTANONE	3.0						
2-HEXANONE	50.0						
	3.0	-		4	J 37	2	J <u>3</u> 3
	1.5	2	2	J 1		4	j.
	1.7						
	1.3						
JITACHC TATAL YVIENEG	1.V 2.5						
ACRAI FIN	150.0						
ACRYLONITRILF	150.0						
	* # ¥ # V						



PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'D: CAWAPP'D: CSP DATE ISSUED: 1-28-88 PAGE 7 OF 13

COMPOUND	REPORTABLE Detection Limit (VG/L)	WE-6C2S-01(3) 10/01/87	WE-6R4D-01 10/01/87	WE-GR4D-01(1) 10/01/87	WE-6R2S-01 10/01/87	WE-GR2D-01(2) 10/01/87	WE-GFV02-01(2) 10/01/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0						
CHLOROETHANE	1.5						
METHYLENE CHLORIDE	1.0	UJ 270	VJ 2	VJ 170	VJ 1	UJ 190	UJ 220
ACETONE	7.5	UJ <b>300</b> 0			UJ 9		VJ 2010
CARBON DISULFIDE	3.0						
1, 1-DICHLOROETHENE	1.5						
1, 1-DICHLOROETHANE	1.5						
IRANS-1, 2-DICHLOROETHENE	1.5		198	169	J 1		
	1.5		J 1				
1, Z-DICHLUKUEIHANE	1.5					•	
	30.0		•				
ADDON TETDACHLONUEIMARE	1.)						
UTANDON TETRAUNLURIVE	1.3						
RBURUNICHI UBURETNANE	12.0						
1. 2-DICHLORODERNAME	45						
TRANS-1. 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5	1370	388	870	J 54	1020	
DIBROMOCHLOROMETHANE	1.5						
1, 1, 2-TRICHLORDETHANE	1.5						
BENZENE	1.5						250
cis-1, 3-DICHLOROPROPENE	2.0						
2-CHLOROETHYLVINYLETHER	1.5						
BROMOFORM	1.5						
4-METHYL-2-PENTANONE	3.0						
2-HEXANUNE	50.0		_				
	5.0		5		• /		
	1.5				J 1		
	1.3						
EINILBEN/ENE CTVDENE	1.3						
DITACHE TATAL VVIENCE	1.0						70/
ACONIFIN	2.J 450 A						(70
ACRVI ONITRII F	150.0						
NUNILUNIINILL	A SA MARK						

•



PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS

REPORTABLE

•

CK'D: CAN APP'D: CSR DATE ISSUED: 1-28-88 PAGE 8 OF 13

	DETECTION						
20M0011NA		WE-6FV01-01	HE-6AVU5-01	HE-6MH108-01	4E-5804-01	WE-6FV07-01	HE-6FV07-91
CUMPUVAV	(V0/L)	10/01/0/	10/01/6/	10/01/0/	10/01/0/	10/01/0/	10/01/6/
CHI NROMETHANE	10 0	**********					
RROMOMETHANE	10.0						
	10 0						
CHI OROFTHANE	15.0						
METHYLENE CHLORIDE	1.0	111 3	111.2	111 7	11T A	111 7	UT 2
ACETONE	7 5	00 0	1 3070	117 20	<b>UU</b> T		50 L
CARRON DISHIFTOF	3 0		0 0010	00 LV .			
1. 1-DICHLOROFTHENE	1.5						
	15						
TRANS-1, 2-DICHIOROFTHENE	1.5			T 86			
CHI OROFORM	1.5				1 22		
1. 2-DICHI ORDETHANE	1.5				JLL		
2-BUTANONE	50.0						
1. 1. 1-TRICHI OROFTHANE	1.5					٦	7
CARRON TETRACHIORIDE	1.5					5	5
VINYI ACETATE	15.0						
BROMODICHLOROMETHANE	1.5						
1. 2-DICHLOROPROPANE	1.5						
TRANS-1, 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5	2		14	2	19	18
DIBROMOCHLOROMETHANE	1.5				-		
1, 1, 2-TRICHLOROETHANE	1.5						
BENZENE	1.5	18					
cis-1, 3-DICHLOROPROPENE	2.0						
2-CHLOROETHYLVINYLETHER	1.5						
BROMOFORM	1.5						
4-METHYL-2-PENTANONE	3.0						
2-HEXANONE	50.0						
TETRACHLOROETHENE	3.0	J 23	19	J 40		J 94	J 90
TOLUENE ·	1.5			3	J 1	3	
CHLOROBENZENE	1.5						
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5	16	J 319				
ACROLEIN	150.0						
ACRYLONITRILE	150.0						



PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'DICAW APP'DICSR DATE ISSUEDI 1-28-88 PAGE 9 OF 13

· .

	REPORTABLE						
50H00HH6		¥E-S805-01	WE-T803-01	NE-6NN6-01	WE-GWERG-01	#E-G##5-01	WE-6WC4-01
	(06/L)	10/01/8/	10/01/8/	10/01/8/	10/01/8/	10/01/8/	10/06/8/
		========			29922222222	28222222323	
	10.0						
	10.0						
	10.0						
	1.7						
MEINTLENE CHLUKIVE	1.0	UJ 2	UJ Z	UJ 2	UJ 2	UJ 2	UJ 2
ACEIUNE	1.5		-	VJ 23		UJ 7	VJ 14
CARBUN DISULFIDE	3.0						
1, 1-UICHLURUEIHENE	1.5						
1. 1-DICHLOROETHANE	1.5						
TRANS-1, 2-DICHLOROETHENE	1.5	_		J 1			
CHLOROFORM	1.5	19	J 24	•		6	
1, 2-DICHLOROETHANE	1.5						
2-BUTANONE	50.0						
1, 1, 1-TRICHLOROETHANE	1.5						
CARBON TETRACHLORIDE	1.5						
VINYL ACETATE	15.0						
BROMODICHLOROMETHANE	1.5	J 1	Ji				
1, 2-DICHLOROPROPANE	1.5						
TRANS-1, 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5			J 1		J 1	
DIBROMOCHLOROMETHANE	1.5						
1, 1, 2-TRICHLOROETHANE	1.5						
BENZENE	1.5						
cis-1, 3-DICHLOROPROPENE	2.0						
2-CHLOROETHYLVINYLETHER	1.5						
BROMOFORM	1.5						
4-METHYL-2-PENTANONE	3.0						
2-HEXANONE	50.0						
TETRACHLOROETHENE	3.0			2			
TOLVENE ·	1.5	3	2	2		J 1	
CHLOROBENZENE	1.5						
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5						
ACROLEIN	150.0						
ACRYLONITRILE	150.0						



.

WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'D: CAWAPP'D: CSR DATE ISSUED: 1-28-88 PAGE IO OF 13

•

COMPOUND	REPORTABLE Detection Limit (UG/L)	WE-GWC4A-01 10/01/87	WE-6WC7-01 10/06/87	WE-6WC7A-01 10/06/87	WE-GWC3C-01 10/06/87	WE-6WC3-01 10/06/87	NE-6WC3A-01 10/06/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0						
CHLOROETHANE	1.5						
METHYLENE CHLORIDE	1.0	UJ 1	UJ 2	VJ 1	UJ 2	VJ 1	UJ 1
ACETONE	7.5	UJ 9	VJ 12		UJ 1	UJ 27	VJ 22
CARBON DISULFIDE	3.0						
1, 1-DICHLOROETHENE	1.5						
1, 1-DICHLOROETHANE	1.5						
TRANS-1, 2-DICHLURUETHENE	1.5						
	1.5						
1, 2-DICHLURUETHANE	1.5						
	50.0						
1, 1, 1-IKIUHLUKUEIHANE	1.5						
UTNYL ACETATC	1.3						
VIRTE AVEINIE DDOHOATCULODOMETUANE	12.0						
	1.3						
TPANC_4 T_ATAUADDODDDENE	1.2						
	4 5						
ATRICHEDROL MENE	112 45						
1. 1. 2-TRICHLOROFTHANE	1.5						
REN7ENF	1.5						
cis-1. 3-DICHLOROPROPENE	2.0						
2-CHLOROETHYLVINYLETHER	1.5						
BROMOFORM	1.5						
4-METHYL-2-PENTANONE	3.0						
2-HEXANONE	50.0						
TETRACHLOROETHENE	3.0						
TOLUENE ·	1.5		J 1		UJ 1		
CHLOROBENZENE	1.5						
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5						
ACROLEIN	150.0						
ACRYLONITRILE	150.0						


WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

•

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'D: CAW APP'D: CSI2 DATE ISSUED: 1-23-88 PAGE II OF13

COMPOUND	REPORTABLE Detection Limit (UG/L)	WE-GWC2-01(2) 10/07/87 ========	HE-GHC5-01 10/07/87	WE-GWC5A-01(1) 10/07/87	WE-GWC3B-01 10/07/87	WE-6WC6-01 10/07/87	WE-GWC6A-01 10/07/87
CHLOROMETHANE	10.0						
BROMOMETHANE	10.0						
VINYL CHLORIDE	10.0			•. •			J 4
	1.5			117 44			
	1.0	HT 400		VJ 11	UJ 1	VJ 1	VJ 1
AVEIUNE CADDON ATOMICTOC	1.3	VJ 48V	VJ 1	VJ 4/	VJ 7	Λî Q	0J 8
VARDUN UIGVLFIVE	J.V 4 5						
I I I VIVALURUCIACAL I ILAIAU ADACTUANC	1.3						
	1.2	784			A		40
	4 5	TÜL			T		VF
1. 2-DICHLOROFTHANE	1.5						
2-BUTANONE	50.0						
1, 1, 1-TRICHLOROETHANE	1.5						
CARBON TETRACHLORIDE	1.5						
VINYL ACETATE	15.0						
BROMODICHLOROMETHANE	1.5						
1, 2-DICHLOROPROPANE	1.5						
TRANS-1, 3-DICHLOROPROPENE	1.0						
TRICHLOROETHENE	1.5	180			4		9
DIBROMOCHLOROMETHANE	1.5						
1. 1. 2-IRICHLOROETHANE	1.5						
	1.5						
	Z.V 4 E						
Z-CUFOKOCIUITAITEIUEK BOURUEUDA	1.3						
A-HETHVI -7-PENTANONE	1.2						
2-HEYANONE	50.0						
	3.0	226		191	19		7
TOLUENE	1.5		J1	• / •	• :		2
CHLOROBENZENE	1.5						
ETHYLBENZENE	1.5						
STYRENE	1.0						
TOTAL XYLENES	2.5						
ACROLEIN	150.0						
ACKYLONITRILE	150.0						
•							



WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'D: CAW APP'D: CSR DATE ISSUED: 1-28-88 PAGE 12 DF 13

60480/105	REPORTABLE DETECTION LIMIT	HE-	-6WC4-91	WE-SB06-01	WE-TB04-01	WE-CWDS-01
CUMPUUND	(06/L)	1(	0/01/8/	10/0//8/	10/10/8/	10/10/8/
		==:				
	10.0					
	10.0					
	10.0					
VALURUEIAMINE METUVIENE AUIADINE	1.5	ei T	<b>•</b>			11 <b>.</b> 7
ACTONE VALUAIVE	1.0	0J 117	2	11 <b>7</b> A	117 4	UJ 1 HT A
AVELUNE CADDAN ATCHLETAE	(.) A T	VJ	21	VJ 4		VJ 1
4 4_DIAURODACTUC	3.0				UI LU	
	1.3					
	45					
CHI OBOEODM	4 5			45		1 54
1. 2-DICHLOROFTHANE	1.2			12		3 30
2-RIITANNNE	50 0					
1. 1. 1-TRICHLOROFTHANE	1.5					
CARBON TETRACHI ORIDE	1.5					
VINVI ACFTATE	15.0					
RROMODICHI OROMETHANE	1.5					4
1. 2-DICHLOROPROPANE	1.5					ł
TRANS-1, 3-DICHLOROPROPENE	1.0					
TRICHLOROETHENE	1.5					
DIBROMOCHLOROMETHANE	1.5					
1, 1, 2-TRICHLOROETHANE	1.5					
BENZENE	1.5			•		
cis-1, 3-DICHLOROPROPENE	2.0					
2-CHLOROETHYLVINYLETHER	1.5					
BROMOFORM	1.5					
4-METHYL-2-PENTANONE	3.0					
2-HEXANONE	50.0					
TETRACHLOROETHENE	3.0					
TOLUENE	1.5	J	1	J 1		J 1
CHLOROBENZENE	1.5					
ETHYLBENZENE	1.5					
SIYKENE	1.0					
IUIAL XYLENES	2.5					
ACKULEIN	150.0					
ACKYLUNIIKILE	150.0					



WARZYN ENGINEERING INC. • ONE SCIENCE COURT • UNIVERSITY RESEARCH PARK • P.O. BOX 5385 • MADISON, WISCONSIN 53705 • (608) 273-0440

PROJECT: WAUSAU NPL LOCATION: WAUSAU. WISCONSIN C#: 13076.23 ORGANIC RESULTS CK'D: CAWAPP'D: CSR DATE ISSUED: 1-28-88 PAGE 13 OF 13

(1) ANALYSIS PERFORMED ON A 1:10 DILUTION.
(2) ANALYSIS PERFORMED ON A 1:100 DILUTION.
(3) ANALYSIS PERFORMED ON A 1:200 DILUTION.

U = ANALYZED. BUT NOT DETECTED. J = ESTIMATED VALUE.

B = COMPOUND ALSO DETECTED IN BLANK.

### APPENDIX G

### RESULTS OF FIELD GAS CHROMATOGRAPH AND CONTRACT LABORATORY ANALYSES OF GROUNDWATER SAMPLES COLLECTED DURING DRILLING

G.1

1

CLP LAB RESULTS VOC SAMPLES COLLECTED DURING DRILLING

PROJECT: WAUSAU NPL	ck'd: Caw App'd: Kof
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2-16-88
C#: 13076.30	PAGE   OF 8
ORGANIC RESULTS	

COMPOUND	SW LAB DETECTION LIMIT (UG/L)	ENSECO DETECTION LIMIT (UG/L)	SW LAB WE-GE21-133 11/13/87	S₩ LAB ₩E-GE21-133-9 11/13/87	SW LAB WE-GE24-40 10/15/87	SW LAB WE-6E25-120 10/15/87	SW LAB WE-6E25-120-9 10/15/87
ΓΗΙ ΠΡΠΜΕΤΗΔΝΕ	1 0	5 Λ					
BROHOMETHANE	1.0	5.0					
	1.0	5.0			18.0		
CHLOROETHANE	1.0	1.0			1010		
METHYLENE CHLORIDE	1.0	5.0			0.6 /J		0.5 /.1
ACETONE	1.0	10.0		30.0			
CARBON DISULFIDE	1.0	1.0					
1.1-DICHLOROETHENE	1.0	1.0					
1,1-DICHLOROETHANE	1.0	1.0					
TRANS-1, 2-DICHLOROETHENE	1.0	1.0			3.8		
CHLOROFORM	1.0	1.0	0.7 B/UJ	0.7 B/UJ		6.4	5.0
1.2-DICHLOROETHANE	1.0	1.0					
2-BUTANONE	1.0	10.0					
1,1.1-TRICHLOROETHANE	1.0	1.0					
CARBON TETRACHLORIDE	1.0	1.0					
VINYL ACETATE	1.0	10.0					
BROMODICHLOROMETHANE	1.0	1.0					
1,2-DICHLOROPROPANE	1.0	1.0					
TRANS-1,3-DICHLOROPROPENE	1.0	1.0					
TRICHLOROETHENE	1.0	1.0	3.0	2.0		0.7 /J	0.6 /J
DIBROMOCHLOROMETHANE	1.0	1.0					
1.1.2-TRICHLOROETHANE	1.0	1.0					
BENZENE	1.0	1.0					
cis-1,3-DICHLOROPROPENE	1.0	1.0					
2-CHLOROETHYLVINYLETHER	1.0	10.0					
BROMOFORM	1.0	1.0					
4-RETHYL-2-PENTANUNE	1.0	10.0					
2-HEXANUNE	1.0	10.0					
	1.0	1.0					
1,1,2,2-TETRACHLUKUETHANE	1.0	1.0	<b>T</b> A				
	1.0	1.0	3.0	3.0	2.0	1,4	1.6
	1.0	1.0					
CTYDENE	1.0	1.0					
JITNERE Total Avience	1.0	1.0	A B 1/1	0 0 1/			
IVIAL ATLENED	1.0	1.0	0.4 ]/]	2.0 J/			
CHLORINATED ETHENES TOTAL:			3.0	2.0	3.8	0.7	0.6

·

•

PROJECT: WAUSAU NPL	CK'D: GAW APP'D: KOF
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: ,7-16-88
C#: 13076.30	PAGE 2 OF S
ORGANIC RESULTS	

	SW LAB DETECTION	ENSECO Detection	ENSECO	ENSECO	SH LAB	SH LAB	SW LAB
50H00UU5	LIMIT		WE-6E25-154	WE-6E30-100	WE-GE30-133	WE-6E32-14	WE-6E33-14
CUMPUUND	(U6/L)	(UG/L)	10/20/8/	10/28/8/	11/04/8/	11/12/8/	11/12/8/
	1.0	5.0	5.0 J				
	1.0	5.0	<b>r</b> . <b>r</b>				
	1.0	5.0	5.0 J				
	1.0	1.0	1.0 J				
	1.0	5.0	1.0 J/J		1.0		
	1.0	10.0	10.0 J	10.0 8			
LAKBUN DISULFIDE	1.0	1.0	1.0 J				
	1.0	1.0					
	1.0	1.0					
TRANS-1, 2-DICHLURUETHENE	1.0	1.0				330.0	
	1.0	1.0				20.0 B/UJ	10.0 B/UJ
1.2-DICHLURUETHANE	1.0	1.0					
2-BUTANUNE	1.0	10.0					
1.1.1-IRICHLUKUEIHANE	1.0	1.0					
CARBON TETRACHLORIDE	1.0	1.0					
VINYL ACETATE	1.0	10.0					
BROMODICHLOROMETHANE	1.0	1.0					
1.2-DICHLOROPROPANE	1.0	1.0					
TRANS-1, 3-DICHLOROPROPENE	1.0	1.0					
TRICHLOROETHENE	1.0	1.0			7.6	270.0	
DIBROMOCHLOROMETHANE	1.0	1.0			·		
1,1,2-TRICHLOROETHANE	1.0	1.0					
BENZENE	1.0	1.0					
cis-1,3-DICHLOROPROPENE	1.0	1.0					
2-CHLOROETHYLVINYLETHER	1.0	10.0					
BROMOFORM	1.0	1.0					
4-METHYL-2-PENTANONE	1.0	10.0					
2-HEXANONE	1.0	10.0					
TETRACHLOROETHENE	1.0	1.0				850.0	470.0
1,1,2,2-TETRACHLOROETHANE	1.0	1.0					
TOLVENE	1.0	1.0	2.0	3.0	2.4		
CHLOROBENZENE	1.0	1.0					
ETHYLBENZENE	1.0	1.0					
STYRENE	1.0	1.0					
TOTAL XYLENES	1.0	1.0					
CHLORINATED ETHENES TOTAL:					7.6	1450.0	470.0

PROJECT: WAUSAU NPL	CK'D: CAW APP'D: KDF
Location: Wausau, Wisconsin	DATE ISSUED: 2-16-88
C#: 13076.30	PAGE 3 DF 8
ORGANIC RESULTS	

COMPOUND	SH LAB DETECTION LIMIT (UG/L)	ENSECO DETECTION LIMIT (UG/L)	SW LAB WE-GE34-14 11/12/87	SW LAB WE-GW35-18 11/12/87	SW LAB WE-6E36-16 11/12/87	SW LAB WE-GE38-18 11/13/87	SW LAB WE-GW52-100 11/05/87
CHI NRAMETHANE	1 0	5 Λ					
RRAMAMETHANE	1.0	5.0					
	1.0	5.0					
CHLOROETHANE	1.0	1.0					
METHYLENE CHLORIDE	1.0	5.0		130.0 /UJ			0.6 /J
ACETONE	1.0	10.0		10010 /00			
CARBON DISULFIDE	1.0	1.0					
1.1-DICHLOROETHENE	1.0	1.0					
1.1-DICHLOROETHANE	1.0	1.0					
TRANS-1, 2-DICHLOROETHENE	1.0	1.0			•		2.7
CHLOROFORM	1.0	1.0	0.6 B/UJ	210.0 B/UJ	0.4 B/UJ	0.3 B/UJ	
1.2-DICHLOROETHANE	1.0	1.0					
2-BUTANONE	1.0	10.0					
1.1.1-TRICHLOROETHANE	1.0	1.0	2.0		2.0	0.5	
CARBON TETRACHLORIDE	1.0	1.0				•	
VINYL ACETATE	1.0	10.0					
BROMODICHLOROMETHANE	1.0	1.0					
1.2-DICHLOROPROPANE	1.0	1.0					
TRANS-1,3-DICHLOROPROPENE	1.0	1.0					
TRICHLOROETHENE	1.0	1.0	0.6 /J		2.0		32.0
DIBROMOCHLOROMETHANE	1.0	1.0					
1.1.2-TRICHLOROETHANE	1.0	i.0	•				
BENZENE	1.0	1.0					
cis-1.3-DICHLOROPROPENE	1.0	1.0					
2-CHLOROETHYLVINYLETHER	1.0	10.0					
BROMOFORM	1.0	1.0					
4-METHYL-2-PENTANONE	1.0	10.0					
2-HEXANONE	1.0	10.0					
TETRACHLOROETHENE	1.0	. 1.0	60.0	5700.0	20.0	30.0	
1,1,2,2-TETRACHLORUETHANE	1.0	1.0					
	1.0	1.0			1.0		0.7
	1.0	1.0					
EINYLKENZENE	1.0	1.0					
	1.0	1.0					
IUIAL ATLENES	1.0	1.0					
CHLORINATED ETHENES TOTAL:			60.6	5700.0	22.0	30.0	34.7

.

.

.

.

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.30 ORGANIC RESULTS CK'D: BAW APP'D: KOF DATE ISSUED: 2-16-88 PAGE 4 DF 8

S₩ LAB ENSECO S₩ LAB ENSECO DETECTION DETECTION S₩ LAB S₩ LAB ENSECO LIMIT LIMIT WE-6W53-75 WE-6W53-125 WE-6E54-85 WE-GW55-60 WE-6W55-70 COMPOUND (UG/L) (UG/L) 11/03/87 11/05/87 11/12/87 10/20/87 10/20/87 ---------------CHLOROMETHANE 1.0 5.0 5.0 J 5.0 J BROMOMETHANE 1.0 5.0 VINYL CHLORIDE 5.0 J 1.0 5.0 5.0 J CHLOROETHANE 1.0 1.0 1.0 J 1.0 J METHYLENE CHLORIDE 0.7 /J 5.0 J 1.0 5.0 2.0 J 1.0 ACETONE 10.0 10.0 J 10.0 J CARBON DISULFIDE 1.0 1.0 1.0 J 1.0 J · 0.8 /J 1.1-DICHLOROETHENE 1.0 1.0 1.1-DICHLOROETHANE 1.0 1.0 6.3 TRANS-1, 2-DICHLOROETHENE 1.0 1.0 76.0 641.0 /0 30.0 CHLOROFORM 0.8 /J 2.2 0.2 B/UJ 1.0 1.0 1.2-DICHLOROETHANE 1.0 1.0 2-BUTANONE 1.0 10.0 5.0 R/J 1,1,1-TRICHLOROETHANE 1.0 1.0 14.0 CARBON TETRACHLORIDE 1.0 1.0 VINYL ACETATE 1.0 10.0 BROMODICHLOROMETHANE 1.0 1.0 1,2-DICHLOROPROPANE 1.0 1.0 TRANS-1, 3-DICHLOROPROPENE 1.0 1.0 TRICHLOROETHENE 1.0 1.0 1256.0 1330.0 /0 30.0 DIBROMOCHLOROMETHANE 1.0 1.0 1.1.2-TRICHLOROETHANE 4.6 1.0 1.0 1.0 BENZENE 1.0 cis-1.3-DICHLOROPROPENE 1.0 1.0 2-CHLOROETHYLVINYLETHER 1.0 10.0 BROMOFORM 1.0 1.0 4-METHYL-2-PENTANONE 1.0 10.0 2-HEXANONE 1.0 10.0 TETRACHLOROETHENE 3.1 8.0 1.0 1.0 20.0 1,1,2,2-TETRACHLOROETHANE 1.0 1.0 TOLUENE 3.7 0.8 /J 1.0 1.0 5.0 4.0 5.0 CHLOROBENZENE 1.0 1.0 ETHYLBENZENE 1.0 1.0 , STYRENE 1.0 1.0 TOTAL XYLENES 1.0 1.0 1.2 2.0 3.0 CHLORINATED ETHENES TOTAL: 1335.9 1979.0 80.0

PROJECT: WAUSAU NPL	CK'D: CANN APP'D: KOF
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2-110 58
C#: 13076.30	PAGE 5 OF 8
ORGANIC RESULTS	

÷

COMPOUND ·	SW LAB DETECTION LIMIT (UG/L)	ENSECO Detection Linit (UG/L)	ENSECO WE-6W55-80 10/20/87	ENSECO WE-6W55-115 10/29/87	S₩ LAB ₩E-6₩55A-43 10/15/87	ENSECO WE-GW56-50 10/20/87	ENSECD WE-GW57-21 10/20/87
CHI OROMETHANE	1.0	5.0	5 0 T			5.0 T	5.0 1
BROMOMETHANE	1.0	5.0	310 0			340 0	210 0
VINYL CHLORIDE	1.0	5.0	5.0 J			5.0 J	5.0 J
CHLORDETHANE	1.0	1.0	1.0 J			1.0 J	1.0 J
METHYLENE CHLORIDE	1.0	5.0	5.0 J			5.0 J	5.0 J
ACETONE	1.0	10.0	9.0 J/J	150.0 B/		10.0 J	10.0 J
CARBON DISULFIDE	1.0	1.0	1.0 J			1.0 J	1.0 J
1,1-DICHLOROETHENE	1.0	1.0					
1,1-DICHLOROETHANE	1.0	1.0					
TRANS-1, 2-DICHLOROETHENE	1.0	1.0			5.4		
CHLOROFORM	1.0	1.0					
1,2-DICHLOROETHANE	1.0	1.0					
2-BUTANONE	1.0	10.0	2.0 R/J			2.0 R/J	1.0 R/J
1,1,1-TRICHLOROETHANE	1.0	1.0					
CÁRBON TETRACHLORIDE	1.0	1.0					
VINYL ACETATE	1.0	10.0					
BROMODICHLOROMETHANE	1.0	1.0					
1,2-DICHLOROPROPANE	1.0	1.0					
TRANS-1.3-DICHLOROPROPENE	1.0	1.0					
TRICHLOROETHENE	1.0	1.0		3200.0	27.0		
DIBROMOCHLOROMETHANE	1.0	1.0					
1,1,2-TRICHLOROETHANE	1.0	1.0					
BENZENE	1.0	1.0					
cis-1,3-DICHLOROPROPENE	1.0	1.0					
2-CHLOROETHYLVINYLETHER	1.0	10.0					
BROMOFORM	1.0	1.0					
4-METHYL-2-PENTANONE	1.0	10.0					
2-HEXANONE	1.0	10.0					
TETRACHLOROETHENE	1.0	1.0					
1,1,2,2-TETRACHLOROETHANE	1.0	1.0					
TOLUENE	1.0	1.0	4.0		0.8 /J		2.0
CHLOROBENZENE	1.0	1.0					
ETHYLBENZENE	1.0	1.0					
STYRENE	1.0	1.0					
TOTAL XYLENES	1.0	1.0					
CHLORINATED ETHENES TOTAL:				3200.0	32.4	1.0	

.

.

.

PROJECT: WAUSAU NPL	CK'D: CAN APP'D: KOF
LOCATION: WAUSAU, WISCONSIN	DATE ISSUED: 2 -16.88
C#: 13076.30	PAGE 6 OF 8
ORGANIC RESULTS	•

•

COMPOUND	SW LAB DETECTION LIMIT (UG/L)	ENSECO DETECTION LIMIT (UG/L)	ENSECO WE-SB01 10/29/87	S₩ LAB ₩E-SB02 11/04/87	SW LAB WE-SB03 11/12/87	ENSECO WE-SW09' 10/28/87	ENSECO WE-SW10
CHLOROMETHANE	1.0	5.0					<u>`</u> }
BROMOMETHANE	1.0	5.0					
VINYL CHLORIDE	1.0	5.0					
CHLOROETHANE	1.0	1.0					
METHYLENE CHLORIDE	1.0	5.0			0.6		
ACETONE	1.0	10.0	6.0 B/J			20.0 B	20.0 B
CARBON DISULFIDE	1.0	1.0					
1,1-DICHLOROETHENE	1.0	1.0					
1.1-DICHLOROETHANE	1.0	1.0					
TRANS-1, 2-DICHLOROETHENE	1.0	1.0					
CHLOROFORM	1.0	1.0			0.2 U/J		
1,2-DICHLOROETHANE	1.0	1.0	_				
2-BUTANONE	1.0	10.0	3.0 R/J			2.0 R/J	20.0 R/U
1,1,1-TRICHLOROETHANE	1.0	1.0					
CARBUN TETRACHLORIDE	1.0	1.0					
	1.0	10.0					
	1.0	1.0			<b>_</b> .		
1,2-DICHLURUPRUPANE	1.0	1.0			3.0		
TRANS-1, 3-DICHLUKUPKUPENE	1.0	1.0	• •		<b>.</b> .		<b>_</b>
	1.0	1.0	3.0		3.0	82.0	70.0
	1.0	1.0					
	1.0	1.0					
DENLENE	1.0	1.0					
	1.0	1.0					
2~UNLURUEINILVINILEINER DONMOENDM	1.0	10.0					
ALMETUVI LOLDENTANANE	1.V 4 A	1.0					
9-UEYANANE	· 110	10.0					
TET94/WI ADAETUENE	1.v 4 A	10.0			2 0		
	1.V 4 ()	1.0			Z.V		
	1.0	1.0	<b>٦</b> ۵	7 2	7 0	2.0	
	1 0	1.0	210	J.L	U+V	2.0	
FTHYI REN7ENE	1 0	1 0					
STYRENE	1.0	1 0					
TOTAL YVI ENES	1 0	1.0					
CALLE A LEALA	117	117					
CHLORINATED ETHENES TOTAL:			3.0		5.0	82.0	70.0

• •

PROJECT:HAUSAUNPLCK'D: CAWAPP'D: KOFLOCATION:HAUSAU, WISCONSINDATEISSUED: 2-16-98C#:13076.30PAGE 7 OF SORGANIC RESULTS

.

-

-

COMPOUND	SW LAB DETECTION LIMIT (UG/L)	ENSECO DETECTION LIMIT (UG/L)	SW LAB WE-GCW4-130 10/15/87	ENSECO \\55-01 10/29/87
CHI OROMETHANE	1.0	5.0		
RROMOMETHANE	1.0	5.0		
	1.0	5.0		
CHI OROFTHANE	1.0	1.0		
METHYLENE CHIORIDE	1.0	5.0		
ACETONE	1.0	10.0		150.0 R
CARBON DISULFIDE	1.0	1.0		12010 0
1.1-DICHLOROFTHENE	1.0	1.0		
1.1-DICHLOROETHANE	1.0	1.0		
TRANS-1, 2-DICHLOROETHENE	1.0	1.0	3.4	
CHLOROFORM	1.0	1.0		
1,2-DICHLOROETHANE	1.0	1.0		
2-BUTANONE	1.0	10.0		1000.0 R
1.1.1-TRICHLOROETHANE	1.0	1.0		
CARBON TETRACHLORIDE	1.0	1.0		
VINYL ACETATE	1.0	10.0		
BROMODICHLOROMETHANE	1.0	1.0		
1.2-DICHLOROPROPANE	1.0	1.0		
TRANS-1, 3-DICHLOROPROPENE	1.0	1.0		
TRICHLOROETHENE	1.0	1.0	14.0	
DIBROMOCHLOROMETHANE	1.0	1.0		
1.1,2-TRICHLOROETHANE	1.0	1.0		3200.0
BENZENE	1.0	1.0		
cis-1.3-DICHLOROPROPENE	1.0	1.0		
2-CHLOROETHYLVINYLETHER	1.0	10.0		
8ROMOFORM	1.0	1.0		
4-METHYL-2-PENTANONE	1.0	10.0		
2-HEXANONE	1.0	10.0		
TETRACHLOROETHENE	1.0	1.0	0.8 J/	
1.1,2,2-TETRACHLOROETHANE	1.0	1.0		
TOLUENE	1.0	1.0	1.5	
CHLOROBENZENE	1.0	1.0		
ETHYLBENZENE	1.0	1.0		
STYRENE	1.0	1.0		
TOTAL XYLENES	1.0	1.0		
CHLORINATED ETHENES TOTAL:			18.2	

PROJECT: WAUSAU NPL LOCATION: WAUSAU, WISCONSIN C#: 13076.30 ORGANIC RESULTS CK'D: CAW APP'D: KOF DATE ISSUED: 2-16-88 PAGE 8 OF 8

.

-

QUALIFIER INFORMATION:

U = ANALYZED, BUT NOT DETECTED.

- J = ESTIMATED VALUE.
- B = COMPOUND ALSO DETECTED IN BLANK.

R = UNUSUABLE DATA

D = SAMPLE WAS DILUTED.

\_\_/\_:-HARZYN DATA VALIDATION QUALIFIER / LABORATORY QUALIFIER

G.2

FIELD GC VOC SAMPLES COLLECTED DURING DRILLING

,

					W Nat Voc Analys	AUSAU NPL SIT TER SAMPLING SIS DURING DR	E AND ILLINB											
	DILUTION	. DEPTH	DATE	TOLUENE	1.1 DCE	1,2-DCE	TCE	PCE	BENZENE	Eth-Benzene	NECL 2	i.1DCA	CHEL 3	1,2004	1.1.1TCA	RRC1 2CH	EL RRZEN	RRANAFORM
	FACTOR	(FEET)	COLLECTED	UG/L	U8/L	UB/L	U8/L	U6/L	UB/L	UG/L	UB/L	US/L	UG/L	UG/L	US/L	UB/L	US/L	UG/L
DETECTION 1 Intt				1.0	1.0	1.0	1.0	1.0	2.0	2.0	5.0	2.0	2.0	5.0	1.0	5.0	25.0	50.0
		·····																
-																		
#ELL # F20		21	10-24-87	RADI (R)		1.35	7 19	42.9				•			0421			
E20		35	10-26-87	BMDL (8)		BNDL	3.41	7.88							DUDE			
E20		51	10-27-87	BMDL (B)														
E20 DUP		51	10-27-87	BKOL (B)														
E20		66	10-27-87	BMDL (B)														
E20		COMPLETED	11-3-87	BNDL (B)														
E21		91	11-12-87	BHOL (B)				1.05 (1)										
E21		107	11-12-87					BMDL (1)										
E21		122	11-13-67	BHDL (B)														
E21 DUP		122	11-13-87	BHOL (B)														
E21		132	11-13-87	BNDL (8)			1.98	BHDL										
E21		CONPLETED	12-2-87		-	8MOL	23.7											
E22(2)		20	10-13-87	12.0(B)	BHDL (B)		8HDL	. 11.7			BKDL (B)							
E22(2) DUP		20	10-13-87	12.6(8)	BMDL(B) -		BMOL	12.2										
E22		36	10-13-87	BHDL (B)	BMDL (B) 🐧						BHDL (B)							
E22		50	10-13-87	BMDL (B)														
E22		65	10-14-87	BHDL (B)														
£77		79	10-13-87	BADL (B)									• ••					
		COMPLETED	10-10-8/	2.10(8)					,				2.08					
E23A(2)		COMPLETED	10-30-87	BNDL (B)			3.53	37.6	3.9									
E24A		25-35	10-15-87	BHDL (B)	1.93	13.7	75.5+	293+							BKDL			
E24A DUP		25-35	10-15-87	BNDL (B)	2.42	15.6	78.1+	304+							BNOL			
E24		40	10-15-87	BHOL (8)		1.43	BHDL	BMDL										
E24		55	10-15-87	BNDL (B)			1.25	BNDL			•							
624 638		() (0)00 ()	10-13-87	BUDT (B)			BADI.	BADL					•					
224		CURFLETED	11-4-01	011/1 (07			BRUL	BAUL										
E25		32	10-13-87	BNDL (B)				BHDL										
E25		45	10-13-87	BHDL (B)			BNDL											
E25		50	10-13-87	BHDL (8)														
E25		75	10-13-87	BHOL (B)														
123 195		90	10-14-87	BADL (B)														
EZU E25 NUP		105	10-14-8/	DRM (B)			-											
E25		120	10-15-87	REAL (B)			Quar						4 70(0)					
E25		135	10-14-87	1.97(B)			BKDL						4.70(0)					
E25		154	10-20-87	BKDL (B)			BHDL	BNDL										
E25		COMPLETED	11-3-87															
E25A		COMPLETED	10-26-87	BMDL (B)			8MDL	BHOL										
5710			11-0-07	13 3181														
.4DM		LUNPLEIED	11-4-8/	12,2(8)														

. .

.

.

2.1

.

• • •

e gorane i e i

#### NAUSAU NPL GITE Water Sanpling and VOC Analysis during drilling

.

	DILUTION	DEPTH -	DATE	TOLUENE	1,1 DCE	1,2-DCE	TCE	PCE	BENZENE ET	H-BENZENE	MECL 2	1,1DCA	CHEL 3	1,20CA	1,1,1TCA	BRCL 2CH	CL BR2CH	BRONDFORM
DETECTION	FIRCTUR	(PEE))	COLLECTED	10	U6/L	U6/L	UG/L	UG/L	UG/L	U6/L	UG/L	UG/L	UG/L	UG/L	U6/L	UG/L	UG/L	UG/L
LIMIT				1.0	1.0	1.0	1.0	1.0	2.0	2.0	5.0	2.0	2.0	5.0	3.0	5.0	25.0	50.0
						•••••••••••							••-		******			
E26A DUP		COMPLETED	11-9-87	28.1(8)														
E26A		COMPLETED	11-12-87	17.2(8)														
E26		35	11-9-87	SMOL (B)														
E26		50	11-9-87															
E26		65	11-10-87	BKDL (B)														
E26		80	11-10-87	1.10(8)														
£26		COMPLETED	11-12-87	BADL (B)								•						
£27		90	12-2-87	BADL									6.19					
E27		115	12-2-87	BHDL			BNDL	BKOL					63.9+					
E27		125	12-2-87	1.92			BKDL		BNDL	BKDL			48.7					
£27 (4)		COMPLETED	12-12-87	BKDL		90.7	440	1.49			BMOL		BNDL		BMDL			
E28		COMPLETED	10-16-87	2.22(B)									BAL D					
E280UP		COMPLETED	10-16-87	BKDL (B)		•		BHOL										
E29A		COMPLETED	11-12-87	RMDL (B)														
E29A DUP		COMPLETED	11-12-87	BHDL (B)														
E30		26	10-28-87	9.10(B)			BHDL		BMDL (B)	7.58								
E30		41	10-28-87	BKDL (B)														
E30		56	10-28-87	BNDL (8)														
230		71	10-29-87	BADL (B)														
E30		51	10-29-07	BKOL (B) BUDE (B)			0.401											
F30		101	10-29-07	DHUL (D) DHUL (D)			SUNT											
E 30		111	10-29-87	RMOI (R)			RMRI								DHRI			
E30		121	10-30-87	BHDL (B)			DUDT								BROL			
E30 DUP		121	10-30-B7	BHOL (B)														
E30		COMPLETED 132	11-2-87	BHDL (B)			5.34											
E30 DUP		132	11-2-87	BNDL (B)			5.51											
E 30		COMPLETED	11-4-87	BHOL (B)			6.51											
E30 DUP		COMPLETED	11-4-87	BMDL (B)			6.62											
E31		28	11-2-87	BNDL (B)														
E31		40	11-2-87	BNDL (B)														
E31		55	11-3-87	BHOL (B)														
E31		70	11-3-87	BMOL (B)														
E31		80	11-3-87	BHOL (B)														
£31		90	11-4-87	BMDL (B)														
E31		100	11-4-87	8KDL (8)														
531		110	11-4-87	BHDL (B)														
631 631 AUD		120	11-4-8/	BADL (B)														
E31 VUP 631		120	11-4-8/	RUAT (R)														
E91		130	11-4-8/	RUNT (9)														

•

÷ •

3

.

					H Na Voc Analy:	AUSAU NPL SITI Ter Sampling ( Sis Durikg Dr)	E And Illing											
DETECTION LIMIT	DILUTION Factor	DEPTH (FEET)	DATE COLLECTED	TOLUENE UG/L 1.0	1,1 DCE US/L 1.0	i,2-DCE US/L 1.0	TCE UG/L 1.0	PCE UG/L 1.0	BENZENE EI UG/L 2.0	H-BENZENE UG/L 2.0	HECL 2 U&/L 5.0	1,1DCA UG/L 2.0	CHCL3 UG/L 2.0	1,20CA UG/L 5.0	i,1,1TCA UG/L 1.0	BRCL2CH UG/L 5.0	CLBR2CH UG/L 25.0	BROMOFORM UG/L So. 0
E31 E31 DUP		COMPLETED Completed	11-10-87 11-10-87	BMDL (B) BNDL (B)		BADL	3.87 2.28	1.35 1.28										
E32		14	11-12-87		1.49	164+	292+	506+	•						2.21			
E33	200	14 14	11-12-87 11-12-87	BNDL (8)		1.3	2.87	376+										
E34 E34	100	14 14	11-12-87 11-12-87	4.43(8)			BNDL	73.5										
E35	40	18	11-12-87	BHOL (B)			BKDL	8200#										
E36		16	11-13-87	BMDL (B)			1.68	19.2							BHDL			
E37		COMPLETED	11-13-87	BXDL (B)			2.94	17.8	13.8									
E38	40	18	11-13-87	BNDL (B)				BHOL										
#20 #20 #20 #20 #20 #20 #20		35 45 55 65 65 65 90 75 85 Completed	10-27-87 10-27-87 10-27-87 10-28-87 10-28-87 10-28-87 10-28-87 10-28-87 11-4-87	BMDL (B) BMDL (B) BMDL (B) BMDL (B) BMDL (B) BMDL (B) GMDL (B) (1.0		2.21 9.63 11	48.6 29 19.3 BNDL BNDL BNDL BNDL BNDL											
W51A		COMPLETED	10-16-87	BNDL (B)							•		6.66					
52 52 52 52 52 52 52 52 52 52 52 52 52 5	40 40 40	41 52 61 71 81 04 91 101 111 121 131 131	11-3-87 11-4-87 11-4-87 11-4-87 11-5-87 11-5-87 11-5-87 11-5-87 11-5-87 11-6-87 11-9-87 11-9-87	(1.0 (1.0 BHDL(B) (1.0 (1.0 (1.0 (1.0 (1.0 BHDL(B) BHDL(B) BHDL(B) BHDL(B)			BNDL BNDL BNDL BNDL 30 71.8 653 BNDL 30.4											
W53A W53A DUP W53		COMPLETED Coxpleted 35	11-2-87 11-2-87 11-3-87	BMDL (B) BMDL (B) BMDL (B)		1.74	47.8 50.2 31.7					3.02			3.02			

					VOC ANALY	SIS DURING DR	RILLING											
		,-	\$															
	DILUTION	• DEPTH	DATE	TOLUENE	1,1 DCE	1,2-DCE	TCE	PCE	BENJENE ETH	I-BENZENE	NECL 2	i,iDCA	CHCF 3	1,20CA	1,1,11CA	BRCL2CH	CL BR2CH	BRONDFORM
NETECTION	FALTUN	(FEEL)		65/L	08/L	U8/L	US/L	U6/L	UG/L	UG/L	UG/L	U6/L	US/L	UG/L	U6/L	US/L	U6/L	U6/L
DETECTION				1.0	1.0	1.0	1.0	1.0	2.0	2.0	5.0	2.0	2.0	5.0	1.0	5.0	25.0	50.0
		••••••••••																
-													************			*****		**
W53		55	11-3-87		6.18	102+	33.6	RHDL			RNDL	51.5		CHOI	174			
¥53		65	11-3-87		BKDL	56.5+	732+	1.63				13.5		DITUR.	19.3			
#53	40	75	11-4-87	BHDL (B)		52.3	14B0											
W53	40	85	11-4-87	BNDL (B)			1 3 2 0											
W\$3	40	95	11-4-87	BNDL (B)		156	1960	SKOL										
N53		105	11-4-87	COULD NOT REC	OVER SAMPLE,	DENSE FINE S	iand											
N53	40	115	11-4-87	BNDL (B)		430	1850	BNDL										
153	40	125	11-5-87	BNDL (B)		328	1700	9MDL										
853	40	135	11-5-87	BHOL (B)			BADL	•										
K22		135	11-5-87	BNDL (B)		8.82	52.1	BNOL										
#33 NET		145	11-5-87	BMDL (B)		69.7*	323+	BHDL							BNDL			
833 467		100	11-6-8/	BADL (B)		13.3	99.10	BNOL										
133		CONFLETED 125	11-13-8/	RUDE (R)	(40	- 223	1220	BKOL	(80	(80	<200	(80	<80					
N54		75	11-11-07			7 00	7/6.	20.1										
NS4 DISP			11-11-97			3.07	303*	20.1			•				1.23			
154	40	45	11-12-97	RKM (R)		0.70	3/34	20.2	•.						1.55			
¥54	40	55	11-12-87	RHOL (B)			49.9	PHDL										
854		65	11-12-87	0		A.49	1934	28.8										
W54	40	75	11-12-87	BMDL (B)			75.6	56.7										
W54		85	11-12-87		BNDL	12.8	31.7+	23.1+				BNDL			5.94			•
															•			
N224		COMPLETED	10-15-87	BNDL (B)		1.68	28.3											
800		50	10-20-87	BMDL (B)		BMDL	35,9											
#JJ 855		00 70	10-21-07	BROL (B)			BNDL	1.36							•			
N55		90	10-21-07	DAULIS)							•							
N55		90	10-22-97	PRIM (P)			<b>DKDI</b>											
855		100	10~22-87	A.90(R)		5.20	19 14											
#55		100000	10-22-87	1.00(B)		3.98	70.04											
¥55	40	110	10-26-87	BNDL (B)		•••••	3980	BHDI										
¥55	•	120	10-27-87		1.42	18.6	6004	BNDL										
#55	40	COMPLETED	10-29-87	BNDL (B)			4320+											
W36A		COMPLETED	10-16-87	BADL (B)			1.58											
N26		31.5	10-19-87	3.77(8)			5.38											
#36 #54		40	10-19-87	5×4× 454	11	GHT SAND, NO	SAMPLE OBTA	INED										
M20		50	10-20-8/	RUNT (R)				BMOL (1)										
#J0 #54			10-20-07	BUDY (B)				•										
400		LUNPLE (EP	10-28-87	BRIVL (B)														
W57		71	10-21-87	RMM (R)						•								
N57		32	10-21-87	RHDI (R)														
W57 DUP		32	10-21-87	BKOL (A)														
¥57		41	10-21-87	SMDL (B)	•		BHDI											
NS7 DUP		41	10-21-87	BHDL (B)			BKDL											

WAUSAU NPL SITE WATER SAMPLING AND

ì

					VDC ANALY	SIS DURING D	ILLING												
DETECTION	DILUTION Factor	DEPTH (FEET)	DATE COLLECTED	TOLUENE US/L 1.0	1,1 DCE US/L 1.0	1,2-DCE US/L 1.0	TCE US/L 1.0	PCE UB/L 1.0	BEWZENE ETH- UG/L . 2.0	-BENZENE UG/L 2.0	NECL 2 UG/L 5.0	1, IDCA UG/L 2.0	CKCL3 UG/L 2.0	1,2DCA UG/L 5.0	i,i,iTCA UG/L i.0	BRCL 2CH UG/L 5.0	CLBR2CH UG/L 25.0	BRONOFORM UG/L 50.0	
LIMIT	*******																	••••	
									***********	**********				*********					
¥57		51	10-22-87	BHDL (B)			BKOL							•					
#57		61	10-22-87	BHDL (B)															
827		71	10-22-87	BHDL (B)															•
W0/		CORPLETED	10-30-87	BXDL (B)				BADL (3)											
BLK H20			10-13-87	1.53	BHDL						2.3	•	3.1 -						•••••••••••
WATER TRUCK	K 1		10-13-87	BMDL(B)			BMOL	BMOL			•••		52.9(R)			RKO			
WATER TRUCK	(2		10-13-87	BMDL (B)			BHOL						51.5(B)			RNNI			
SWO1			10-14-87	BNDL (B)											•				
S¥02			10-15-87	BNDL (B)		BHOL	108+	2.91					•.						
SNO3			10-15-87	BHDL (B)		BXDL	79.2+	1.33											
SW04			10-15-87	BMDL (B)			BNDL						BHDL (B)						
SNUS			10-15-87	BMDL (B)			160+												
5808			10-19-87	BADL (B)			108+												
5807(2)			10-20-67	3.01(8)					BHDL				20.3						L 1
5809			10-20-87	BADL (B)				BNDL											ı.
5810			10-28-87	2.0/(8)			1524												
SHLODIE			10-20-07	BRUL (D)			B/.1+												
SW11			10-29-97	DADL (D)			83,48												
CITY WATER	SYSTEM		10-14-97	2 5(8)			DWN						15.8			-			
BLK WATER			10-14-87	2.5(6)			BUAR						20.8(8)			BHOL			
BLK WATER			10-15-87	BKDL									3.3						
BLK WATER			10-19-87	BHDL									ONUL						
BLK WATER			10-20-87	BND1		•													
BLANK WATER	•		11-2-87	BMDL															•
BLANK WATER	1		11-3-07	BADL												•			• • • • •
BLANK WATER	:		11-4-87	BHOL															
BLANK WATER			11-5-87	BHOL	BNDL														
BLANK WATER	1		11-6-87	BHOL															
BLANK WATER			11-9-87	BHOL															
BLANK WATER			11-10-87	BADL		BNDL									BHOL				
BLANK WATER			11-11-87	BNDL											BKOL				•
BLANK WATER			11-12-87	BHDL															
C DIANKI WHILK			11-13-87	BHDL												•			
S DLANKS K	EUK		10-24-87	BMDL (B)			2.58												
S. BLANKY K	50K		11-4 07	BHUL (B)															
S. BLANKA K	FCK		11-9-8/	DRUL (B)															
S. BLANKS K	FCK		11-7-0/	DELLES			RUAL												
S. BLANKA KA	ECK (4)		12-12-87	RMDI (B)		DRUI	<b>ČN</b> RI	<b>D</b> MOI											
WATER TRUCK			10-22-87	BADL (B)		BURL	DANL	AUNT			BADL								
WATER TRUCK			10-23-87	BHDL (B)															
WATER TRUCK	DUP		10-23-87	BHOL (B)															
WATER TRUCK			10-28-87	BMDL (B)															
WATER TRUCK			11-2-87	BHOL (B)															

WAUSAU NPL SITE WATER SAMPLING AND

NAUSI	AU NPL SITE
WATER	SAMPLING AND
VOC ANALYSIS	DURING DRILLING

DIL Fac Detection Limit	LUTION Ctor	DEP (FEE	TH DATE T) COLLECTED	TOLUEWE UG/L 1.0	1,1 DCE UG/L 1.0	1,2-DCE US/L 1.0	TCE UG/L 1.0	PCE UG/L 1.0	BENZENE ET UG/L 2.0	H-BENZENE US/L 2.0	KECL2 UG/L 5.0	I, IDCA UB/L 2.0	CHCL 3 UG/L 2.0	1,2DCA UG/L 5.0	1,1,11CA US/L 1.0	BRCL 2CH UG/L 5.0	CLBR2CH UG/L 25.0	BROMOFORM US/L 50.0
CW10 MN7A MN7ADUP CN4 Wilgon Hurd BDT. H20 "Clear"			10-16-97 10-19-87 10-19-87 10-30-87 10-30-87 10-30-87 10-16-87	BMDL (B) BMDL (B) BMDL BMDL		BKDL	BNDL BNDL 1.42 BNDL	1.09 1.15 13.8		BMDL			22.4					
NOTES • DENDTES ESTINA BMDL-DETECTED BU Conpleted-Well 31 B-Found in Blank (1) Possible Cari	NTED VALUE It below m Installed, Iry over ei	IIWIMUH REP See Appen Rror	DRTABLE DETECTI DIX C FOR CONST	DN LIMIT Ruction Detai	L (DEPTH, ETI	C.)												

÷

12) CONTAINED UNIDENTIFIED PEAKS IN CHROMATOGRAM 13) POSSIBLE SAMPLING DEVICE CONTAINATION 14) ANALYZED BY WARZYN LAB IN MADISON

# APPENDIX H

# SUMMARY OF MONITORING WELL CONSTRUCTION DETAILS AND OBSERVED GROUNDWATER ELEVATIONS

#### XONITORING WELL CONSTRUCTION DETAILS AND WATER LEVELS Wausau water supply wpl site Wausau, wisconsin

.

.

2

.

.

.

· · ·

·

. .

								OCTOBE	2 5,1987	DECEMBEI	10,1987	JANUARY	7, 1988
	TOP OF	TOP OF	6RDUND	WELL									•
	RISER	STEEL CASING	SURFACE	DEPTH	LENGTH	SCREEN		DEPTH TO	NATER	DEPTH TO	WATER	DEPTH TO	WATER
NELL	ELEVATION	ELEVATION	ELEVATION	FROM TOP	OF SCREEN	INTERVAL		WATER	TABLE ELEV	WATER	TABLE ELEV	WATER	TABLE ELEV
10	(FEET MSL)	(FEET MSL)	(FEET MSL)	OF RISER	(FEET)	(FEET MSL)	COMMENTS	(FEET)	(FEET MSL)	(FEET)	(FEET HSL)	(FEET)	(FEET MSL)
			EAST WELL F	IELD		*****				•••••••••••••	*************	••••••	
CW3	1204.08	1202.31		92.00	40.00	1152.64-1112.64	PILINPING	42.00	1142.09	17 00	1107 40	47 66	
CIN	1198.25		1198.19	130.00	40.00	1108.25-1048.25				Not Dupping	110/.00	43.00	1101.00
HURD	1199.79		1198.70	100.00	20.00	1119.52-1099.52		_	_	43 SA	1101 20	FUNFIND	
WERGIN	1201.09			50			PUXP ING	41.43	1159 44	13.30	1100.27	14.13 DUNOTNO	1183.64
NC1	1197.22	1197.36	1195.30	23.00	10.00	1183.97-1173.97		12, 28	1194 94	12 14	1105.04	17 27	
NC2	1198.22	1198.24	1196.10	24.00	10.00	1183.93-1173.93		13 19	1195 01	13.10	1103.00	13.27	1183.93
NC3	1198.37	1198.41	1196.60	161.00	3.00	1040.11-1037.11		13.17	1185 20	13.10	1103.04	14.32	1183.90
NC3A	1198.00	1198.04	1196.40	65.00	3.00	1135.76-1132.76		12.90	1185 10	13.17	1105.10	14.47	1103.10
WC3B	1198.15	1198.19	1196.90	24.00	10.00	1183.89-1173.89		12 90	1105.10	12.70	1103.02	14.12	1103.00
NC3C	1198.62	1198.76	1196.90	29.00	10.00	1179.37-1169.37		13.44	1184 99	13.20	1104.07	14.39	1103.01
NC4	1196.86	1196.88	1195.00	60.00	3.00	1139.58-1134.58		11.44	1185 42	11.44	1104.07	19.77	1103.03
WC4A	1196.69	1196.75	1195.00	30.00	10.00	1176.41-1166.41		11.28	1185.41	11 34	1105.10	12.30	1104.20
¥C5	1196.73	1196.75	1195.00	70.00	3.00	1129.49-1126.49		11.98	1194 85	11 59	1105.55	12.72	1104.27
WC5A	1196.75	1196.85	1194.70	30.00	10.00	1176.52-1166.52		11.91	1184.RA	11.57	1105.14	12.07	1104.04
NC6	1199.25	1198.25	1196.50	70	3.00	1131.01-1128.01		12.97	1185 28	11.37	1105.10	14.14	1184.03
WC6A	1198.73	1198.69	1196.90	30.00	10.00	1178.50-1168.50		13.44	1185 29	13.25	1105.04	14.00	1103.34
¥C7	1197.06	1197.12	1195.10	60.00	3.00	1139.82-1136.82		11.25	1185 81	11 92	1105.14	13.34	1103.34
WC7A	1196.88	1195.94	1194.90	30.00	10.00	1176.63-1166.63		11.42	1185 44	11 74	1105.11	13.40	1103.00
KN8	1198.96	none	1198.20	23.50	10.00	1185.20-1175.20		13.42	1185 34	11 77	1103.12	13.27	1103.01
WCX1	1199.40	1199.62	1196.80	26.50	10.00	1182.90-1172.90		14.47	1184 73	14 70	1194 70	15.14	1103.02
NCX2	1199.72	none		26.50	10.00	1183.10-1173.10		14.72	1185.00	14.76	1104.70	10.04	1103.30
NC13	1199.90	1200.13	1197.20	26.50	10.00	1183.40-1173.40		15.04	1184 84	15.10	1104.70	DUNDING	1103.03
NC14	1202.25	none		26.50	10.00	1185.50-1175.50	PURPING				1104.70	PUTFING	-
WC15	1203.39	none		26.50	10.00	1186.70-1176.70	PUXPING	21.20	1187.19	20 43	1197 94	PUNPIND	-
NC16	1200.14	none		26.50	10.00	1183.40-1173.40	PURPING	15.16	1184.98	15 21	1104 91	14 41	1107 67
NC17	1202.47	none		27.50	10.00	1184.60-1174.60	PUMPING	20.24	1182.23	20.23	1101 74	DINDING	1103.33
NCX8	1202.04	8008		26.50	10.00	1185.30-1175.30	PURP ING	18.45	1183.39	17 14	1104 00	10 74	1101 70
NCX9	1199.25	0008		26.50	10.00	1182.50-1172.50		14.22	1185.03	14.23	1185 02	15.49	1103.70
NCX10	1203.29	1203.29	1200.10	26.50	10.00	1186.60-1176.60	PUMPING	18.26	1185.03	18.24	1185.03	19 44	1193.93
NCX11	1203.73	none		26.50	10.00	1187.00-1177.00		-	-	-		19 92	1193 81
WCI12	1199.79	1199.81	1196.80	26.50	10.00	1183.10-1173.10		14.48	1185.11	14.72	1185.07	15 94	1103.01
NCX13	1199.52	none		26.70	10.00	1182.60-1172.60		14.33	1185.19	14.38	1185 14	15.40	1103.03
NCX14	1199.46	hohe		26.70	10.00	1182.50-1172.50		14.22	1185.24	14.28	1185.19	15.52	1183 94
WCX15	1199.20	none		26.50	10.00	1182.50-1172.50		14.33	1184.87	14.05	1185.14	15.24	1183 94
N¥7A	1201.28	1201.34	1199.10	69.50	10.00	1141.58-1131.58		18.39	1192.89	17.26	1184.02	17.91	1193 37
N¥9A	1197.10	1197.10	1195.00	141.00	10	1065.68-1055.68		11.32	1185.78	11.79	1185.31	13.38	1183.72
HW10A	1206.94	1206.98	1204.60	76.50	10.00	1140.20-1130.20		21.85	1185.09	22.20	1184.74	22.80	1184.14
NW10B	1206.80	1206.86	1204.70	35.00	10.00	1181.55-1171.55		21.70	1185.10	22.04	1184.74	22.69	1184.11
HW 1 1 #	1210.15			35	10	1184.90-1174.90		25.28	1184.87	25.58	1184.57		-
H#12	1200.08	COULD N	OT LOCATE	70.0	20.00	1150.08-1130.08 C	ANT FIND	-	•			-	-
8¥13+	1211.34	1211.42	1211.40	45.00	10.00	1176.09-1155.09		26.35	1184.99	26.65	1184.68	27.28	1184.06
M¥14	1198.21	1198.26	, 1198.30	45	10.00	1162.97-1152.97		16.01	1182.20	14.00	1184.21	14.74	1183.47

#### MONITORING WELL CONSTRUCTION DETAILS AND WATER LEVELS Wausau water supply NPL Site Wausau, Wisconsin

.

· · .

.

:

.

.

· •.

· · · ·

÷

	100 OF	100 OF	0001120					OCTOBER	5,1987	DECEMBER	10,1987	JANUARY	7, 1988
WELL	RISER ELEVATION	STEEL CASING ELEVATION	SURFACE	DEPTH FROM TOP	LENGTH OF SCREEN	SCREEN INTERVAL		DEPTH TO Water	WATER TABLE ELEV	DEPTH TO NATER	WATER Table flev	DEPTH TO NATER	NATER Table flev
10	(FEET MSL)	(FEET HSL)	(FEET MSL)	OF RISER	(FEET)	(FEET MSL)	COMMENTS	(FEET)	(FEET HSL)	(FEET)	(FEET MSL)	(FEET)	(FEET MSL)
WH S	1198.61	1198.73	1197.30	40.00	5.00	1153.37-1158.37		14.79	1183.82	13.49	1185.13	14.91	1183.70
WW2	1203.26	1203.38	1202.00	40.00	5.00	1158.02-1163.02		19.59	1183.67	17.81	1185.45	19.31	1183.95
WN 3	1201.90	1202.06	1200.70	40.00	5.00	1156.66-1161.55		19.06	1182.84	16.55	1185.35	18.09	1183.81
WW 4	1202.31	1202.41	1200.90	40.00	5.00	1167.11-1162.11		19.35	1182.96	17.22	1185.09	18.82	1183.49
WN5	1210.33	1210.43	1208.30	37.00	5.00	1178.05-1173.05		26.72	1183.61	25.48	1184.85	26.83	1183.50
MM-0	1200.64	1200.96	1199.20	41.00	5.00	1164.42-1159.42		17.73	1182.91	16.04	1184.60	17.61	1183.03
WW7	1200.86	1201.08	1199.20	48.00	5.00	1157.63-1152.63		18.04	1182.82	15.96	1184.90	17.63	1183.23
TCT1 (40)	1204.55	1204.75	1202.00	72.10	5.00	1137.25-1132.25		-	-	-	•	20.82	1183.73
TC12(41)	1203.54	1203.68	1200.70	22.10	15.00	1196.19-1181.19		19.56	1183.98	18.30	1185.24	19.96	1183.58
TCT3(42)	1201.66	NONE	1200.40	54.00	5.00	1152.43-1147.43		19.57	1182.09	16.40	1185.26	18.02	1193.64
TCT4 (43)	1203.23	1203.35	1201.70	23.80	15.00	1194.17-1179.17		20.35	1182.88	17.69	1185.54	19.20	1184.03
TCT5(44)	1204.45	1204.57	1202.30	23.00	15.00	1196.21-1181.21		-	-	18.81	1195.64	20.22	1184.23
FVD1	1199.70	1199.74	1197.60	22.00	10.00	1187.70-1177.70		15.39	1184.31	14.74	1184.96	15.94	1183.76
FVD2	1199.27	1199.35	1197.30	20.00	10.00	1189.27-1179.27		14.90	1184.37	14.30	1184.97	15.48	1183.79
FVDS	1198.88	1198.92	1196.90	20.50	10.00	1188.35-1178.35		14.61	1184.27	13.68	1185.00	15.13	1183.75
FVD7	1198.59	1198.73	1196.90	18.50	10.00	1189.77-1179.77		14.68	1183.91	13.54	1185.05	14.94	1183.65
6M5D	1200.38	1200.90	1200.90	114.00	10.00	1096.21-1086.21		17.79	1182.59	15.31	1185.07	16.97	1183.41
GN6D	1198.78	1199.06	1199.10	126.00	10.00	1082.46-1072.46		15.86	1182.92	13.64	1185.14	15.26	1183.52
6H7D	1198.77	1199.21	1199.20	123.00	10.00	1085.54-1075.54		15.39	1183.38	13.79	1184.98	15.25	1183.52
GK8D+	1196.18			122.50	10.00	1083.43-1073.43		12.53	1183.65	11.08	1185.10	12.54	1183.64
6X95	1198.94	1199.23	1199.20	20.00	10.00	1188.67-1178.67		15.60	1183.34	13.82	1185.12	15.38	1183.56
E20	1199.18	1199.34	1197.20	79.50	5.00	1122.70-1117.70				14.02	1185.16	15.46	1183.72
E21	1197.61	1197.53	1195.20	129.50	5.00	1071.20-1065.70				11.57	1186.04	12.55	1185.06
EZIA	1197.95	1197.87	1195.20	22.00	10.00	1183.20-1173.20				11.93	1186.02	12.94	1185.01
E22	1195.54	1196.08	1196.10	93.70	5.00	1107.40-1102.40				10.47	1185.07	· 11.76	1183.78
E22A	1195.93	1196.43	1196.40	22.00	10.00	1184.40-1174.40				10.87	1185.06	12.10	1183.83
E23A	1197.69	1198.15	1198.20	21.40	10.00	1186.80-1176.80				12.80	1184.89	14.24	1183.45
E24	1210.13	1210.15	1208.50	85.70	5.00	1127.80-1122.80				25.26	1184.87	26.13	1184.00
E24A	1211.18	1211.18	1209.00	35.00	10.00	1184.00-1174.00				26.36	1184.82	27.22	1193.96
E25	1213.93	1213.99	1211.70	135.00	5.00	1081.70-1076.70		·		29.34	1184.59	29.79	1184.14
E25A	1213.87	1213.93	1211.70	37.50	10.00	1184.20-1174.20				.29.2B	1184.59	29.76	1184.11
E26	1199.08	1199.02	1196.70	95.00	5.00	1106.70-1101.70				13.76	1185.32	14.91	1184.17
E26A	1199.23	1199.23	1196.60	23.00	10.00	1183.60-1173.60				13.68	1185.35	15.01	1184.22
E27	1195.71	1196.31	1196.30	136.50	5.00	1064.80-1059.80				-	-	10.57	1185.14
E28A	1211.69	1212.14	1212.10	37.00	10.00	1185.10-1175.10				26.49	1185.19	27.66	1184.02
E29A	1200.30	1200.80	1200.80	29.00	10.00	1181.80-1171.80				15.20	1185.10	16.94	1183.36
E30	1204.58	1204.68	1202.10	132.80	5.00	1074.30-1069.30				18.99	1185.59	20.25	1184.33
E31	1201.15	1201.65	1201.60	135.50	5.00	1071.10-1066.10				15.72	1185.43	17.43	1183.72
E37A	1197.80	1198.28	1198.30	26.00	10.00	1182.30-1172.30				12.95	1184.85	14.34	1183.46

.

.

#### NOMITORING WELL CONSTRUCTION DETAILS AND WATER LEVELS Wausau water supply wpl site Wausau, wisconsin

.

:

.

·. .

:

	top of	TOP OF ,	GROUND	WELL				OCTOBE	R 5,1987	DECEMBER	10,1987	JANUARY	7, 1988
WELL 1D	RISER Elevation (Feet MSL)	STEEL CASING ELEVATION (FEET MSL)	SURFACE Elevation (Feet MSL)	DEPTH FROM TOP OF RISER	LENGTH OF SCREEN (FEET)	SCREEN INTERVAL (FEET MSL)	CONNENTS	DEPTH TO Nater (Feet)	WATER TABLE ELEV (FEET MSL)	DEPTH TO Water (Feet)	WATER TABLE ELEV (FEET MSL)	DEPTH TO Water (Feet)	WATER TABLE ELEV (FEET MSL)
					********	WEST WELL FIELD							
CW6	1220.02		1220.02	100.00	38.50	1120.02-1158.52	PUKPINS	60.58	1159.44	43.00	1177.02	40.00	1140.02
CN7	1223.63		1223.63	100.00	39.00	1123.63-1162.63	PURPING	64.23	1159.40	65.00	1159.43		1159 43
CW9	1224.56		1224.56	100.00	60.00	1124.56-1184.56	PUMPING	62.00	1162.56	59.00	1165.56	43.00	1101 54
CW90BS	1224.40	1224.40	1222.30	78.00				41.10	1183.30			40.29	1184.11
CHIO			1215.05							SEALED	<b>1</b>	SEALED	
CIS	1223.69		1220.98	29.90	15.00	1206.08-1191.08		30.72	1192.97	>32.01	1223.49	29.95	1193 74
C2S	1219.24	1219.36	1216.30	37.90	15.00	1193.34-1178.34		32.21	1187.03	32.46	1186.78	32.45	1184.59
C3S	1220.24	1220.52	1217.60	38.90	15.00	1193.51-1178.51		33.20	1187.04	33.54	1186.70	33.84	1184 40
C4S	1216.84	1216.94	1214.30	32.20	15.00	1197.06-1182.06		29.84	1187.00	30, 19	1186.65	30.50	1186.34
C4D	1216.32	1216.56	1214.20	104.20	5.00	1114.84-1109.84		29.36	1186.96	29.66	1186.66	30.02	1184 30
C65	1221.69		1219.32	39.50	15.00	1194.82-1179.82		34.50	1187.19	34.94	1186.75	35.13	1184.54
C75	1221.00	1221.12	1218.20	36.00	15.00	1197.26-1182.26		33.91	1187.09	34.29	1186.71	34,40	1186.40
#1A	1215.79	1215.93	1214.21	130.00	8.00	1092.21-1084.21		30.05	1185.74	30.48	1185.31	30.03	1185.76
NJA NJA	1223.26		1221.11	140.00	10.00	1091.11-1081.11		38.43	1164.83	38.98	1184.28	38.34	1184.92
<b>U</b> 3B	1223.53		1221.17	74.70	10.00	1156.27-1146.27		38.62	1184.91	39.15	1184.38	38.58	1184.95
#4R	1215.22	1215.52	1215.50	100.00	10.00	1125.59-1115.59	•	32.72	1182.50	32.59	1182.63	31.37	1183.85
#48	1215.58	1215.62	1215.60	60.5	10.00	1165.18-1155.18		32.82	1182.76	32.99	1182.59	31.79	1183.79
840	1215.34	1215.39	1215.40	40.00	10.00	1185.69-1175.69		32.44	1182.90	32.70	1182.64	31.49	1183.85
83	1219.22	•	1219.08	45.00	10.00	1184.28-1174.28		36.42	1182.80	36.92	1182.30		•
86	1218.93		1218.93	45.00	10.00	1184.00-1174.00	05	STRUCTED	-			-	-
W/	1219.10		1219.10	45.00	10.00	1184.06-1174.06		37.10	1182.00	37.52	1181.58	•	-
168 110	1217.55		1217.55									-	-
#Y	1201.91	1201.97	1202.00	50.00				18.29	1183.62	20.64	1181.27	17.46	1184.45
PLUR SI	1215.85			95.00			•	26.47	1189.38	26.74	1189.11	26.00	1189.85
#15	1222.13	1222.19	1220.10	40.50	10.00	1189.51-1179.51		34.35	1187.78	34.92	1187.21	34.97	1187.16
RID	1222.39	1222.41	1220.10	121.00	10.00	1109.16-1099.16		34.85	1187.54	35.41	1186.98	35.43	1186.96
K25	1209.88	1209.96	1208.10	28.00	10.00	1190.05-1180.05		22.44	1187.44	23.28	1186.60	23.05	1186.83
R2V	1204.38	1209.82	1207.90	135.00	10.00	1082.69-1072.69		23.21	1186.37	23.60	1185.98	23.41	1186.17
835 070	1215.29	1215.35	1212.80	32.00	10.00	1190.79-1180.79		27.29	1188.00	28.00	1187.29	28.07	1187.22
RJU	1215.55	1215.57	1213.10	136.00	10.00	1087.09-1077.09		28.90	1186.63	29.24	1186.29	29.18	1186.35
MAN CHIC	1219.24	1219.28	1216.00	133.00	10.00	1093.05-1083.05		32.25	1186.99	32.51	1186.73	32.72	1186.52
0515	1216.07	1216.11	1214.30	37.00	10	1167.42-1157.42		30.23	1195.84	30.80	1185.27	30.16	1185.91
0//25	1211.91		1212.30	34.00	10.00	1108.79-1178.79		26.03	1185.88	26.52	1185.39	26.12	1185.79
0033	1214.72		1215.10	37.00	10.00	1188.10-1178.10		28.20	1186.52	28.52	1186.20	28.21	1186.51
CH43	1216.13		1214.30	29.00	10.00	1188.31-1178.31	•	30.06	1186.07	30.62	1185.51	30.02	1186.11
REV DUAN	1216.46		1214.50	145.00	10.00	1079.52-1069.52		30.34	1186.12	30.42	1186.04	30.32	1186.14
WJU 1651A	1215.67	1215.77	1213.30	82.80	5.00	1135.50-1130.50				29.07	1186.60	29.00	1186.67
MEJ NEJ	1224.30	1224.46	1222.20	44.70	10.00	1187.50-1177.50				37.10	1187.40	37.22	1187.28
W52A	1219.18	1219.22	1216.50	124.00	5.00	1097.50-1092.50				32.23	1186.95	32.74	1186.44
WIT	1214.08	1219.10	1216.80	36.00	10.00	1190.80-1180.80				32.70	1186.38	32.27	1186.81
M32	1216.77	1217.53	1217.50	125.50	5.00	1097.00-1092.00				30.10	1186.67	•	-

.

#### MONITORINB WELL CONSTRUCTION DETAILS AND WATER LEVELS Wausau Water Supply Mpl Site Wausau, Wisconsin

.

.

:

	TOP OF	TOP OF	SPALING	WELL				OCTOBE	R 5,1987	DECEMBER	10,1987	JANUARY	7, 1988
NEEL ID 	RISER ELEVATION (FEET MSL)	STEEL CASING Elevation (Feet MSL)	SURFACE ELEVATION (FEET HSL)	DEPTH FROM TOP DF RISER	LENGTN Of Screen (Feet)	SCREEN Interval (Feet MSL)	CONNENTS	Ó DEPTH TO Nater (feet)	WATER TABLE ELEV (FEET MSL)	DEPTH TO WATER (FEET)	WATER TABLE ELEV (FEET MSL)	DEPTH TO Water (Feet)	WATER TABLE ELEV (FEET MSL)
¥53A	1217.00	1217.62	1217.60	41.30	10.00	1186.30-1176.30				10 11	1101 10		********
N54	1216.31	1216.87	1216.90	65.50	5.00	1156.40-1151.40				30.31	1100.07	-	
W55	1217.69	1217.93	1217.90	115.50	5.00	1107.40-1102.40				29.71	1171.00	29.85	1150.40
W55A	1217.40	1217.98	1218.00	43.00	10.00	1185.00-1175.00				32.70	1104.10	32.14	1185.54
¥56	1200.11	1200.17	1198.90	44.50	5.00	1137 40-1132 40				31.68	1185.52	31.62	1185.78
¥56A	1200.95	1200.95	1198.80	70.00	10.00	1100 00-1170 00				14.49	1185.62	14.11	1186.00
¥57	1205.30	1205.30	1202.10	77 50	5 00	1120 (0.1124 (0				11.76	1189.19	11.91	1189.04
561	1189 39	1109 30		//	3.00	1127.00-1124.00				21.98	1183.32	20.91	1184.39
\$67	1107.34	1107.30										FROZEN	-
	1113134	1173.34										2.02	1191.32

.

.

• CORRECTED BY ADDING 0.25 TO RMT SURVEYED TOP OF CASING ELEVATION - Water level kot recorded

· · .

•

## APPENDIX I

· .

.

· · ·

•

• .

# HYDRAULIC CONDUCTIVITY TEST METHODS AND RESULTS

### BAILDOWN HYDRAULIC CONDUCTIVITY TEST METHODS AND RESULTS

The purpose of the baildown tests conducted on the site is to measure in-situ saturated hydraulic conductivity of subsurface materials. Baildown tests measure the saturated hydraulic conductivity of undisturbed, in-place aquifer material, whereas laboratory tests require removal of a sample from its natural environment.

The general procedure for a baildown test is to instantaneously remove a measured volume of water from the well as rapidly as possible, by bailing or pumping, and measure the rate at which the water in the well returns to its static level. The hydraulic conductivity of the aquifer material is a function of the rate of water level rise and the well geometry. In permeable aquifer material, the location of the well screen with respect to the water table and the base of the aquifer are important. The configuration of a typical baildown test is illustrated in Figure A.

### DATA REDUCTION

Several methods are available to interpret the water level versus time data that are obtained from a baildown test. These include Hvorslev (1951), NAVFAC (1971), Papadopulos, et al. (1973), and Bouwer and Rice (1976). The first three references use an analytical solution to a well fully penetrating a confined aquifer. The method by Bouwer and Rice utilizes an analog model of both fully and partially penetrating wells to aid in solution of the modified Thiem equation. The Bouwer and Rice method was selected because of its ability to incorporate the effects on recovery rate due to a partially penetrating well.

The Bouwer and Rice method is based on solution of a modified Thiem equation for radial flow to a pumped well as shown in Equation 1.

 $Q = 2 (KLy)/(ln(R_e/r_W))$  (1)

Where:

Q = flow into the well  $(L^3/T)$ 

- K = hydraulic conductivity of the aquifer (L/T)
- L = open length of open interval in the well (L)
- y = difference between the water level in the well and the equilibrium level in the aquifer (L)
- $R_{\rho}$  = radius of influence of the well (L)
- $r_w$  = effective well radius (L)

In a single well test, the value of  $R_e$  is unknown. Values of  $R_e$ , in terms of the  $\ln(R_e/r_w)$  were determined by Bower and Rice (1976) with an electric analog model of a homogeneous isotropic aquifer. The analog model was used to analyze the effects of the aquifer and well geometry. Results of the study for a partially penetrating well is shown in Equation 2 using Equation 3 to determine the value of  $\ln(R_e/r_w)$ .

$$K = \frac{r_{c}^{2} \ln(R_{e}/r_{w})}{2L} \quad \frac{1}{t} \quad \ln \frac{y_{0}}{y_{t}} \quad \dots \quad \dots \quad (2)$$

Where:

 $r_{c}$  = radius of the well casing (L)

t = time(T)

y<sub>o</sub>,y<sub>t</sub> = difference between the water level in the well and the equilibrium level in the aquifer at times o and t

$$\ln(R_{e}/r_{w}) = 1.1/\ln(Hr_{w}) + \frac{A+B \ln(D-H)/r_{w}}{L/r_{w}} - \frac{1}{L/r_{w}}$$
(3)

Where:

A,B = constants obtained from Figure B

H = depth to the bottom of the screen from the water table

D = thickness of the aquifer

As noted by Bouwer and Rice, a semilog plot of  $y_0/y_t$  versus time (t) (on the linear scale) should yield a straight line.

A FORTRAN program was developed by WEI to reduce the baildown field test data. The program allows for skewed data points and outliers to be deleted from the time-drawdown plot, and the remaining data points are then matched to a linear least square fit.

Input data for each test is listed in the following pages. Output from the test analysis follows the input data. Results of the tests are summarized and discussed in the text.

### **REFERENCES CITED**

- Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12, No. 3, p. 423-428.
- Hvorslev, M.J., 1951, Time Lag and Soil Permeability in Groundwater Observations. U.S. Army Corps of Engineers, Waterways Exp. Sta. Bull 36, Vicksburg, MS.
- Papadopulos, S.S., Bredehoeft, J.D., and Cooper, H.H., Jr., 1973, On the Analysis of 'Slug Test' Data. Water Resources Research, Vol. 9, No. 4., p. 1087-1089.
- United States Department of the Navy, Design Manual: Soil Mechanics, Foundations, and Earth Structures, NAVFAK DM-F, March 1971, p. 7-4-9.

MMM/cac/KJQ [cac-53-49]



FIGURE A BAILDOWN TEST CONFIGURATION







<b>S£100</b> Environment 11/05 Unit# 00168	<b>908</b> :al Logger 18:45 3 Test# 1	BAW DATA AND LST.SQUA	RF FIT
INPUT 1: Let	vel (F) TOC	-1 500	
Reference Scale factor Offset	18.43 50.48 8.00	E2U	
Step# 0 11/	16:29 °		
Elapsed Time	) Value		
0.0000	- 59.28		
0.0033	- 59.27		+
0.0099	- 59.23	Ê_]	
0.0133 0.0166	- 59.22		
0.0200	- 31.64		
0.0233 0.0266	- 32.94 - 41.57	3	+
0.0300	- 39.65		
0.0333 0.0500	- 40.12 - 40.39	2	
0.0666	- 40.65		
0.0833 0.1000	- 40.07 - 41.13		
0.1166	- 41.35		0.0 50
0.1333 0.1500	- 41.57 - 41.81	IIME (SECS) *10'	
0.1666	- 42.04		
0.1833 0.2000	- 42.28 - 42.48		
0.2166	- 42.69		
0.2333	- 42.91 - 43.10		
0.2666	- 43.31		
0.2833	- 43.52 - 43.71	ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼	36
0.3166	- 43.92	WARZYN ENGINEERING.IN(	<b>.</b> .
0.4167	- 45.06	MADISON, WISCONSIN	
0.5000	- 45.93		
0.6667	- 47.46	BAIL DUWN ANALYSIS	
0.7500 0.8333	- 48.12 - 48.75	DATA OBTAINED BY : CSR	
0.9167	- 49.30	DATA ANALYZED BY : CSR	
1.0000	- 49.81 - 50.26	BAIL DOWN PARAMETERS FOR FOR COD	
1.1667	- 50.67	, EXCLUSION FUNCTION EXCLUSION	
1.3333	- 51.39	୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶	10
1.4166	- 51.70	EFFECTIVE WELL DIAMETER = 2.000 INCHES	1
1.5033	- 52.21	EFFECTIVE SCREEN DIAMETER = 2,000 INCHES	•
1.6667	- 52.43		
1.8333	- 52.79	LIFECTIVE SCREEN LENGTH = 5.000 FEET	
1.9167 2.0000	- 52.95 - 53.10	WELL PENETRATION DEPTH = 62.080 FEET	
2.5000	- 53.67	AQUIFER THICKNESS = 119.560 FFFT	
3.5000	- 53.97 - 54.12		
4.0000	- 54.20	18.430 FEET	
4.3000 5.0000	- 54.25	AQUIFER CONDUCTIVITY IS = .170E-02 CM/SEC	
5.5000	- 54.26	OR .362E+02 GAL/FT	/FT/DAY
6.5000	- 54.28	AQUIFER TRANSMISSIVITY IS - SERENCE CHARGE	ere
7.0000 7.5000	- 54.28		266
8.0000	- 54.28	OR .416E+04 GAL/FT	/DAY
8.5000 9.0000	- 54.28 - 54.28	****	l‡
9.5000	- 54.28	CENSORED DATA END POINTS ARE :	
10.0000 12.0000	- 54.29 - 54.29	START TIME IS = .000E+00 SECON	ວຣ
END		END TIME IS = .100E+03 SECONT	20
			)5

· · · · ·

. .

. .

•

		105				
			ם מדמח		SOLIDRE	FIT
						1 1 1
		-	E2	O REP		
SE1000B						
11/05 18:	144 L		<b>★</b> ,			
Unit# 00168 T	lest# 2 _		- total			
INPUT 1: Level	(F) TOC			<del>*</del> **		
Reference	18.43 [	5 -		, '~ <del>*</del> **+	En Alera	
Scale factor - Offset	0.89 (				· + + +	
Step# 0 11/05	17:29				· + -	F.
Elapsed Time	Value	" - -				++
0.0000	14.23	· 1				
0.0033 0.0066	14.44 21.28					
0.0099 0.0133	49.02	₽	·····		T	<del></del> 1
0.0166	32.50	0.0 20.0	40.0	60.0 8	30.0 100.0	120.0
0.0200 0.0233	34.12 33.73		TIME	(SECS)		
0.0266	33.66		1 1 1 1 1			
0.0333	33.50					
0.0500 0.0666	33.15 32.82					
0.0833	32.50					
0.1166	31.91					
0.1333	31.64 31.35					
0.1666	31.08					
0.2000	30.55	66666666666666666666666666666666666666	000000000000000000000000000000000000000	366666666666666666	900000000	
0.2166 0.2333	30.28 30.03	WARZY	NENGINE	ERING,	, INC.	•
0.2500 0.2666	29.77	MAD	ISON. WIS	SCONS1	N.	
0.2833	29.28	D A T			G	
0.3009 0.3166	29.02 28.80	BHI			5	
0.3333 0.4167	28.56	DATA OBTAIN	ED BY 1	CSR		
0.5000	26.41	DATA ANALYZ	ED BY :	CSR		
0.6667	23.47 24.63	BAIL DOWN F	ARAMETERS FOR	E20 REP		
0.7500 0.8333	23.86 23.17	666666666666666666666666666666666666666	86666666666666666	300000000000000000000000000000000000000	36666666	
0.9167	22.57	FFFECTIVE WELL	DIAMETER =	2.000	INCHES	
1.0833	21.53			2.000		
1.1667 1.2500	21.10 20.72	EFFECTIVE SCRE	TEN DIAMEIEK -	2.000		
1.3333 - 1.4166	20.39 20.08	EFFECTIVE SCRE	EEN LENGTH =	5.000	FEET	
1.5000	19.83	WELL PENETRAT	ION DEPTH =	62.080	FEET	
1.5833	19.39 19.40	AQUIFER THICKN	NESS =	119.560	FEET	
1.7500 1.8333	19.21 19.06	STATIC WATER L	_EVEL =	18.430	FEET	
1.9167	18.92			2085-02	CM/SEC	
2.5000	18.35	MADILEK CONDO	2,1411 13 3	. 2002-02		
3.0000 3.5000	18.15 18.06		OR	.440E+02	GAL/FT/FT/DAY	
4.0000	18.01	AQUIFER TRANSM	MISSIVITY IS =	.757E+01	CM+CM/SEC	
9.3000 5.0000	17.99		OR	.526E+04	GAL/FT/DAY	
5.5000 6.0000	17.98 17.98	***	***	***	***	
6.5000	17.98					
7.0000 7.5000	17.98 17.98	CENSORED DATA START TIME IS	END POINTS ARE	: .000E+00	SECONDS	
8.0000	17.98			1005-07		
0.0000 9.0000	17.42	END TIME IS	-	.100E+03	SELUNI/S	
	17.50					
9.5000	99.12					

.

••••••

. .

	RAW DATA AND LST.SQUARE FIT
SE10008 Environmental Logger 11/06 14:28 Unit9 00168 Test\$ 4 INPUT 1: Level (F) TOT	
Reference     11.74       Scale factor     50.48       Offset     0.00       Step8 0     11/06       Elapsed Time     Value       0.0000     11.74       0.0000     11.74       0.0000     11.74       0.0000     11.74       0.0003     12.15       0.0006     14.17       0.0006     14.17       0.0166     13.03       0.0133     12.98       0.0233     12.99       0.0233     12.99       0.0234     12.90	2 0.0 4.0 8.0 12.0 16.0 20.0 24.0 TIME (SECS)
0.0300 12.82 0.0333 12.74	෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧෧
0.0666 11.33 0.0833 11.38	WARZYN ENGINEERING, INC.
0.1000 11.46 0.1166 11.48 0.1333 11.53	MADISON. WISCONSIN
0.1530 11.52 0.1546 11.67	BALL DOWN ANALYSTS
0.1833 11.74 0.2000 11.75 0.2166 11.75	
0.2333 11.74 9.2500 11.72	
0.2855 11.72 0.2833 11.70 0.3000 11.70	BAIL DOWN PARAMETERS FOR 522
0.3146 11.70 0.3333 11.70	
0.5000 11.72 - 0.5333 11.70 -	
0.6667 11.70 0.7500 11.70 0.8333 11.77	EFECTIVE SCREEN DIAMETER = 2,000 INCHES
0.9167 11.72 1.9000 11.70	EFFECTIVE SCREEN LENGTH
1.1667 11.70 1.2500 11.70	WELL PENETRATION DEPTH - 04 740 FEET
1.3333 11.70 1.4165 11.70 1.5000 11.70	
1.5033 11.70 1.6667 11.70 1.700	STATIC WATER LEVEL
1.3333 11.70 1.9167 11.70	
2.0000 11.70 2.5000 11.70 3.0000 11.70	
3.5000 11.70 4.0000 11.70	UR .172E+04 GAL/FT/FT/DAY
5.0000 11.70 5.0000 11.70 5.5000 11.70	293E+03 CM*CM/SEC
6.3000 11.70 6.3300 11.70 7.4000 11.70	UR .203E+06 GAL/FT/DAY
7.5000 11.70 8.0000 11.70	**************************************
8.3090 11.70 9.0000 11.70 9.3000 11.70	START TIME IS = .120E+01 SECONDS
10.6390 11.70 END	END TIME IS = .400E+01 SECONDS

• `

.....



[3] E40



.160E+02 SECONDS

END TIME IS

SE1000B Environmental Logger 11/06 14:25						
Unit# 00168 T	esti 6					
IMPUT 1: Level	(F) TOC					
Reference Scale factor Offset	28.57 50.48 0.00					
Step# 0 11/06	11:33					
Elapsed Time	Value					
9.0000 0.003 0.0046 0.0099 0.0133 0.0165 0.0200 0.0233 0.0265 0.0300 0.0233 0.02500 0.0456 0.0333 0.0500 0.0456 0.0833 0.1500 0.1166 0.1833 0.1500 0.1166 0.2133 0.1500 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2133 0.2166 0.2166 0.2166 0.2133 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2166 0.2333 0.3000 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166 0.3166	27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 33.13 33.57 33.57 33.57 33.57 33.57 34.08 31.57 33.67 34.08 31.57 27.57 27.57 27.57 27.67 27.67 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.67 27.57 27.57 27.57 27.56 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.67 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66					

0000

416 500

915

27

27.54 27.64 27.54 27.54
		105		D			
SI Envi <i>ron</i> a	Lioecs Hental Logger		BAL	Ι ΠΩΤΩ		ST COLLOD	
11-0	5 18:46	L L	1 11 17			-21.200HR	
Unit# 00	168 Test# 0	· · · · · ·	-		E25		
INPUT 1:	Level (F) TOC	( 11	+++				
Reference Scale fact Offset	29.61 or 50.48 , 0.88	I (F T	* 4 4	.+.			
Step# 0	11/05 14:49			×++			
Elapsed Tim	ne Value			<u> </u>	. +-		
0.0000	29.91				×+		
0.0033 0.0066	29.91	문건			$\checkmark$		
0.0099	29.91 29.91	김 씨			$\mathcal{A}$		
0.0133	29.91	ㅋ				×, ∖	
0.0200	29.91	귀.				*	
0.0233	36.78					+	
0.0300	39.47	Ë					
0.0333	42.20	-+			· · · · · · · · · · · · · · · · · · ·		
0.0500	42.18	0.0	4.0	ຣ່.໐	12 0		
0.0833	39.85					10.0 20.	0 24.0
0.1000	35.74			I I ME	E (SEC	S)	
0.1333	34.24						
0.1500	32.11		8888888				
0.1666 0.1833	31.39		00000000	2666666666666666		666666666666666	6666
0.2000	30.47		WA	RZYNE	ENGINI	EERING, TI	
0.2166	30.18			MADIC	0 N		
0.2500	29.99				UN, WI	SCONSIN.	•
0.2666	29.76			BAIL	OWN A	NALYSİS	
0.3000	29.78 29.67		DATA	OBTAINED B	Y 1	CCP	
0.3166	29. 4		DATA			CON	
0.3333	29.62		DATA	HWHLYZED B	Υ:	CSR	
0.5000	29.57		BAIL	DOWN PARAM	ETERS FOR	E25	
0.5833 0.6667	29.57		666666666	000000000000000000000000000000000000000	କ୍ରକ୍ରକ୍ରକ୍ରକ୍ରକ୍ର	8866666666666	
0.7500	29.57		FFFFFF			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1666
0.8333 0.9167	29.56	•	CFFELIIV	E WELL DIAN	METER =	2.000 INCH	ES
1.0000	29.56		EFFECTIV	E SCREEN DI	AMETER =	2.000 INCH	<b>5</b> 0
1.0833	29.56		EFFECTIV	SCREEN LE	-		23
1.2500	29.56					5.000 FEET	
1.3331	29.57		WELL PENE	TRATION DE	PTH =	107.700 FEE1	г
1.0000	29.56		AQUIFER 1	HICKNESS	=	130.000 FEET	
1.5833	29.56		STATIC MA				
1.7500	29.57				2	29.610 FEET	
1.8333	29.57		AQUIFER C	ONDUCTIVIT	YIS =	.302E-01 CM/SE	C
2.0000	29.56				08	640E107 000	
2.5000	29.57				- Cit	.840E+03 GAL/F	T/FT/DAY
3.5000	29,57 29,57		HOUTER I	RHNSMISSIV	ITY IS =	.120E+03 CM*CM	/SEC
4.0000	29.57				OR	.832E+05 BAL /F	T/DAV
9.0000 5.0000	29.59 `` 29.57		****	**	****		
5.5000	29.59		CENCORSE		*********	#######################################	#
6.0000 6.5000	29.59		START TIM	ATA END PO	INTS ARE :	1	
7.0000	29.59					.000E+00 SECONI	os ·
7.5000	29.59		END TIME 1	S	-	.180E+02 SECONF	)5
3.5080	29.59 29.59						
9.0900	29.61						
7.5000 10.0000	29.61						
END	27.39						

		<sup>201</sup> لىبىد	RAW DATA A!	ND L:	ST.SQL	JARE FI	T
		-	E3	כ			
SE1000 Environmenta 11/05 1	)9 1 Logger 2:56		<b>.</b>				
Unit# 00168	Test# 5 🗁						
INPUT 1: Leve			TANK TANK				
		3 4	. ** <del>*</del> *				
Scale factor Offset	.50.48 T 0.00 U	001	<i>*</i>				
Step# 0 11/0	o5 07:35 ⊂	5 3	× + + +				
Elapsed Time	Value	-	<b>N</b> T -	* + +	+ + +	+ + + +	+
0.0000	20.88	4					
0.0033	20.88	5					
0.0099	25.44	-+		T		······	
0.0133	38.72	0.0	10.0 20.0 3	30.0	40.0	50.0	έο.o
0.0200	45.00			ດຕາ	w 1 O <sup>1</sup>		
0.0233	43.98		TIME (SE	CD1	*1U		
0.0300	37.64		· .				
0.0333	37.48						
0.0666	36.60		···· · ·				
0.0833	36.34						
0.1000	35.80						
0.1333	35.56						
0.1500	35.32 35.10	•	@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@	0000000	666666666666666666666666666666666666666	00000000	
0.1833	34.88		WARZYN ENG	INE	ERING	TNC	
0.2000	34.62 34.43						
0.2333	34.19		HADISUN.	WIS	CUNSI	Ν.	
0.2500	33.99 33.75		BAIL DOW	NAN	ALYSI	S	
0.2833	33.54		DATA OBTAINED BY :		CSR		
0.3166	· 33.14		DATA ANALYZED BY			•	
0.3333	32.92		-		Lak		
0.3000	31.95		BAIL DOWN PARAMETER	S FOR	E30		
0.5833	30.18		666666666666666666666666666666666666666	6666666	9999999999	96666666	
0.7500	29.40	· -	EFFECTIVE WELL DIAMETER	e _	2 000		
0.8333	27.99				2.000	INCHES	
1.0000	26.81		EFFECTIVE SCREEN DIAME	TER =	2,000	INCHES	
1.0833	26.29		EFFECTIVE SCREEN LENGT		5.000	FEET	
1.2500	25.36		WELL PENETRATION DEPTH	=	114 800	6667 <sup>.</sup>	
1.3333	24.96				114.800	FEE1	
1.5000	24.26		AUDIFER THICKNESS	=	117.000	FEET	
1.5833	23.96		STATIC WATER LEVEL	·	20.570	FEET	
1.7500	23.43		AQUIFER CONDUCTIVITY IS	5 <i>=</i>	.144F-02	CM/SEC	
1.8333	23.19					0	
2.0000	22.80			UR	.305E+02	GAL/FT/FT/D	AY
2.5000	21.98		AQUIFER TRANSMISSIVITY	IS =	.514E+01	CM*CM/SEC	
3.5000	21.28			OR	.357E+04	GAL/FT/DAY	
4.0000 4.5000	21.15		****				
5.0000	21.06			******	****	* # # # # # #	
5.5000	21.04		CENSORED DATA END POINT	S ARE :			
6.5000	21.03		CONTINUE 15	=	.100E+01	SECONDS	
7.0000	21.03		END TIME IS	=	180E+02	SECONDS	
7.5000 8.0000	21.03						
8.5000	21.03						
7.0000 9.5000	21.03 21.03						
10.0000	21.03						
END							

.

•

SE1000B	ł	י ד	\						
Environmental	Logaer	1	\		ροτο	0.00		000000	r- + <del>-</del>
12/03 15	: 24	- I	+\	ННW	UHIH	HINL	7 F21	. SUUHRE	FII
Unit# 00168	Test# 1		+	•	N	JU O	<b>-</b>		
INPUT 1: Level	(F) TOC	_ 1	4		ļ	IMA	۲		
Reference .	14.21	근 윜							
Scale factor Offset	50.48 0.00								
Step# 0 12/03	07:23	Z	*	١					
Elapsed Time	Value				-	+ <sup>+</sup> +			
0.0000	14.19	무귀		\	+		+		
0.0033	14.17	순 원					•		
0.0099	14.17								
0.0133	17.54								
0.0166	18.17	4							+
0.0233	18.76	-1							
0.0266	19.64			1					
0.0300	19.86	L L							
0.0500	19.16	-+-		T		r		·····	<u>-</u>
0.0666	17.41	0.0	) !	5.0	10.0	15	.0 20	0.0 25.0	30.0
0.0833	15.89				ттм				
0.1166	13.98				I I MI	EU	2EL21		
0.1333	13.49								
0.1666	13.28								
0.1833	13.52			•				•	
0.2000	13.82							•	
0.2333	14.40								
0.2500	14.54								
0.2833	14.37								
0.3000	14.36	0	000000 <b>00</b>	00000000	66666666	999999	000000000000000000000000000000000000000	966666666	
0.3166	14.21	•	WΑ	RZYN	ENGI	NEE	RING	. T N C.	
0.4167	14.09								
0.5000	14.25			MADI	5 O N. I	A I S	CONSI	N.	
0.6667	14.19			BAIL	D O W N	AN	ALYSI	S	
0.7500	14.17		DATA		BV .		<b>CCD</b>		
0.9167	14.17				5		LSK		
1.0000	14.17		DATA	ANALYZED	BY 1		CSR		
1.1667	14.17		BAIL	DOWN PAR	AMETERS F	FOR	MW9A		
1.2500	14.17	-							
1.3333	14.17	(g)	9999999999	866666666	966666666666	366666	00000000000	86666666	
1.5000	14.17	l	EFFECTIV	E WELL D	IAMETER	-	2.000	INCHES	
1.5833	14.17		EFFECTIV	E SCREEN	DIAMETER	2 =	2.000	INCHES	
1.7500	14.17					•	2.000	11101123	
1.8333	14.17	L L	FFECTIV	E SCREEN	LENGTH	=	10.000	FEET	
2.0000	14.17	I	HELL PEN	ETRATION	DEPTH	=	127.500	FEET	
2.5000	14.17	4		THICKNES	-	_ ·	120.000		
3.5000	14.17			INTERNES:	3	3	128.800	FEEI	
4.0000	14.16	9	STATIC W	ATER LEVE	IL.	=	13.280	FEET	
5.0000	14.16	"	QUIFER (	CONDUCTIN	JITY IS	=	.457E-01	CM/SEC	
5.5000	14.16								
- 6.0000 6.5000	14.16					OR	.968E+03	GAL/FT/FT/DAY	1
7.0000	14.14	4	QUIFER '	TRANSMISS	SIVITY IS	; =	.179E+03	CM+CM/SEC	
7.5000	14.14					00	1000.01		
8.5000	14.14					UR	.123E+06	GAL/FT/DAY	
9.0000	14.13	#1	*****	******	******	****	******	******	
7.5000 10.0000	14.13	ſ	ENSORED						
12.0000	14.11	5	START TI	ME IS		an <u>e</u> 1 a	.000E+00	SECONDS	
14.0000	14.11			10		_		0500105	
18.0000	14.09	. 6	IND ITTE	13		-	.810E+01	SECONDS	
20.0000	14.08								
22.0000	14.08								

.

END

•

		1	
SE1000	0B		
11/05 1	1 Logger 12:58		
		1 \+ HAW DATA AND LST.SQUARE FIT	
Unit# 00168	Test# 3		
INPUT 1: Leve	el (F) TOC	1 🕅 🔟 🖓 🖓	
Reference	16.75		
Offset	0.00		
Step# 0 11/0	04 16:21		
Elaosed Time	Value		
0.0000	- 47.22		
0.0055	- 47.24		
0.0099	- 47.25	₩ 3 \'''+.	
0.0133	- 47.24		
0.0200	- 41.58		
0.0233	- 39.01	· · ·	
0.0266	- 37.55		
0.0333	- 36.88		
0.0500	- 39.51		
0.0833	- 42.15	ייייי. גער המער הגיר הגיר ה.1 מ.8 ס.0	n
0.1000	- 45.52		.0
. 0.1166	- 46.35	TIME (SECS)	
0.1500	- 46.79		
0.1666	- 47.05		
0.1833	- 47.06		
0.2166	- 47.08		
0.2333	- 47.10		
0.2500	- 47.11	<b>ຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨ</b>	
0.2833	- 47.13		
0.3000	- 47.14	WARZYN ENGINEERING, INC.	
0.3333	- 47.14	MADISON. WISCONSIN.	
0.4167	- 47.18		
0.5000	- 47.19	BAIL DOWN ANALYSIS	
0.6667	- 47.21	DATA OBTAINED BY : CSR	•
0.7500	- 47.21		
0.8333	- 47.21	. DATA ANALYZED BY : CSR	
1.0000	- 47.21	BAIL DOWN PARAMETERS FOR W50 COR	
1.0833	- 47.21	<b>ຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨ</b>	
1.2500	- 47.22		
1.3333	- 47.22	EFFECTIVE WELL DIAMETER = 2.000 INCHES	
1.5000	- 47.22	EFFECTIVE SCREEN DIAMETER = 2.000 INCHES	
1.5833	- 47.21		
1.6667	- 47.21	EFFECTIVE SCREEN LENGTH = 5.500 FEET	
1.8333	- 47.22	WELL PENETRATION DEPTH = 55.600 FEET	
1.9167	- 47.22		
2.5000	- 47.22	AUDIPER (AICKNESS = 107.800 FEE)	
3.0000	- 47.22	STATIC WATER LEVEL = 29.550 FEET	
3.5000	- 47.22	ADVITE CONDUCTIVITY IS = $413E-01$ CM/SEC	
4.5000	- 47.21		
5.0000	- 47.21	OR .875E+03 GAL/FT/FT/DAY	
5.5000 6.0000	- 47.22 - 47.22	AQUIFER TRANSMISSIVITY IS = .134E+03 CM*CM/SEC	
6.5000	- 47.21		
7.0000	- 47.21	DR .943E+05 GAL/FT/DAY	
7.3000 8.0000	- 47.21	******	
8.5000	- 47.21		
9.0000	- 47.21	CENSORED DATA END POINTS ARE : START TIME IS = 1005+01 SECONDS	
10.0000	- 47.21		
END		END TIME IS = .300E+01 SECONDS	

•

.

l.

	Ng .
008 tal Logger 12:59	RAW DATA AND LST.SQUARE FIT
8 Test# 2	ъλ W50 REP
vel (F) TOC	
29.55 50.48 1.0.00 /04 16:01 Value	
27.48 27.48 27.48 27.48 27.48 27.48 27.48 27.48 27.48 27.48 27.48	
29.48 38.15	
37.28 34.73	
32.68	IIME (SEUS)
30.39	
29.93 29.74	· · · ·
29.67 29.67	
29.66	
29.66	<b>େଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜ</b>
29.64 29.62	WARZYN ENGINEERING, INC.
29.61	MADISON. WISCONSIN.
29.57	BAIL DOWN ANALYSIS
29.58 29.56	
29.56	
29.55	DATA ANALYZED BY : CSR
29.55 29.53	BAIL DOWN PARAMETERS FOR WSO REP
29.55	ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼
29.53	EFFECTIVE WELL DIAMETER = 2.000 INCHES
. 29.53 29.53	EFFECTIVE SCREEN DIAMETER = 2,000 INCUSE
29.55	
29.55	EFFECTIVE SUREEN LENGTH = 5.500 FEET
29.55 29.55	WELL PENETRATION DEPTH = \$5.600 FEET
29.55	AQUIFER THICKNESS = 107.800 FEET
29.55	STATIC WATER LEVEL = 29.550 FEET
29.55 29.53	AQUIFER CONDUCTIVITY IS = .475E-01 CM/SEC
29.53 29.53	
29.55	UK .101E+04 GAL/FT/FT/DAY
29.55	AQUIFER TRANSMISSIVITY IS = .156E+03 CM*CM/SEC
29.55 29.55	DR .108E+06 GAL/FT/DAY
27.55	****
27.55	CENSORED DATA END POINTS ARE :
29.53 29.55	START TIME IS = .200E+01 SECONDS
29.53	END TIME IS = .800E+01 SECONDS
27.33 29.55	
29.55	
27.00	

S Environ	E1000E mental	: 1.00	aer
11/	05 12	: 59	
Unit# O	0168	Test	# 2
INPUT 1:	Level	(F)	то
Reference		29	. 55
Offset	tor	. 0	. 48
Step# 0	11/04	16	:01
Elapsed T	ime	Val	ue
0,0000			
0.0033		27	. 48
0.0066		29	. 48 48
0.0133		29	. 48
0.0166		29	. 48
0.0200		29	. 48 48
0.0266		29	. 48
0.0300		29	. 48
0.0333		29	.48
0.0666		37	.28
0.0833		34	.73
0.1000		32	. 68
0.1333		30	. 39
0.1500		29	. 93
0.1866		29	- 67
0.2000		29	. 67
0.2166		29	. 66
0.2333		29	. 66
0.2666		29	. 64
0.2833		29	. 62
0.3166		29	.61
0.3333		29	. 57
0.4167		29	.58
0.5833		29	.56
0.6667		29	.55
0.7500		29	.55 .55
0.9167		29	.55
1.0000		29	.55
1.1667		29	.53
1.2500		. 29	.53
1.3333		29	.53
1.5000		29	.55
1.5833		29	.55
1.7500		29 29	.55
1.8333		29	. 35
1.9167		29	.55
2.5000		29	.55
3.0000		29	.53
3.5000		29	.53
4.5000		29	.55
5.0000		29	.55
6.0000		29	. 33 . 55
6.5000		29	. 55
7.0000		29	.55
8.0000		29	.53
8.5000		29	.53
9.0000 9.5000		29	.55
10.0000		29	.53
12.0000		29	. 55
14.0000		29	.55
END		£7	

		RAW DATA AND LST.SQUARE FIL
SE10 Environmen	100B Ital Logger	
11/05	12:52	
Unit <b># 00</b> 16	8 Test# 9	
INPUT 1: Le	wel (F) TOC	
Reference	27.75	
Scale factor Offset	50.48 0.00	
Step# 0 11	 ∕05 10:39	
Elapsed Time	Value	
9.0000	27.78	
0.0033	27.95 30.18	
0.0099	30.84	
0.0166	29.59 28.97	
0.0200	29.29	
0.0233	29.51 29.31	0.0 10.0 20.0 30.0 $40.0$ 50.0 $60.0$
9.0300	28.14	TIME (SECS) *10 <sup>1</sup>
0.0333	27.97 27.86	
0.0666	27.76	
0.0833 0.1000	27.71	
0.1166	27.79	•
0.1333 0.1500	27.67	
0.1666	27.67	
0.1833 0.2000	27.67	
0.2166	27.67	
0.2333 0.2500	27.67	୶ଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌ
0.2666	27.67	WARZYN ENGINEERING, INC.
0.2833 . 0.3000	27.67	MADISON. WISCONSIN.
0.3166	27.67	
0.3333 0.4167	27.67	BAIL DOWN ANALYSIS
0.5000	27.67	DATA OBTAINED BY : CSR
0.5833 0.6667	27.67 27.67	DATA ANALYZED BY : CSR
0.7509	27.67	
0.8333 0.9167	27.67 27.67	BAIL DOWN PARAMETERS FOR R35
1.0000	27.67	<b>େ</b> ଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜେଜ
1.1667	27.67 27.67	EFFECTIVE WELL DIAMETER = 2.000 INCHES
1.2500	27.67	FFECTIVE SCREEN DIAMETER = 2 000 INCHES
1.4166	27.67	
1.5000	27.67	EFFECTIVE SCREEN LENGTH = 6.970 FEET
1.6667	27.67	WELL PENETRATION DEPTH = 6.970 FEET
1.7500	27.67	AQUIFER THICKNESS = 110.000 FEET
1.9167	27.67	
2.0000 2.5000	27.67	STATIC WATER LEVEL = 27.750 FEET
3.0000	27.65	AQUIFER CONDUCTIVITY IS = .680E-01 CM/SEC
3.5000	27.65	DR .144E+04 GAL/FT/FT/DAY
4.5000	27.65	
3.0000 5.5000	27.65 27.65	· MWUITER IRHNSTISSIVIII IS = .228E+03 LM+LM/SEL
6.0000	27.65	OR .158E+06 GAL/FT/DAY
6.3000 7.0000	27.65 27.65	****
7.5000	27.63	
8.0000 8.5000	27.63 27.65	CENSURED DATA END PDINTS ARE : START TIME IS = .000E+00 SECONDS
9.0000	27.65	
9.5000	27.63	END TIME IS = .000E+00 SECONDS
END	_ 27.03	

.

,



WA	RZ	Y	N	ε	Ν	G	I	N	E (	ΞF	2	1 1	N (	3	• 1	[]	V	c.	
	MA	D	I	S		۱.	W	I	S	C	o	N	S	I	Ν.				
	ВА	I	L.	D	٥	ω	N	A	N	A	L	Y	s	I	s				
DATA	OBT	A 1 I	VED	в	۲ :					C	CSF	२							
DATA	ANA	LY:	ZEX	в	Y 1					C	CSF	२							
BAIL	DOW	NF	PAF		ETE	RS	3 F	OR		ŀ	121	L							

### 

EFFECTIVE WELL DIAMETER	=	2.000	INCHES
EFFECTIVE SCREEN DIAMETER	R =	2.000	INCHES
EFFECTIVE SCREEN LENGTH	-	10.000	FEET
WELL PENETRATION DEPTH	=	10.000	FEET
AQUIFER THICKNESS	= '	29.200	FEET
STATIC WATER LEVEL		35.850	FEET
AQUIFER CONDUCTIVITY IS	=	.103E-01	CM/SEC
	OR	.218E+03	GAL/FT/FT/DAY
AQUIFER TRANSMISSIVITY IS	6 =	.914E+01	CM+CM/SEC
	OR	.636E+04	GAL/FT/DAY
*****	*****	******	*****
CENSORED DATA END POINTS START TIME IS	ARE : =	.000E+00	SECONDS

arent	1102 15	-	.000E+00	SECUNDS
END TI	ME IS	=	.120E+02	SECONDS

SE1000 Environmenta 12/03 1	B 1 Logo <b>er</b> 5:25
Unit# 00168	Test# 0
INPUT 1: Leve	1 (F) TOC
Reference Scale factor Offset	37.00 50.48 0.00
Step# 0 12/0	2 08:14
Elapsed Time	Value
0.0000 0.0033 0.0046 0.0099 0.0133 0.0146 0.0200 0.0233 0.0246 0.0333 0.0246 0.0333 0.0500 0.0446 0.0833 0.1000 0.1146 0.1333 0.1500 0.1464 0.1833 0.1500 0.1464 0.2333 0.2500 0.2466 0.2833 0.2500 0.2466 0.2833 0.3000 0.2166 0.2333 0.2500 0.2466 0.2833 0.3000 0.3166 0.3333 0.4667 0.7500 0.5833 0.4667 1.0500 0.5833 1.1667 1.2500 0.8333 1.1667 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.5833 1.4167 1.0000 0.5833 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.2500 0.8333 1.4167 1.0000 0.5500 0.5500 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.55000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.50000 0.500000000	35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.864 35.555 35.5555 35.5555 35.555555 35.55555555

END



END

SE Environ	1000B Jental Logger	с. С	
11/0 Unit# 00	5 12:53 168 Test# 8	BAW DATA AND LST SOUDE	<b>[</b> ], 1
INPUT 1:	Level (F) TOC		ΓIΙ
Reference	29,00	ĩ₄ R3D	
Scale facto Offset	or 50.48		
Step# 0 j	11/05 10:00	L ±	
Elapsed Tin	ne Value		
0.0000	28.12		
0.0055	28.12		
0.0099	28.39	お 特 (1)	
0.0133	29.68		
0.0166	31.21		
0.0233	32.79 .74 75	Ξ \ <del>'</del>	
0.0266	35.86		
0.0300	37.30	-{	
0.0333	38.38		
0.0666	39.28		+
0.0833	33.55		
0.1000	31.78	0.0 10.0 20.0 30.0 00.0 50.0	
0.1166	30.88		60.0
0.1500	30.24	$IIME^{\circ}$ (SECS) $*10^{1}$	
0.1666	27.76		
0.1833	29.11		
0.2000	28.90		
0.2333	28.76	ୢ	
0.2500	28.58		
0.2666	28.53	WARZYN ENGINEERING, INC	
0.2833	28.49		
0.3166	28.45	MADISON. WISCONSIN.	
0.3333	28.39	BAIL DOWN ANALYSTS	
0.4167	28.31		
0.5833	28.28	DATA OBTAINED BY : CSR	
0.6667	28.25	DATA ANALYZED BY	
0.7500	28.23		
0.8333	28.23	BAIL DOWN PARAMETERS FOR R3D	
1.0000	28.21	000000000000000000000000000000000000000	
1.0833	28.21		
1.1667	28.21	EFFECTIVE WELL DIAMETER = 2.000 INCHES	
1.3333	28.20	EFFECTIVE SCREEN DIAMETER - C 000 DURING	
1.4166	28.20	2.000 INCHES	
1.5000	28.20	EFFECTIVE SCREEN LENGTH = 10.000 FEET	
1.6667	28.20	WELL PENETRATION DEBTU	
1.7500	28.20	110.000 FEET	
1.8333	28.20	AQUIFER THICKNESS = 110.000 FEET	
2.0000	28.20	STATIC WATER LEVEL	
2.5000	28.18	STATIE WATER LEVEL = 28.180 FEET	
3.0000	28.18	AQUIFER CONDUCTIVITY IS = .858E-02 CM/SEC	
3.5000	28.18		
4.5000	28.18	OR .182E+03 GAL/FT/FT/DAY	
5.0000	28.18	AQUIFER TRANSMISSIVITY IS	
5.5000	28.18	2682+02 LM+LM/SEC	
6.0000 6.5000	28.20	OR .200E+05 GAL/FT/DAY	
7.0000	28.18	***	
7.5000	28.18	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
8.0000	28.18	CENSORED DATA END POINTS ARE :	
8.0000 9.0000	28.18	START TIME IS = .300E+01 SECONDS	
9.5000	28.18	END TIME IS	
10.0000	28.18	- SOUE+02 SECONDS	
CIND			

		·· .						
						•	:	
			•		:			
					•		ν.	
SE1000B Environmental 11/05 12	Logger	01						
Upit# 00149								
INPUT 11 Level	(5) 100	1	RAW	DATA A	AND	LST.S	QUARE F	TT
Reference	70 00	Ţ		0				
Scale factor Offset	50.48 0.00	· _ _ ⊵ ₩			ξΟ			
Step# 0 11/05	09:01 · F		" <del>*</del>					
Elapsed Time	Value		1 <del>}</del>					
0.0000	29.98			K., _				
0.0066	34.09	5_1		' <del>*</del> *		4		
0.0133	32.48	듣 닠		×	4			
0.0200	31.54 31.48				_¥	ι.		
0.0233 0.0266	31.35 L 31.32				·	* '		
0.0300	31.21	4				+4	<del>t</del> +	
0.0500	30.89	~						
0.0822	30.70	5						
0.1166	30.46 30.36	0.0	· · · · · · · · · · · · · · · · · · ·	8.0	12.0	16.0		
0.1333 0.1500	30.27 30.22			TIME	(00			24.0
0.1666 0.1833	30.19			IIME	(DE	.631		
0.2000	30.12							
0.2333	30.07	,						
0.2500	30.06 30.04		GGGGGGGGGGGGGGGGGGG		000000	000000000000000000000000000000000000000	36666666	
0.2833 0.3000	30.04 30.03		WARZ	YNENGI	NEE	RING	, I N C.	
0.3166 0.3333	30.03		MAI	DISON.	WISO	CONSI	N.	
0.4167	30.00		ВА	IL DOWN	AN	ALYSI	S	
0.5833	29.98		DATA OBTA	INED BY :		CSR		
0.7500	29.98		DATA ANAL	YZED BY :		CSR		
0.9167	29.98 <sup>.</sup> 29.98		BAIL DOWN	PARAMETERS	FOR	C4S		
1.0000	29.98 29.98		666666666666666666666666666666666666666	699999999999	0000000	2000000000	26666666	
1.1667 1.2500	29.98 29.98		EFFECTIVE WEL	LL DIAMETER	=	2.000	INCHES	
1.3333 1.4166	29.96		EFFECTIVE SC	REEN DIAMETE	R =	2,000	INCHES	
1.5000	29.98		EFFECTIVE SC	REEN LENGTH		4 740	FEFT	
1.6667	29.98		WELL PENETRA		_	4.740		
1.8333	29.98		ACUICED THE		-	4.740	FEEI	
2.0000	29.98		AGOIFER THICK	(NESS	=	130.000	FEET	
2.5000 3.0000	29.96 29.96		STATIC WATER	LEVEL	-	30.000	FEET	
. 3.5000 4.0000	29.96 29.96		AQUIFER CONDL	JCTIVITY IS	=	.137E-01	CM/SEC	
4.5000 5.0000	29.96				OR	.290E+03	GAL/FT/FT/DAY	/
5.5000	29.96		AQUIFER TRANS	SMISSIVITY I	S =	.542E+02	CM*CM/SEC	
6.5000 7.0000	29.96				OR	.376E+05	GAL/FT/DAY	
7.5000	27.76		****	*****	*****	******	****	
8.5000	27.96 29.96		CENSORED DATA	END POINTS	ARE :			
9.0000 9.5000	29.96 29.96		START TIME IS	5	=	.600E+00	SECONDS	
10.0000 END	29,96		END TIME IS		<b>2</b> 2	.200E+02	SECONDS	
·								
	· . 				7.		•	
	ζ.				• •			
÷					<i></i> .		*	



÷



		<u></u>	
SELOOO	P	ž] U25	
Environmenta	al Logger		
12/03 1	5:23		
Unit# 00168	Test# 2		
	10307 2		
INPUT 1: Leve	A1 (F) TOC	· · · · · · · · · · · · · · · · · · ·	
Reference	32.71		
Scale factor	50.48		•
UT Set		;≓ ∽↓∔	
Step# 0 12/0	3 09:32	╔╴╾┥	
Elapsed Time	Value		
0.0000	32.69	∾┤₩┽ ┽ ┽ ┽ ┼	
0.0046	33.10	N	
0.0099	33.07		
0.0166	32.69		
0.0200	32.93		.0
0.0233	33.22	TIME (SECS)	
0.0300	33.14		
0.0333	33.04		
0.0566	32.74		
0.0833	32.72		
0.1166	32.71	·	
0.1333	32.69		
0.1500	32.71		
0.1833	32.69		
0.2000	32.69	୫ <b>୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫୫</b> ୫୫୫୫୫୫	
0.2333	32.69	WARZYN ENGINEERING ING	
0.2500	32.69	A A A C A C A O I NEEKING, INC.	
0.2833	32.69	MADISON. WISCONSIN.	
0.3000	32.69	BAIL DOWN ANALYSIS	
0.3333	32.69		
0.4167	32.69	DATH OBTHINED BY : CSR	
0.5000	32.69	DATA ANALYZED BY : CSR	
0.6667	32.69	BAIL DOWN PARAMETERS FOR COS	
0.7500	32.69		
0.9167	32.69	୴୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶୶	
1.0000	32.71	EFFECTIVE WELL DIAMETER = 2.000 INCHES	
1.1667	32.69	EFFECTIVE SCREEN DIAMETER - 2 000 INCUSO	
1.2500 1.5333	32.69	2.000 INLHES	
1.4166	32.69	EFFECTIVE SCREEN LENGTH = 5.200 FEET	
1.3000	32.69	WELL PENETRATION DEPTH = 5.200 FEET	
1.6667	32.69	ADUTEER THICKNESS	
1.7500	32.69	HOUT EN INTERNESS 4 117.310 FEET	
1.8333	32.69 32.71	STATIC WATER LEVEL = 32.690 FEET	
2.0000	32.69	AQUIFER CONDUCTIVITY IS = .430E-01 CM/SEC	
2.5000	32.69		
3.5000	32.69	DR .911E+03 GAL/FT/FT/DAY	
4.0000	32.69	AQUIFER TRANSMISSIVITY IS = .154E+03 CM+CM/SEC	
5.0000	47.59		
5.5000	47.59	UK .107E+06 GAL/FT/DAY	
6.0000 6.5000	47.59 47.59	*****	
7.0000	47.59	CENSORED DATA END POINTS ARE	
7.5000	47.59	START TIME IS = .000E+00 SECONDS	
8.5000	47.59	END TIME IS	
9.0000	47.59		
10.0000	47.59 47.59		

END

.

.

. .

			-
SE Environ 11/0	E1000B mental 05 13:	Logg 01	er
Unit# 00	168	Fest#	0
INPUT 1:	Level	(F)	TOC
Reference Scale fact Offset	or	32. •50. 0.	21 48 00 .
Step# 0	11/04	07:	42
Elapsed Ti	.me	Valu	e 
0.0000 0.0033 0.0046 0.0079 0.0133 0.0166 0.0200 0.0233 0.0266 0.0233 0.0266 0.0333 0.0266 0.0333 0.0500 0.0666 0.1333 0.1500 0.1166 0.1833 0.2500 0.2166 0.2333 0.2500 0.2166 0.2333 0.2500 0.2466 0.2333 0.2500 0.2466 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.2500 0.2666 0.2833 0.9147 1.2500 0.8333 1.1667 1.2500 1.8333 1.1667 1.2500 1.8333 1.9167 2.0000 2.5000 3.5000 3.5000 4.5000 5.5000 5.5000 6.0000 6.5000 7.5000 8.0000		322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   322. 322.   323. 322.   323. 323.   322. 323.   322. 323.   322. 323.   322. 323.   323. 323.   323. 323.   323. 323.   323. 323.   323. 323.   323. 33.   323. 33.   323. 33.   323. 33.   323. 33.   323. 33.   33. 33.   33. 33.   33.	
9.0000 9.0000		32.0 32.0 32.0	26 26



WARZYN ENGINEERI<sup>®</sup>NG, INC. MADISON. WISCONSIN. BAIL DOWN ANALYSIS DATA OBTAINED BY : CSR DATA ANALYZED BY : CSR

BAIL DOWN PARAMETERS FOR WSS ·

	EFFECTIVE WELL DIAMETER	-	2,000	INCHES
	EFFECTIVE SCREEN DIAMETE	R =	2.000	INCHES
	EFFECTIVE SCREEN LENGTH	=	5.000	FEET
	WELL PENETRATION DEPTH	=	83.300	FEET
	AQUIFER THICKNESS	=	97.600	FEET
	STATIC WATER LEVEL		32.210	FEET
	AQUIFER CONDUCTIVITY IS	=	.699E-02	CM/SEC
		OR	.151E+03	GAL/FT/FT/DAY
	AQUIFER TRANSMISSIVITY I	S =	.198E+02	CM*CM/SEC
		OŖ	.137E+05	GAL/FT/DAY
ŧ	******	#####	*******	****
	CENSORED DATA END POINTS START TIME IS	ARE	: .300E+01	SECONDS

.300E+01 SECONDS END TIME IS .300E+02 SECONDS

END

10.0000

SE10 Fovironmen			
11/05	13:00		
Unit# 0016	8 Test# 1		
INFUT 1: Le	vel (F) TOC		
Reference	32.21		
Scale factor	50.48		
Utfset	0.00	$\Xi$ $\downarrow$	
Step# 0 11.	/04 10:19		
Elapsed Time	Value	· 두 뇌 · · · · · · · · · · · · · · · · ·	
0.0000	31.17		
0.0033	31.17		
0.0088	31.17	4	
0.0133	31.18	┥., ++	
0.0166	31.20	4 .	
0.0200	31.18	2	
0,0266	31.18		
0.0300	35.97		0 0
0.0333	40.91		0.0
0.0666	42.09	TIME (SECS)	
0.0833	40.51		
0.1000	39.82		
0.1333	39.20	- (M -	
0.1500	38.12		
0.1666	37.64		
0.1833	37.21		
0.2166	36.44	000000000000000000000000000000000000000	
0.2333	36.09	୶୶୷୶୶ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼	
0.2566	35.79	WARZYN ENGINEERING, INC.	
0.2833	35.23		
0.3000	34.98	ABISON. WISCONSIN.	
0.3333	34.55	BAIL DOWN ANALYSIS	
0.4167	33.75		
0.5833	33.21		
0.6667	32.64	DATA ANALYZED BY : CSR	
0.7500	32.49	BAIL DOWN PARAMETERS FOR USS BED	
0.8333	32.40		
1.0000	32.28	୕ୖଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌଌ	
1.0833	32.27	EFFECTIVE WELL DIAMETER = 2,000 INCHES	
1.2500	32.24		
1.3333	32.22	2.000 INCHES	
1.4166	32.22	EFFECTIVE SCREEN LENGTH = 5.000 FEET	
1.5833	32.21		
1.6667	32.21	B3.300 FEET	
1.8333	32.21	AQUIFER THICKNESS = 97.600 FEET	
1.9167	32.21	STATIC WATER LEVEL	
2.0000	32.21	STATES WATCH CLACE IN S2.210 FEET	
3.0000	32.21	AQUIFER CONDUCTIVITY IS = .692E-02 CM/SEC	
3.5000	32.21		
4.0000	32.21	IN .14/E+US GAL/FT/FT/DAY	
5.0000	32.19	AQUIFER TRANSMISSIVITY IS = .206E+02 CM*CM/SEC	
5.5000	32.21		
6.0000 6.5000	32.21	. UN .143E+05 GAL/FT/DAY	
7.0000	32.21	****	
7.5000	32.21	CENSURED DATA FUD POINTS ADD	
8.0000 8.5000	32.21	START TIME IS = .290E+01 SECONDS	
9.0000	32.21		•
9.5000	32.21	END TIME IS = .600E+02 SECONDS	
10.0000	32.21		

END

			10 <sup>0</sup> 10 <sup>1</sup>		RA	N DATA	AND L W55A	ST.SQL	IARE	FIT
		 10	DRAWDOWN (FT) 10-2 10-1			+			+	+ +
	Environmenti 11/06	ai Logger 14:36	'n							
	INPUT 1: Leve	I (F) TOC	01	4						<u>-</u>
• •	Reference Scale factor Dffset	32.40 50.48 0.00		0.0	10.0	20.0 TIME	30.0 (SECS)	40.0 √1∩ <sup>1</sup>	50.0	60.0
	Step# 0 11/0	06 07:50 -				1 1110		*10		
	0.0000	32.24	•							
	0.0055	31.93 32.09 32.76	•						-	
	0.0166 0.0200 0.0233	32.25 32.06								
	0.0266 0.0300 0.0333	32.38 32.25 33.93	. @@		8686666666	366666666666				
	0.0500 0.0666 0.0833	33.24 33.18 33.11		WA	RZYN	ENGIN	EERING	, INC.		
	0.1000 0.1166 0.1333	33.06 33.00 32.95			MADIS	30N. W	ISCONS	IN.		
	9.1500 0.1566 0.1833	32.92 32.87 32.84			BAIL	DOWN	ANALYS	IS		
	0.2000 0.2166 0.2333	32.83 32.79 32.76		DATA		BY :	CSR			
	0.2500 0.2666 0.2833	32.75 32.73 32.71		BATI	DOWN PAR	BY : METERS EN	USR 8 11550			
	0.3000 0.3166 0.3333	32.70 32.67 32.65	ee	000000	000000000000000000000000000000000000000		666666666666666666666666666666666666666	666666666		
	0.4167 0.5000 0.5833	32.59 32.55 32.52	۰E	FFECTI	VE WELL D	AMETER	= 2.00	0 INCHES		·
:	0.6567 0.7500 0.8333	32.49 32.47 32.46	E	FFECTI	VE SCREEN	DIAMETER	= 2.00	0 INCHES		
	0.9157 1.0000 1.0833	32.46 32.44 32.44	E	FFECTI	VE SCREEN	LENGTH	= 10.00	O FEET		
	1.1667 1.2500 1.3333	32.44 32.43 37.43	ы	ELL PE	NETRATION	DEPTH	= 10.00	O FEET		
	1.4166 1.5000	32.43 32.43	A	QUIFER	THICKNES	6	<b>□ 97.6</b> 0	0 FEET		
	1.8667	32.43 32.41 32.41	S	TATIC I	WATER LEVE		= 32.,40	O FEET		
	1.9167	32.41 32.41 32.41	A	QUIFER	CONDUCTIN	VITY IS	= .189E-0	2 CM/SEC		
	2.5000 3.0000 3.5000	32.40 32.40 32.41	~	011550	TRANCHIC		R .402E+0	2 GAL/FT/FT	T/DAY	
	+.0090 4.5000 5.0000	32.40 - 32.43 32.40	H	2017 EK	11921122	UI 1711112	024E+0		-	•
	5.5000 6.5000 6.5000	32.40 32.40 32.40	**	*****	*****	******	*****	- GHL/PI/DF	• (	
	7.0000 7.5000 8.0000	32.40 32.40 32.41	CI	ENSORE	D DATA END	POINTS A	RE :			
	8.5000 9.0000 9.5000	32.40 32.40 32.41	S	TART T	IME IS	•	= .200E+0	1 SECONDS		
	10.0000 END	32.41	E	ND TIME	E IS		= .500E+0	2 SECONDS		

• •

. ;

. . .

.

APPENDIX J GROUNDWATER MODEL INPUT PARAMETERS U.S. GEOLOGICAL SURVEY MODULAR FINITE-DIFFERENCE GROUND-WATER MODEL

run at 10:53:58 on 9-FEB-88 Wausau - transient, 1 layer, pumps on 1 LAYERS 69 ROWS 36 COLUMNS 138 STRESS PERIOD(S) IN SIMULATION MODEL TIME UNIT IS SECONDS input file list block.dat pump78.dat river44.dat rech-nw-peri.dat sip.dat output.dat nodal.dat volcty.dat I/O UNITS: ELEMENT OF IUNIT: 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 I/O UNIT: 7 8 0 9 0 0 0 10 11 0 0 12 13 14 0 0 0 0 0 0 0 0 0 0 BAS1 -- BASIC MODEL PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM UNIT 5 ARRAYS RHS AND BUFF WILL SHARE MEMORY. START HEAD WILL NOT BE SAVED -- DRAWDOWN CANNOT BE CALCULATED 19981 ELEMENTS IN X ARRAY ARE USED BY BAS 19981 ELEMENTS OF X ARRAY USED OUT OF 200000 BCF1 -- BLOCK-CENTERED FLOW PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM UNIT 7 TRANSIENT SIMULATION LAYER AQUIFER TYPE -----------------1 1 7453 ELEMENTS IN X ARRAY ARE USED BY BCF 27434 ELEMENTS OF X ARRAY USED OUT OF 200000 WEL1 -- WELL PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM 8 MAXIMUM OF 8 WELLS 32 ELEMENTS IN X ARRAY ARE USED FOR WELLS 27468 ELEMENTS OF X ARRAY USED OUT OF 200000 RCH1 -- RECHARGE PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM UNIT 10 OPTION 1 -- RECHARGE TO TOP LAYER 2484 ELEMENTS OF X ARRAY USED FOR RECHARGE 29950 ELEMENTS OF X ARRAY USED OUT OF 200000 RIV1 -- RIVER PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM UNIT 9 MAXIMUM OF 366 RIVER NODES CELL-BY-CELL FLOWS WILL BE PRINTED 2196 ELEMENTS IN X ARRAY ARE USED FOR RIVERS 32146 ELEMENTS OF X ARRAY USED OUT OF 200000 SIP1 -- STRONGLY IMPLICIT PROCEDURE SOLUTION PACKAGE, VERSION 1, 12/08/83 INPUT READ FROM UNIT 11 MAXIMUM OF 100 ITERATIONS ALLOWED FOR CLOSURE **5 ITERATION PARAMETERS** 10341 ELEMENTS IN X ARRAY ARE USED BY SIP 42487 ELEMENTS OF X ARRAY USED OUT OF 200000 Wausau - transient, 1 layer, pumps on

												80		DAR)	( AF	RAY	/ F(	DR I		R	1	WILL	. B	ER	EAD	ON	UN	ст 2	25 (	JSIN	IG F	FORI		:			 (	3613	)
	1	2	3	4	5	8	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	28	27	28	29	30	31	32	33	34	35	36	 		-
1 2	0 0	0	0 0	0	0 0	0	0	0	0	0	0	0 0	0	 0 0	1	1	1 1 1	1 1	1	1	1	1 1	1 1	1	1 1 1	1 1	0 0	0 0	 0 0										

3 4 5 6 7 8 9 0 1 1 2 3 4 1 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 3 4 5 6 7 8 9 0 1 2 3 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 3 4 5 6 7 8 9 0 1 2 3 3 3 3 3 3 3 3 3 4 5 6 7 8 9 0 1 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	011111111111000000000000000000000000000	011111111111111110000000000000000000000	011111111111111111000000000000001111111	01111111111111111100000000000000000001111	011111111111110000000000000000000000000	011111111111110000000000011111111111111	011111111111111101111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	011111111111111111111111111111111111111	111111111111111111111111111111111111111	111111111111111111111111111111111111111	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	111111110000000000000000000000000000000	111000000000000000000000000000000000000	000000000000000000000000000000000000000
45	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	ī	1	1	1 ·	1	1	1	ī	1	i	ī	1	1	1	1 1	ō	Ō	o o
47	0	ŏ	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 1	1	1 1	1	1 1	1 1	1 1	$\begin{array}{c}1 \\ 1 \end{array}$	L L	1 1	1 1	1 1	1	$\begin{array}{ccc} 1 & 1 \\ 1 & 1 \end{array}$	0	0	0 0
48 49	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 1		1	1	1	1	1 1	0	0	0
50	ŏ	ŏ	1	i	1	i	i	i	1	i	ī	i	ī	i	1	i	1	1	1	1	1	1	1	1	1 1	L L	1	1	1	1	1 0	ŏ	ŏ	
51 52	0	0	1	1	1	1	1	1	1	1	1 1	1	1 1	1 1	1 1	1	1	1	1 :	1	1	1 1	1	1 1	1 1		1 :	1	1	1	1 1 1 1 0	0	0 0	
53	Ō	Ō	1	1	1	1	1	1	1	ī	1	ī	1	1	1	ī	1	1	i :	1	i '	<b>i</b> '	i :	1	i i	<b>i</b> :	1	i	i	i	i ŏ	ŏ	ŏ	ŏŏ
54 55	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 1		1	1	1	1	1 0	0	0 0	0
56	ŏ	ŏ	ī	i	i	i	ī	1	i	i	ī	i	1	i	1	1	1	1	1 3	1	1	1	1	1	1 1	L :	1	1	1	1	$\begin{array}{c} 1 \\ 1 \\ \end{array}$	ŏ	0 0	
57 58	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 1		1		1	1	1 1	0	0	0 0
59	ŏ	ŏ	ŏ	ī	i	ī	1	1	ī	1	1	1	1	1	1	1	1	1	1 1	1	1	1	1 :	1	1 1 1 1	L :	1	1	1	1	1 0	0		0 0
60 81	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 1	L	1	L	1	1	o ō	Ō	Ō	0
61 62	0	0	0	0	1	1	1 1	1 1	1	1 1	1 :	1 :	1 1	1	1	1	1 :	1	11		1 :		1	1	1 0	0	0 0							
63	ō	ō	ō	ō	ī	ī	1	1	ī	1	ī	1	ī	ī	ī	ī	ī	i	<b>i</b> i	i	<b>i</b> :	i	i	i :	1 1		<b>i</b> :	. :	i	1	οŏ	ŏ	ŏč	$\tilde{\mathbf{b}}$

÷.

64	ο	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0	0
65	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	Ó	Ó	Ō	Ō	ō	Ō
66	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0	0
87	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0	0
68	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0
69	0	0	1	1	1	1	1.	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0
AQUII	FER	HEA	DW	ILL/	BE	SE	ΤТ	0	123	0.0			TA	LL	NO-	FLO	₩N	ODE	S (	IBO	UND	=0)	•													

--------

.

# INITIAL HEAD FOR LAYER 1 WILL BE READ ON UNIT 26 USING FORMAT: (10f8.0)

λ.

	1 16	2 17	3 18	4 19	5 20	8 21	7 22	8 23	9 24	10 25	11 26	12 27	13 28	14 29	15 30
	31	32	33	34	35	36									
1	1265.1	1290.1	1290.1	1290.1	1251.4	1230.1	1230.1	1230.1	1230.1	1230.1	1230.1	1230.1	1230.1	1218.9	1221.8
	1223.2	1222.3	1224.0	1222.7	1215.9	1208.4	1187.9	1187.9	1187.9	1187.9	1187.9	1187.9	1187.9	1187.9	1187.9
•	1187.9	1188.4	1188.8	1221.9	1288.7	1290.1									
2	1230.1	1290.1	1290.1	1290.1	1230.1	1230.1	1230.1	1200.1	1200.1	1200.1	1200.1	1200.1	1200.1	1200.1	1200.1
	1190.1	1190.1	1190.1	1190.1	1180.2	11/5.1	1188.0	1187.8	1187.9	1181.8	1187.9	1187.9	1187.9	1187.9	1187.9
2	107.8	107.8	1168.2	1217.8	1200.1	1380.1	1020 1	1000 1	1200 1	1200 1	1000 1	1000 1	1000 1	1000 1	1000 1
3	1200 1	1230.1	1203.0	1230.1	1230.1	1230.1	1230.1	1230.1	1200.1	1200.1	1100.1	1200.1	1200.1	1200.1	1200.1
	1187 9	1187 9	1188 1	1188 3	1250.1	1200.1	1200.1	1200.1	1200.1	1200.1	1180.1	1190.1	1160.1	1101.4	1191.9
4	1471.7	1434.9	1384 0	1332 7	1202.2	1283 A	1249 8	1242 2	1238 0	1234 8	1232 A	1230 9	1220 2	1227 B	1228 0
-	1224.1	1222.0	1219.4	1215.8	1209.2	1198.0	1189.8	1189.0	1188.9	1188.7	1188.8	1188 4	1188 1	1199 0	1127 0
	1187.9	1187.9	1188.0	1188.0	1200.1	1279.6						1100.4		1100.0	1107.0
Б	1471.5	1434.1	1379.6	1321.6	1270.2	1234.5	1223.8	1217.8	1214.0	1211.2	1209.3	1207.8	1208.5	1205.1	1203.8
	1202.5	1201.0	1199.4	1197.4	1195.0	1191.7	1188.9	1187.9	1187.8	1187.7	1187.6	1187.5	1187.5	1187.6	1187.8
	1187.9	1187.9	1187.9	1187.9	1228.2	1252.7									
6	1471.4	1433.2	1374.5	1306.6	1251.3	1222.0	1211.0	1204.8	1201.4	1198.9	1197.3	1196.2	1195.1	1194.2	1193.3
	1192.4	1191.5	1190.7	1189.8	1188.8	1187.4	1186.5	1186.5	1186.6	1186.6	1186.7	1186.8	1186.9	1187.2	1187.6
	1187.9	1187.9	1187.9	1202.3	1239.2	1230.6									
7	1471.4	1432.6	1369.7	1296.5	1245.2	1217.2	1204.3	1197.6	1194.6	1192.5	1191.2	1190.2	1189.4	1188.7	1188.0
	1187.4	1186.8	1186.5	1186.3	1186.1	1186.0	1186.0	1186.0	1186.1	1186.2	1186.3	1186.4	1186.6	1186.9	1187.3
	1187.9	1187.9	1187.9	1230.0	1248.3	1234.1									
8	1471.3	1432.2	1366.6	1293.8	1242.9	1214.5	1202.1	1194.0	1192.0	1190.4	1189.2	1188.4	1187.7	1187.1	1186.6
	1186.3	1186.1	1185.9	1185.8	1185.7	1185.7	1185.7	1185.7	1185.8	1185.9	1185.9	1186.1	1186.3	1186.6	1187.2
	1187.9	1187.9	1187.9	1220.7	1241.2	1240.7									
8	1471.3	1431.8	1364.0	1292.3	1241.5	1212.6	1199.0	1192.7	1190.8	1189.3	1188.1	1187.3	1186.8	1186.4	1186.2
	1188.0	1185.8	1185.7	1185.6	1185.5	1185.4	1185.4	1185.4	1185.4	1185.5	1185.6	1185.7	1185.9	1186.4	1187.1
••	1187.9	1187.9	1187.9	1244.5	1243.0	1249.1									
10	14/1.3	1431.6	1362.0	1291.6	1240.8	1211.0	1195.9	1192.1	1190.0	1188.3	1187.0	1188.7	1186.4	1186.1	1185.9
	1185.8	1185.6	1185.5	1185.4	1185.3	1185.3	1185.2	1185.2	1185.2	1185.2	1185.3	1185.5	1185.8	1188.2	1187.0
	1471 2	1187.9	1187.9	1258.8	1247.7	1265.9	1105 0	1101 0	1100 0	1107 0	1100 0	1100 5		1100 0	
11	14/1.3	1431.4	1300.3	1291.4	1240.5	1210.0	1190.2	1191.0	1108.0	110/.9	1100.8	1180.8	1186.3	1186.0	1185.8
	1100./	1100.0	1100.0	1100.4	1100.3	1180.2	1185.1	1189.1	1180.1	1100.2	1185.2	1185.4	1185.5	1186.1	1187.0
12	1471 2	1421 2	1211.2	1203.0	1240.3	12/2.0	1104 0	1101 0	1100 0	1107 B	1108 7	1108 E	1100 0	1100 0	1105 7
12	14/1.3 1195 7	1431.3 1105 A	1300.0 1195 E	1195 4	1195 2	1105 1	1194.2	1191.0	1108.2	1107.0	1100.7	1100.0	1100.2	1100.0	1100./
	1197 0	1197 0	1201 0	1289 0	1244 9	1282 B	1100.0	1100.0	1100.0	1100.0	1100.1	1100.3	1100.0	1100.0	1107.0
13	1471 2	1431 2	1358 7	1200.0	1240 4	1202.0	1103 3	1190 4	1188 8	1187 4	1188 R	1198 4	1198 2	1198 0	1195 0
	1185 7	1185 A	1185 5	1185 3	1185 2	1185 0	1184 9	1184 8	1184 8	1184 0	1185 0	1195 2	1105.2	1198 0	1107.0
	1187.9	1187.9	1240.9	1280.5	1247 7	1285.3	1104.0	1104.0	110410	1104.0	1100.0	1100.2	1100.4	1100.0	1107.0
14	1471.2	1431.2	1354.8	1292.9	1240.4	1208.8	1192.2	1189.8	1188.4	1187.2	1188.4	1188.3	1188 1	1188 0	1185 8
	1185.7	1185.6	1185.4	1185.3	1185.1	1184.9	1184.7	1184.5	1184.4	1184.6	1184.9	1185.1	1185.4	1186.0	1187.1
	1187.9	1187.9	1250.2	1271.9	1259.5	1281.5									
15	1242.7	1230.1	1352.7	1294.2	1240.5	1208.7	1188.5	1189.1	1188.1	1187.1	1186.4	1186.3	1186.1	1186.0	1185.8
	1185.7	1185.6	1185.4	1185.3	1185.1	1184.9	1184.6	1184.2	1183.8	1184.3	1184.7	1185.1	1185.4	1186.0	1187.3

	1187.9	1187.9	1282.7	1257.9	1255.5	1277.8										
16	1247.8	1230.1	1351.0	1298.0	1240.5	1208.9	1188.9	1188.6	1187.8	1187.0	1186.4	1186.3	1186.1	1186.0	1185.8	
	1185.7	1185.6	1185.4	1185.3	1185.1	1184.9	1184.5	1183.8	1182.4	1183.9	1184.6	1185.1	1185.4	1188.2	1187.6	
	1187.9	1187.9	1259.0	1280.3	1274.0	1330.9										
17	1245.9	1230.1	1349.5	1298.3	1208.4	1209.5	1188.8	1188.3	1187.7	1187.0	1188.4	1186.3	1186.2	1186.0	1185.9	
	1185.7	1185.8	1185.4	1185.3	1185.2	1185.0	1184.7	1184.4	1184.0	1184.5	1184.9	1185.2	1185.5	1186.3	1187.7	
	1187.9	1188.0	1262.3	1269.2	1284.5	1340.5										
18	1250.1	1230.1	1348.4	1300.1	1225.9	1222.8	1188.8	1188.3	1187.8	1187.2	1186.5	1186.3	1186.2	1186.0	1185.9	
	1185.7	1185.5	1185.4	1185.4	1185.3	1185.2	1185.0	1184.9	1184.8	1184.9	1185.2	1185.4	1185.7	1186.4	1187.8	
	1187.9	1188.0	1274.1	1278.0	1287.4	1349.1										
19	1250.1	1230.1	1347.6	1301.3	1214.3	1224.7	1188.8	1188.4	1187.9	1187.6	1186.6	1186.4	1186.3	1186.1	1185.9	
	1185.7	1185.5	1185.4	1185.4	1185.4	1185.4	1185.3	1185.3	1185.3	1185.3	1185.6	1185.7	1185.9	1186.6	1187.8	
	1187.9	1208.5	1255.8	1273.5	1281.8	1359.5									1107.10	
20	1243.9	1230.1	1347.1	1302.1	1208.6	1228.5	1228.3	1188.6	1188.0	1187.4	1186.7	1186.5	1186.4	1188 2	1185 9	
	1185.6	1185.2	1185.4	1185.5	1185.8	1185.6	1185.8	1185 8	1185 8	1185 7	1185 8	1185 0	1198 1	1198 9	1197 0	
	1187.9	1210.3	1287.9	1268.1	1281.4	1368.9	1100.0	1100.0	1100.0	1100.7	1100.0	1100.0	1100.1	1100.0	1107.8	
21	1242 3	1230 1	1348 9	1302 5	1224 2	1230 1	1189 9	1188 0	1188 2	1197 4	1198 9	1198 7	1198 E	1198 2	1198 0	
~ *	1195 5	1184 5	1185 3	1185 8	1185 7	1185 8	1185 8	1185 9	1185 9	1198 0	1198 1	1100.7	1198 4	1100.3	1100.0	
	1197 9	1207 5	1284 5	1288 8	1277 9	1300.1	1100.0	1100.0	1100.0	1100.0	1100.1	1100.2	1100.4	1107.2	1107.9	
22	1244 1	1230 1	1207.0	1223 1	1222 0	1230 1	1190.0	1189 2	1188 5	1197 7	1197 0	1198 0	1198 7	1198 E	1198 2	
	1198 0	1195 A	1195 9	1195 0	1198 0	1188 1	1198 1	1198 1	1198 2	1198 2	1107.0	1100.8	1100.7	1100.0	1100.3	
	1197 9	1220 4	1287 4	1270 1	1202.8	1300.1	1100.1	1100.1	1100.2	1100.2	1100.3	1100.0	1100.7	1107.0	1107.9	
22	1228 8	1220.4	12207.4	1270.1	1220 1	1000.1	1100 2	1190 0	1100 2	1100 0	1107 4	1107 0	1107 0	1198 0	1100 7	
23	1198 5	1198 3	1198 3	1198 2	1198 4	1198 A	1190.3	1198 5	1108.5 1108 E	1100.2	1107.4	1107.2	1107.0	1100.9	1100.7	
	1100.0	1200.3	1278 0	1289 4	1259 0	1200.4	1100.4	1100.0	1100.0	1100.0	1100.7	1100.9	110/.1	1107.0	1101.9	
04	107.0	1220.0	1270.0	1200.4	1220 1	1000.1	1100 7	1100.9	1101 7	1100 0	1107 0	1107 7	1107 E	1107 2	1107 1	
27	1230.7	1198 0	1100 0	1104 0	1108 7	1108 7	1190.7	1100.0	1191.7	1109.0	1107.3	110/./	1107.0	1107.3	1107.1	
	1107.0	1210 5	1254 4	1200.0	1250 8	1200.1	1100.0	1100.0	1100.9	1107.0	110/.1	1187.3	110/.0	1101.9	1191.9	
05	1020 1	1218.0	1020 1	1227 1	1000.0	1000.1	1100.0	1101 0	1101 0	1100 0	1100 4	1100 0	1107 0	1107 7	1107 0	
20	1107 4	1107 2	1107 0	1107 0	1107 1	1107 1	1107 1	1181.2	1191.0	1109.0	1100.4	1100.2	1107.9	1107.7	1107.0	
	1107.4	1107.3	1107.2	1107.2	1245 1	1200 1	110/.1	110/.2	1107.2	1167.3	1187.5	1187.7	1187.8	1191.9	1181.8	
00	1020.1	1227.0	12/0./	1270.0	1000 7	1350.1	1100 E	1100.0	1101 1	1100.0	1100 1	1100 7	1100 5	1100 0	1100 0	
20	1230.1	1230.1	1230.1	1230.1	1222.7 1107 F	1214.7	1190.5	1190.8	1191.1	1190.8	1189.1	1188.7	1188.5	1188.2	1188.0	
	1107.9	1107.0	110/./	1107.0	110/.0	1200 1	1107.5	110/.5	1191.0	1187.0	1187.7	118/./	1187.8	1187.8	1187.8	
~7	1192.0	1237.7	12/4.3	1290.1	13/0./	1390.1	1100 0	1100 0								
27	1240.7	1230.1	1230.1	1230.1	1220.0	1194.7	1189.0	1189.8	1189.8	1189.8	1189.3	1188.9	1188.8	1188.4	1188.2	
	1100.1	1107.9	110/.9	110/.0	118/./	118/./	110/./	1187.7	1187.7	1187.7	1187.7	118/./	1187.7	1187.7	1187.9	
	1217.4	1247.9	1280.3	1290.1	1390.1	1390.1										
28	1240.0	1230.1	1230.1	1222.3	1210.2	1189.2	1189.3	1189.3	1189.2	1189.1	1189.0	1188.8	1188.8	1188.4	1188.2	
	1188.1	1188.0	1187.9	1187.8	1187.8	118/./	1187.7	1187.7	1187.7	1187.8	1187.8	1187.8	1187.8	1187.8	1187.7	
~~	1229.7	1275.6	1290.1	1290.1	1390.1	1390.1	1100 0									
29	1260.1	1214.3	1230.1	1219.1	1223.4	1189.0	1189.0	1188.9	1188.8	1188.6	1188.5	1188.4	1188.3	1188.2	1188.1	
	1188.0	1187.9	1187.9	1187.8	1187.8	118/./	1187.7	1187.6	1187.6	1187.5	1187.5	1187.5	1187.4	1187.4	1197.9	
~~	1238.8	1282.8	1290.1	1290.1	1348.4	1390.1										
30	1250.1	1208.2	1230.1	1215.9	1211.3	1188.9	1188.7	1188.8	1188.5	1188.3	1188.2	1188.2	1188.1	1188.0	1188.0	
	1187.9	1187.8	1187.8	1187.7	1187.7	1187.8	1187.5	1187.5	1187.4	1187.4	1187.3	1187.3	1187.3	1187.3	1187.3	
~ ~	1232.1	12/7.0	1275.1	1290.1	1368.7	1390.1										
31	1250.1	1207.5	1225.3	1230.1	1221.5	1188.8	1188.5	1188.4	1188.2	1188.1	1188.0	1188.0	1187.9	1187.9	1187.8	
	1187.8	1187.7	1187.8	1187.8	1187.5	1187.4	1187.3	1187.2	1187.2	1187.1	1187.1	1187.1	1187.0	1187.1	1187.2	
	1241.8	1259.9	1273.0	1290.1	1349.5	1390.1										
32	1260.1	1200.1	1223.3	1230.1	1228.6	1188.7	1188.3	1188.1	1188.0	1187.9	1187.8	1187.8	1187.8	1187.7	1187.7	
	1187.6	1187.5	1187.4	1187.3	1187.2	1187.0	1186.9	1186.9	1186.8	1186.8	1186.7	1186.7	1186.7	1186.8	1186.9	
	1221.1	1238.7	1282.1	1290.1	1290.1	1390.1										
33	1250.1	1200.1	1212.8	1230.1	1230.1	1188.5	1188.2	1188.0	1187.9	1187.8	1187.7	1187.7	1187.8	1187.5	1187.5	
	1187.3	1187.2	1187.1	1186.9	1186.7	1186.6	1186.4	1186.3	1186.3	1186.3	1186.3	1188.4	1188.4	1186.4	1186.5	
	1200.1	1213.4	1281.8	1290.1	1290.1	1390.1										
34	1250.1	1200.1	1203.9	1223.0	1230.1	1188.4	1188.1	1187.9	1187.8	1187.7	1187.6	1187.5	1187.5	1187.4	1187.3	
	1187.1	1187.0	1186.8	1186.6	1186.4	1186.2	1185.9	1185.4	1185.7	1185.9	1186.0	1186.1	1186.1	1186.2	1186.3	
	1200.1	1220.4	1267.5	1290.1	1290.1	1390.1										
35	1250.1	1200.1	1203.5	1226.1	1222.1	1188.3	1188.0	1187.9	1187.8	1187.6	1187.5	1187.4	1187.3	1187.2	1187.1	
	1186.9	1186.7	1186.5	1186.4	1186.2	1186.0	1185.9	1185.8	1185.8	1185.8	1185.9	1185.9	1186.0	1186.0	1186.2	
	1204.3	1240.9	1279.4	1290.1	1290.1	1365.0										

يهريد زيبي تشد شبير بثقة للبينة زلمب عمل ألته ملاج أألته إيمع عمل خا

.

•

38	1250.1	1200.1	1194.0	1213.0	1216.9	1188.3	1188.0	1187.9	1187.8	1187.6	1187.4	1187.3	1187.2	1187.0	1186.9
	1188.7	1186.5	1186.3	1186.1	1186.0	1185.8	1185.8	1185.7	1185.7	1185.7	1185.8	1185.8	1185.9	1185.9	1188.1
	1203.0	1240.1	1281.2	1265.8	1290.1	1374.4									
37	1250.1	1200.1	1190.4	1204.4	1184.2	1188.2	1188.0	1187.9	1187.8	1187.5	1187.3	1187.2	1187.1	1186.9	1188.8
	1186.5	1186.3	1188.1	1185.9	1185.7	1185.6	1185.6	1185.6	1185.8	1185.6	1185.7	1185.7	1185.8	1185.9	1186.0
	1208.5	1247.4	1279.8	1268.2	1290.1	1368.5									
38	1250.1	1204.1	1190.4	1193.3	1188.7	1188.3	1188.0	1187.9	1187.7	1187.5	1187.3	1187.2	1187.1	1186.9	1188.7
	1186.4	1186.1	1185.8	1185.5	1185.3	1185.3	1185.3	1185.4	1185.5	1185.6	1185.6	1185.7	1185.7	1185.9	1188 0
	1201.3	1242.7	1274.5	1253.6	1290.1	1367.8		•							1100.0
39	1248.0	1204.3	1190.3	1189.4	1188.7	1188.3	1188.0	1187.9	1187.7	1187.5	1187.3	1187 2	1187 0	1188 0	1198 8
	1186.4	1186.0	1185.7	1185.2	1184.8	1184.9	1185.2	1185.3	1185.4	1185 5	1185 8	1185 7	1195 7	1195 0	1100.0
	1201.8	1239.1	1268.8	1275.8	1290.1	1359.8		1100.0	1100.4	1100.0	1100.0	1100.7	1100.7	1105.9	1100.0
40	1248.9	1200.1	1190.3	1189 4	1188 7	1199 3	1199 0	1197 0	1107 0	1107 E	1107 2	1107 0	1107 1	1108 0	1100 0
	1186.3	1188.0	1185.5	1184 8	1193 7	1194 A	1195 0	1195 0	1107.0	1107.0	1107.3	110/.2	1107.1	1180.9	1180.8
	1207 7	1244 2	1255 0	1288 5	1200.1	1282 5	1100.0	1100.2	1100.4	1100.0	1105.0	1100.7	1100.7	1100.9	1188.1
<b>4</b> 1	1248 0	1200 1	1100.3	1190 4	1109 7	1100 2	1100 0	1107 0	1107 0	1107 0	1107 5	1107 0	1107 0		
	1108 4	1108 0	1100.3	1105.4	1100.7	1100.3	1100.0	1107.9	1107.0	1107.0	1107.0	1187.3	1187.2	1188.9	1188.7
	1200.4	100.0	100.0	1100.1	1104.0	1104.8	1182.1	1185.3	1185.5	1185.8	1185.8	1185.7	1185.8	1185.9	1186.1
40	1047 0	1227.2	1243.1	1240.8	1290.1	1300.4									
42	1247.8	1200.1	1190.2	1189.3	1188.7	1188.3	1188.1	1187.9	1187.8	1187.7	1187.8	1187.5	1187.3	1187.0	1186.8
	1100.0	1100.2	1100.9	1185.0	1185.4	1185.4	1185.4	1185.5	1185.8	1185.7	1185.8	1185.8	1185.9	1186.0	1188.2
40	1204.4	1221.7	1240.2	1249.8	1290.1	1369.0									
43	1245.7	1200.1	1190.2	1189.3	1188.7	1188.3	1188.1	1187.9	1187.8	1187.8	1187.7	1187.5	1187.4	1187.1	1188.9
	1186.6	1188.4	1188.2	1188.0	1185.9	1185.8	1185.8	1185.8	1185.8	1185.9	1185.9	1186.0	1186.1	1186.2	1188.3
	1208.3	1201.5	1234.9	1242.4	1290.1	1378.7									
44	1243.2	1200.1	1190.1	1189.3	1188.7	1188.3	1188.1	1187.9	1187.9	1187.8	1187.7	1187.5	1187.3	1187.1	1186.9
	1188.8	1186.8	1188.4	1186.3	1186.2	1186.1	1186.1	1186.1	1188.1	1188.1	1188.1	1188.2	1186.3	1186.4	1186.5
	1187.4	1205.0	1232.8	1244.7	1290.1	1335.7									
45	1257.5	1200.1	1190.1	1189.2	1188.7	1188.3	1188.1	1187.9	1187.9	1187.8	1187.7	1187.5	1187.3	1187.1	1186.9
	1186.8	1186.7	1186.6	1186.5	1186.4	1186.4	1186.3	1186.3	1186.3	1186.3	1186.4	1186.4	1188.5	1186.6	1188.7
	1187.2	1203.8	1237.4	1264.1	1285.5	1347.4									
46	1263.5	1200.1	1190.1	1189.2	1188.7	1188.3	1188.1	1187.9	1187.9	1187.8	1187.8	1187.5	1187.2	1187.0	1186.9
	1186.8	1186.7	1186.7	1186.6	1186.6	1186.5	1186.5	1186.5	1186.5	1188.5	1188.5	1188.8	1186.6	1186.7	1186.9
	1187.2	1200.9	1239.5	1277.0	1281.5	1315.3									
47	1268.1	1208.9	1190.0	1189.2	1188.7	1188.3	1188.1	1188.0	1187.9	1187.7	1187.8	1187.4	1187.0	1188.8	1188.7
	1186.7	1188.7	1188.7	1186.7	1186.7	1186.6	1188.8	1186.6	1186.6	1186.7	1186.7	1186.7	1186.8	1186.8	1187.0
	1187.2	1201.1	1237.0	1272.8	1282.2	1284.1									
48	1270.8	1205.9	1190.0	1189.2	1188.6	1188.3	1188.1	1188.0	1187.9	1187.7	1187.5	1187.3	1186.8	1188.4	1188.5
	1186.6	1186.7	1186.7	1186.7	1186.7	1186.7	1186.7	1186.7	1186.7	1186.8	1186.8	1186.8	1186.8	1186.9	1187 0
	1187.3	1201.4	1239.8	1282.1	1282.7	1278.5									
49	1275.1	1205.0	1190.0	1189.1	1188.6	1188.3	1188.1	1188.0	1187.9	1187.7	1187.5	1187.2	1186.6	1185.5	1188 3
	1186.6	1186.7	1186.8	1186.8	1188.8	1188.8	1186.8	1186.8	1186.8	1186.8	1188.9	1186.9	1186.9	1187 0	1197 1
	1187.3	1208.4	1242.1	1279.2	1268.8	1285.7									
50	1277.5	1204.1	1190.0	1189.1	1188.6	1188.3	1188.1	1188.0	1187.9	1187.7	1187.8	1187.3	1188 9	1188 5	1198 8
	1186.7	1186.8	1186.8	1188.9	1186.9	1186.9	1188.9	1188.9	1188.9	1188 9	1188 9	1188 9	1187 0	1187 0	1107 1
	1187.3	1211.4	1242.7	1271.2	1273.6	1285.7			1100.0	1100.0	1100.0	1100.0	1107.0	1107.0	1107.1
Б1	1266.2	1203.1	1190.0	1189 1	1188 8	1188 3	1199 1	1199 0	1197 0	1107 0	1107 8	1107 4	1107 0	1198 0	1100 0
	1188.9	1186 9	1188 9	1188 0	1198 0	1107.0	1107 0	1100.0	1107.0	1107.0	1107.0	1107.4	1107.2	1100.8	1100.9
	1187 4	1204 5	1242 9	1257 1	1279 4	1007.0	1107.0	1167.0	1107.0	1107.0	1107.0	1107.0	1107.0	110/.1	1187.2
52	1278.0	1202 0	1190.0	1190 1	1100 8	1100 2	1100 1	1100 0	1107 0	1107 0	1107 7	1107 0	1107 4	1107 0	
~~	1187 1	1197 1	1197 1	1107 1	1100.0	1100.3	1100.1	1100.0	1107.9	1107.0	1107.7	1107.0	1107.4	1187.2	1187.1
	1197 4	1208 5	1041 7	107.1	100/.1	1107.0	1187.0	1187.0	1187.0	118/.1	118/.1	118/.1	1187.1	1187.2	1187.2
E2	1077 0	1200.0	1100 0	1200.0	1204.7	1243.0									
03	1107 9	1107 0	1190.0	1109.0	1108.0	1188.3	1188.1	1188.0	1187.9	1187.8	1187.8	1187.7	1187.8	1187.4	1187.3
	1107.3	1011 0	10/.2	110/.2	118/.2	118/.1	118/.1	1187.1	1187.1	1187.1	118/.1	1187.2	1187.2	1187.2	1187.3
E 4	1000 1	1211.2	1243.2	1204.0	1204.8	1234.8									
04	1280.1	1213.8	1190.0	1189.0	1188.6	1188.3	1188.1	1188.0	1187.9	1187.9	1187.8	1187.8	1187.7	1187.6	1187.5
	118/.4	118/.4	1187.3	1187.3	1187.3	1187.2	1187.2	1187.2	1187.2	1187.2	1187.2	1187.2	1187.2	1187.3	1187.3
	1187.4	1203.6	1231.7	1248.0	1242.7	1235.2									
55	1284.8	1231.3	1190.0	1188.9	1188.5	1188.3	1188.1	1188.0	1187.9	1187.9	1187.9	1187.8	1187.8	1187.7	1187.6
	1187.5	1187.5	1187.4	1187.4	1187.3	1187.3	1187.3	1187.3	1187.3	1187.3	1187.2	1187.2	1187.3	1187.3	1187.4
	1187.5	1188.0	1214.3	1238.3	1234.3	1273.6									
56	1290.1	1237.0	1190.1	1188.8	1188.4	1188.2	1188.1	1188.0	1187.9	1187.9	1187.9	1187.8	1187.8	1187.7	1187.6

ſ

	1187.6	1187.5	1187.4	1187.4	1187.4	1187.3	1187.3	1187.3	1187.3	1187.2	1187.2	1187.2	1187.2	1187.3	1187.3
	1187.5	1188.0	1211.1	1240.3	1238.3	1275.7									
57	1290.1	1247.2	1190.4	1188.7	1188.3	1188.1	1188.0	1187.9	1187.9	1187.9	1187.8	1187.8	1187.7	1187.6	1187.6
	1187.5	1187.4	1187.4	1187.3	1187.3	1187.2	1187.2	1187.2	1187.2	1187.1	1187.1	1187.1	1187.1	1187.2	1187.2
	1187.4	1188.0	1205.4	1247.9	1254.1	1279.8								110/12	
58	1275.8	1283.0	1221.7	1188.5	1188.1	1188.0	1187.9	1187.9	1187.9	1187.8	1187.7	1187.6	1187 5	1187 4	1197 3
	1187.2	1187.2	1187.1	1187.0	1187.0	1186.9	1186.9	1186.9	1186.8	1186.8	1186 8	1188 8	1188 9	1198 9	1198 0
	1187.1	1189.0	1218.8	1273.9	1324.6	1309.2						1100.0	1100.0	1100.0	1100.8
59	1237.1	1290.1	1248.0	1188.4	1187.8	1187.9	1187.8	1187 8	1187 7	1187 A	1197 4	1197 2	1107 1	1198 0	1100 0
	1186.7	1186.5	1186.4	1186.3	1186.2	1186.2	1186 1	1188 1	1188 0	1188 0	1198 0	1198 0	1107.1	1100.9	1100.0
	1186.5	1204 4	1243 0	1281 8	1371 9	1385 A			1100.0	1100.0	1100.0	1100.0	1100.0	1100.0	1100.1
80	1237 5	1283 0	1287 4	1208 0	1198 0	1197 A	1197 A	1197 4	1197 4	1107 2	1100 0	1100 0	1100 3	1100 0	1105 3
•••	1185 5	1195 3	1195 2	1195 0	1194 0	1194 9	1107.0	110/.4	1107.4	1107.3	1100.9	1100.0	1160.3	1186.0	1185.7
	1104 4	1217 2	1240 1	1200.0	1200 1	1200 1	1104.7	1104.7	1104.0	1104.0	1104.0	1184.5	1184.6	1184.8	1184./
<b>R</b> 1	1224 0	1070 1	1290.1	1322.7	1105 1	1380.1	1107 1	1100 4	1100 1	1105 7	1105 0				
01	1102 7	1102 5	1102 2	1102 1	1100.1	110/.1	110/.1	1100.4	1160.1	1185.7	1185.2	1184.8	1184.5	1184.2	1183.9
	1103.7	1103.0	1103.3	1103.1	1183.0	1182.9	1182.9	1182.8	1182.8	1182.7	1182.7	1182.7	1182.7	1182.9	1183.1
00	1104.2	1223.9	1251.4	1290.1	1347.9	1390.1									
02	1241.2	1241.3	12/1.1	1206.4	1182.6	1186.4	1186.4	1184.9	1184.1	1183.6	1183.1	1182.8	1182.5	1182.3	1182.0
	1181.8	1181.7	1181.5	1181.4	1181.3	1181.2	1181.2	1181.1	1181.1	1181.1	1181.1	1181.1	1181.1	1181.1	1181.5
~~	1186.2	1222.2	1239.3	1278.8	1348.4	1386.1									
63	1208.7	1239.0	1237.2	1206.6	1179.4	1185.4	1185.3	1183.0	1182.1	1181.4	1181.0	1180.8	1180.5	1180.3	1180.1
	1180.0	1179.8	1179.7	1179.6	1179.6	1179.5	1179.5	1179.4	1179.4	1179.4	1179.4	1179.4	1179.4	1179.5	1179.9
	1195.7	1221.1	1238.8	1279.8	1328.2	1363.2									
64	1200.1	1227.7	1217.7	1166.0	1174.7	1182.1	1181.5	1179.8	1179.1	1178.7	1178.4	1178.3	1178.1	1178.0	1177.9
	1177.8	1177.8	1177.7	1177.7	1177.6	1177.8	1177.5	1177.5	1177.5	1177.5	1177.5	1177.4	1177.5	1177.5	1177.6
	1196.7	1214.2	1245.3	1282.0	1271.8	1339.8									
65	1200.1	1215.5	1200.9	1184.0	1167.4	1168.7	1174.1	1175.0	1175.3	1175.4	1175.5	1175.5	1175.5	1175.5	1175.5
	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.5	1175.4	1175.2
	1199.6	1200.1	1236.0	1267.9	1286.5	1280.6									
66	1200.1	1203.9	1180.4	1163.1	1163.1	1165.7	1168.9	1170.5	1171.2	1171.7	1172.0	1172.2	1172.3	1172.5	1172.8
	1172.7	1172.8	1172.9	1173.0	1173.0	1173.1	1173.1	1173.2	1173.2	1173.2	1173.2	1173.2	1173.2	1173.1	1172.9
	1189.8	1200.1	1233.7	1276.3	1265.7	1286.3									
67	1200.1	1180.4	1163.2	1162.4	1161.4	1161.9	1163.4	1165.4	1166.4	1167.1	1167.6	1167.9	1168.2	1168.5	1168.7
	1169.0	1169.2	1169.4	1169.6	1169.7	1169.8	1169.9	1170.0	1170.1	1170.2	1170.2	1170.3	1170.3	1170.4	1170.3
	1173.6	1196.2	1216.3	1236.1	1230.5	1258.1									
68	1200.1	1166.3	1162.9	1162.1	1161.4	1161.4	1162.0	1162.5	1162.9	1163.2	1183.4	1163.6	1163.8	1184 1	1184 4
	1164.8	1165.3	1165.8	1166.0	1166.3	1166.5	1166.7	1166.9	1167.1	1187.2	1187 4	1187 5	1187 7	1187 9	1167 0
	1167.9	1186.1	1200.1	1238.2	1263.4	1290.1					1107.14	1107.0	1107.7	1107.0	1107.8
69	1169.3	1150.1	1162.8	1182 1	1161 6	1181 4	1181 🔺	1181 5	1161 8	1181 0	1182 0	1182 1	1160 1	1160 1	1100 0
••	1162.4	1162.9	1163.3	1163.8	1164.2	1164.5	1184.8	1165.1	1185 3	1185 A	1185 8	1168 0	1168 2	1102.1	1102.2
	1167.0	1169.2	1210 8	1231 8	1279 5	1335 4	1104.0	1100.1	1100.0	1100.0	1100.0	1100.0	1100.2	1100.4	1100.7
HEAD	PRINT FO	RMAT TS	FORMAT N		3 NRAI	NDUMN PP.		AT TS FO		RFR _2					
HEADS	WTIL RE	SAVED O	N LINTT 2			TII RE S		INTT O		DEN -3					
<b>NUTPU</b>	T CONTRO	I TS SPEA	CTETED E	VERY TIM		TEL DE J									
30110		- 10 OFE	CTUTCH E	TENT IIM		<u></u>			TDADY -	1 0000	~~~				
								104 VIITO	UINUFI =	1.000					

			)	ELR WILL BE RE	EAD ON UNIT	7 USING FORMAT	:	(10 <b>f</b> 8.0)	
2100.0	1400.0	1200.0	800.00	600.00	400.00	300.00	200.00	150.00	150.00
100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
100.00	100.00	100.00	100.00	100.00	100.00	150.00	150.00	200.00	300.00
400.00	600.00	800.00	1200.0	1600.0	1800.0				

DELC WILL BE READ ON UNIT 7 USING FORMAT:

(10f8.0)

-----

ر. د د د د	-				t minis e						
		~		ç							
1	800 A	1/	200.0	800 00	800.00	400,00	200,00		150.00	150 00	
10	00.00	10	200.00	100.00	100.00	100.00	100.00	200.00	100.00	100.00	100.0
10	00.00	10	00.00	150.00	150.00	200.00	300.00	200.00	200.00	200.00	200.0
20	00.00	30	00.00	200.00	200.00	200.00	150.00	150.00	100.00	100.00	100.0
10	00.00	18	50.00	150.00	200.00	150.00	150.00	100.00	100.00	100.00	100.0
10	00.00	- 18	50.00 .	150.00	200.00	300.00	300.00	400.00	800.00	600.00	600.0
4(	00.00	30	00.00	300.00	300.00	300.00	400.00	600.00	700.00	800.00	
						PRIMARY	STORAGE COEF	= 0.2500000	FOR LAY	'ER 1	
				HYD. CO	ND. ALONG ROU	S FOR LAYER	1 WILL BE R	READ ON UNIT	27 USING FOR	MAT: (36f4	.0)
	1		2	3	4	5	8	7	8	9	10
	11		12	13	14	15	16	17	18	19	20
	21		22	23	24	25	28	27	28	29	30
	31		32	33	34	35	36				
1	1.0000F-4		1 00005-05	1 00005-05	1 00005-05	1 00005-05	1 00005-05	1 00005 05	1 00005 05	1 00005 05	1 00005 05
4	1.0000F	-05	1.0000E-05	1.0000F-0	5 1.0000F-05	1.0000E-0	5 1.0000E-05		1 00005-05	1 00005-05	1 00005-05
	1.0000E	-05	1.0000E-04	1.0000E-0	3 1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000F-03
	1.0000E	-03	1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-0	3 1.0000E-03				1100002 00
2	1.0000E	-05	1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05
	1.0000E	-05	1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05
	1.0000E	-05	1.0000E-04	1.0000E-0	3 1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
•	1.0000E	-03	1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-0	3 1.0000E-03				
3	1.0000	-05	1.0000E-05	1.0000E-0	5 1.0000E-08		5 1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05
	1.0000E	-05	1.0000E-08	1.0000E-0	3 1 0000E-08	1.0000E-0	1.0000E-00	1.0000E-06	1.0000E-05	1.0000E-05	1.0000E-06
	1.0000E	-03	1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-0	3 1.0000E-03	1.0002-03	1.0002-05	1.00002-03	1.00002-03
4	1.0000E	-05	1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-08	5 1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05
	1.0000E	-05	1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-08	5 1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05
	1.0000E-	-05	1.0000E-04	1.0000E-03	3 1.0000E-03	1.0000E-03	3 1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
-	1.0000E-	·03	1.0000E-03	1.0000E-0	3 1.0000E-03	1.0000E-03	3 1.0000E-03		_		
5	1.0000E	-05	1.0000E-05	1.0000E-0	5 1.0000E-05	1.0000E-08	5 3.0000E-05	3.0000E-05	3.0000E-05	3.0000E-05	3.0000E-05
	3.000E	05	3.0000E-05	3.0000E-0	3.0000E-05	3.0000E-08	5 3.0000E-05	3.0000E-05	3.0000E-05	3.0000E-05	3.0000E-05
	1 0000E	.03	1.0000E-04	1.0000E=03	1.0000E-03	1.0000E-03	1.0000E-03	1.000E-03	1.0000E-03	1.0000E-03	1.0000E-03
8	1.0000E	-05	1.0000E-05	1.0000E-08	5 1.0000E-05	3.0000E-05	5 1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1 0000E-04
-	1.0000E-	-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04	1.0000E-04
	1.0000E-	-04	1.0000E-03	1.0000E-03	3 1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
_	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	3 1.0000E-03				
7	1.0000E-	-05	1.0000E-05	1.0000E-08	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04
	6.0000E-	04	6.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04	5.0000E-04
		04	1.0000E-03	1.000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
R	1,000F-	05	1.00005-05	1.00005-00	3.000E-03	1 00005-04		1 00005-03	1 00005-03	1 00005-03	1 00005 00
•	1.0000F-	03	1.0000E-03	1.0000E-02	1.0000E-08	1.00005-03	1.0000E-04	1.0000E-03	1.0000F-03	1.0000E-03	1 00005-03
	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1100002 00	1.111002 00		
9	1.0000E-	05	1.0000E-05	1.0000E-08	3.0000E-05	1.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-	03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03			–	
10	1.0000E-	05	1.0000E-05	1.0000E-0E	3.0000E-05	1.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.000E-	03	5.000E-03	5 0000E-03	5.0000E-03	5.000E-03	5.0000E-03	ь.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
		03	1 0000E-03	1 0000E-03	1 0000F-03	1 00005-03	1 0000E-03	0.000E-03	5.000E-03	1.0000E-03	1.0000E-03
11	1.0000F-	05	1.0000E-05	1.0000E-08	3.0000E-05	1.0000E-04	5.0000E-03	1.0000F-03	1 00005-02	1 00005-03	1 00005-02
	5.0000E-	03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000F-03	5.0000F-03	5.0000E-03
								U3			

:

	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03			_	
27	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
00	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
28	1.0000E-08	1.0000E-08	1.0000E-08	3.0000E-06	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.000E-03	5.000E-03	5.000E-03	5.0000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	1 0000E-03	<b>B.0000E-03</b>	1 0000E-03	1.0000E-03	5.000E-03	5.0000E-03	5.000E-03	5.0000E-03	1.0000E-03	1.0000E-03
20	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-05	1.0000E-03	1.0000E-03				
29	1.000E-08	5 0000E-03	E 0000E-08	5.000E-08	E 0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	<b>5.0000E-03</b>	5.000E-03	6.0000E-03	1.0000E-03	1.0000E-03
30	1.0000E-05	1.000E-05	1.0000E-05	3 0000E-05	1.0000E-03	E 0000E-04	E 0000E-04	1 00005 00	1 00005 00	1 00005 00
50	5 0000E-03	5 0000E-03	5 0000E-03	5.0000E-03	5 0000E-04	5.0000E-04	5.0000E-04	I.0000E-03	1.0000E-03	1.0000E-03
	5 0000E-03	5.0000E-03	5 0000E-03	5 0000E-03	5.0000E-03	5.000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	0.0002-03	5.000E-03	1.0002-03	1.0000E-03
31	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1 0000E-04	5 0000E-04	5 00005-04	1 0000E-02	1 00005.02	1 00005 02
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-04	5 0000E-03	E 0000E-03	E 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E=03	5.0000E-03	1 0000E-03	1 0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	0.00002 00	0.000E-00	1.0002-05	1.00002-03
32	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1 0000E-03	1 0000E-03	1 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
33	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
34	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
35	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	6.000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
20	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
30	1.0000E-08	1.0000E-08	1.0000E-08	3.0000E-06	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.000E-03	5.000E-03	5.000E-03	5.000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	1 0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	5.000E-03	5.000E-03	5.000E-03	5.0000E-03	1.0000E-03	1.0000E-03
37	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 00005 02	1 00005 03	1 00005 00	1 00005 00
57	5 0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5.0000E-03	E 0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03	5.0000E-03	5.000E-03	5.000E-03	1.0000E-03	5.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	0.0002-00	5.000E-03	1.0002-03	1.0002-03
38	1.0000E-03	1.0000E-03	1.0000F-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03	5 0000E-03	5 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1 0000E-03	1 0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	0.00002 00	0.00002 00	1.00002-00	1.00002-03
39	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000F-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
40	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
41	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				

nge para sing nge nge sing para sali nan sing sing sang sang sang sing sang s

	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
12	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
13	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
14	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
15	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000F-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1 0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				1.00002-00
16	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000F-03	5.0000E-03	5 0000E-03	5 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1 0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	0.00002 00	0.00002 00	1.00002-00	1.00002-03
17	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1 0000E-03	1 0000E-03	1 00005-02
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03	5 0000E-03	E 0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	1 0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	0.0002-00	0.0002-03	1.0002-03	1.0002-03
18	1.0000F-05	1.0000E-05	1 0000E=05	3 0000E-05	1 0000E-04	5 0000E-04	5 0000E-04	1 00005-03	1 00005-02	1 00005 02
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5 0000E-03	E 0000E-03				
	5.0000E-03	5.0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5 0000E-03	5.0000E-03	1 0000E-03	1 0000E-03
	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E=03	0.0002-03	5.000E-03	1.0002-03	1.0002-03
19	1.0000E-05	1 0000E-05	1.0000E-05	3 0000E-05	1.0000E-04	5 0000E-04	5 0000E-04	1 00005-02	1 00005-02	1 00005 02
	5.0000E-03	5 0000E-03	5 0000E-03	5.0000E-00	E 0000E-03	5.0000E-04	5.0000E-04	E 0000E-03	E 0000E 03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.000E-03	5.000E-03	5.000E-03	5.000E-03	1 0000E-03	5.000E-03
	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	0.000E-03	8.000E-03	1.0000E-03	1.00002-03
20	1.0000E-05	1 0000E-05	1 0000E-05	2.0000E-05	1.0000E-04	E 0000E-04	5 0000E-04	1 00005-02	1 00005 02	1 00005 00
	5 0000E-03	5 0000E-03	E 0000E-03	5.000E-08	E 0000E-04	5.000E-04	5.000E-04	1.000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5 0000E-03	5.000E-03	5.0000E-03	5.000E-03	5.000E-03	5.000E-03	5.000E-03	1 0000E-03	5.000E-03
	1 0000E-03	1 0000E-03	1 0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	5.000E-03	8.000E-03	1.00002-03	1.0000E-03
21	1 0000E-05	1 0000E-05	1.0000E-05	2.0000E-05	1.0000E-04	E 0000E-04	E 0000E-04	1 00005 02	1 00005 00	1 00005 00
••	5 0000E-03	5 0000E-03	5.0000E-08	5.000E-08	E 0000E-04	5.000E-04	5.000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.000E-03		5.0000E-03	5.000E-03	5.000E-03	5.000E-03	B.0000E-03	5.0000E-03
	1 0000E-03	1 0000E-03	1 00005-03	1.0000E-03	1.0000E-03	1.0000E-03	0.000E-03	0.000E-03	1.00002-03	1.000E-03
22	1 0000E-05	1 0000E-05	1.0000E-05	2 00005 05	1.0000E-03	1.0000E-03	5 00005 04	1 00005 02	1 00005 00	1 00005 00
	5 0000E-03	E 0000E-03	E 0000E-08	5.0000000000000000000000000000000000000	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.000E-03	1.0000E-03
	5 0000E-03	5.0000E-03	5.000E-03	5.000E-03	5.000E-03	5.000E-03	5.0000E-03	5.0000E-03	8.000E-03	5.000E-03
	1 0000E-03	1 0000E-03	<b>B.0000E-03</b>	5.000E-03	5.000E-03	5.0000E-03	5.000E-03	5.0000E-03	1.0000E-03	1.0000E-03
22	1.0000E-05	1.0000E-05	1.00002-05	1.00002-03	1.00002-03	1.0000E-03				
23	F 0000E-08	1.0000E-08	1.0000E-06	3.000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.000E-03	5.0000E=03	5.000E-03	5.000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	6.0000E-03
	1 0000E-03	5.0000E-03	<b>B.0000E-03</b>	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
~ 4	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
24	1.0000E-06	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	6.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
<b>.</b>	1.000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
26	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	ь.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
26	1.0000E-05	1.0000E-05	1.0000E-05	3.0000E-05	1.0000E-04	5.0000E-04	5.0000E-04	1.0000E-03	1.0000E-03	1.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03
	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	5.0000E-03	1.0000E-03	1.0000E-03

and the state with the state with the state th

.

42	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
43	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
<b>A A</b>	1.0000E-03	1.0000E-03	1.000E-03	1.000E-03	1.0000E-03	1.0000E-03	1 00005 00	1 00005 00	1 00005 00	
	1 0000E-03	1.0000E=03	1.0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1.000E-03	1.0000E-03	1.0000E-03	1.00002-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0002-03	1.0002-03	1.0002-03	1.00002-03
45	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E=03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-02
	1.0000E-03	1 0000E-03	1.0000E-03	1.0000E-03						
	1.0000E-03	1.0000E=03	1.0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1100002 00	1.00002.00	1.000L-03
48	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				-
47	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03			_	
48	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
49	1.0000E=03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 00005 02	1 00005 02	1 00005 00	1 00005 00
40	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E=03	1.0000E-03	1.0000E-03	1.0000E=03	1.0000E-03	1.0000E-03	1.000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0002-03	1.0002-03	1.0002-03	1.0002-03
50	1.0000E-03	1 0000E-03	1 0000E-03							
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
51	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
62	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
52	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 00005 00	1 00005 00		
00	1.0000E-03									
	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03						
	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1.0000E-03	1.0002-03	1.0002-03	1.0002-03	1.00002-03
Б4	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-02
	1.0000E-03	1 0000E-03	1.0000E-03							
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1100002 00		1.00002-00
55	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
56	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
67	1.0000E-03									

1	1265.0	1290.0	1290.0	1290.0	1251.3	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1218.8	1221.7
	1223.1	1222.2	1223.9	1222.6	1215.8	1208.3	1170.0	11/0.0	11/0.0	1170.0	1170.0	1170.0	1170.0	1185.5	1189.2
-	1146.3	1184.5	1158.7	1221.8	1288.6	1290.0									
2	1230.0	1290.0	1290.0	1290.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0
	1230.0	1230.0	1230.0	1230.0	1200.0	1170.0	1150.0	1150.0	1150.0	1150.0	1150.0	1150.0	1150.0	1138.6	1129.8
_	1100.0	1100.0	1124.1	1217.7	1288.0	1390.0									
3	1238.8	1230.0	1252.9	1220.0	1220.0	1220.0	1220.0	1220.0	1220.0	1220.0	1220.0	1220.0	1220.0	1230.0	1230.0
	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1200.0	1200.0	1175.0	1150.0	1125.0	1100.0	1100.0
	1100.0	1100.0	1116.9	1166.3	1251.0	1290.0									
4	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1215.0	1215.0	1220.0	1225.0	1220.0	1220.0	1220.0	1230.0	1230.0
	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1230.0	1180.0	1180.0	1180.0	1180.0	1145.9	1121.1
	1108.3	1100.0	1100.0	1128.5	1200.0	1279.5									
5	1200.0	1200.0	1200.0	1190.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0
	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0	1175.0	1150.0	1125.0	1090.0	1090.0
	1090.0	1090.0	1108.0	1177.8	1228.1	1252.8									
6	1200.0	1200.0	1200.0	1190.0	1180.0	1160.0	1160.0	1175.0	1175.0	1180.0	1180.0	1180.0	1180.0	1180.0	1180.0
	1180.0	1180.0	1180.0	1175.0	1175.0	1175.0	1184.9	1154.0	1150.0	1135.0	1135.0	1125.0	1100.0	1085.0	1075.0
	1080.0	1060.0	1140.0	1202.2	1239.1	1230.5									
7	1200.0	1200.0	1200.0	1200.0	1190.0	1145.0	1135.0	1135.0	1135.0	1140.0	1150.0	1150 0	1150 0	1150 0	1150 0
•	1150.0	1150.0	1150.0	1140.0	1140.0	1135.0	1125.0	1125.0	1115.0	1115.0	1110.0	1100.0	1085 0	1075 0	1082 0
	1050.0	1080.0	1140.0	1229.9	1248.2	1234.0						1100.0	1000.0	10.0.0	1002.0
8	1200.0	1202.2	1200.0	1200.0	1200.0	1140.0	1130.0	1125.0	1120 0	1120 8	1120 0	1120 0	1120 0	1115 0	1115 0
•	1115 0	1115 0	1115 0	1115 0	1110.0	1110 0	1110 0	1100.0	1100.0	1095 0	1095 0	1095 0	1075 0	1082 0	1050.0
	1048 0	1080 0	1175 0	1220 8	1241 1	1240 8	1110.0	1100.0	1100.0	1030.0	1030.0	1000.0	10/0.0	1002.0	1000.0
٥	1200 0	1203 B	1200 0	1200.0	1200 0	1140 0	1130 0	1120 0	1115 0	1115 1	1110 0	1110 0	1110 0	1100.0	1100.0
•	1100.0	1100.0	1100.0	1100.0	1100.0	1095 0	1095 0	1095 0	1090 0	1085 0	1090 0	1070 0	1059 0	1050.0	1047 0
	1047 0	1090.0	1180 0	1244 4	1242 9	1249 0	1000.0	1000.0	1030.0	1000.0	1000.0	10/0.0	1000.0	1000.0	1047.0
10	1200.0	1200.0	1200.0	1200 0	1200.0	1150 0	1135 0	1110.0	1105 0	1100.0	1100.0	1100.0	1005 0	1005 0	1005 0
10	1095 0	1095 0	1090.0	1090.0	1090.0	1090.0	1090.0	1090 0	1075 0	1075 0	1070.0	1060.0	1050.0	1047 0	1055.0
	1047 0	1095 0	1100.0	1258 7	1247 B	1285 8	1000.0	1030.0	10/0.0	10/0.0	10/0.0	1000.0	1080.0	1047.0	1040.0
11	1200.0	1200.0	1200.0	1200.0	1200 0	1150 0	1135 0	1125 0	1115 0	1110.0	1105 0	1100.0	1005 0	1005 0	1005 0
	1005 0	1000.0	1095 0	1095 0	1095 0	1095 0	1095 0	1020.0	1070.0	1085 0	100.0	1050.0	1098.0	1098.0	1095.0
	1055.0	1100.0	1000.0	1055.0	1005.0	1000.0	1000.0	1000.0	10/0.0	1009.0	1060.0	1080.0	1048.0	1047.0	1048.0
10	1200 0	1200.0	1200.0	1202.0	1240.2	1166 0	1140.0	1120 0	1100 0	1115 0	1110.0	1100.0	100E 0	1005 0	1005 0
12	1000.0	1200.0	1200.0	1000.0	1200.0	1000.0	1090.0	1085 0	1000.0	1055.0	1050.0	100.0	1096.0	1045.0	1098.0
	1090.0	1110.0	1090.0	1260.0	1060.0	1080.0	1080.0	1005.0	1000.0	1088.0	1062.0	1048.0	1047.0	1045.0	1043.0
12	1000 0	1200.0	1200.0	1200.0	1200.0	1185 0	1150 0	1140.0	1120 0	1105 0	1100 0	1110 0	1100.0	1005 0	1005 0
13	1200.0	1200.0	1200.0	1200.0	1200.0	1085.0	1000.0	1000 0	1057.0	1120.0	1120.0	1110.0	1100.0	1095.0	1095.0
	1098.0	1090.0	1090.0	1080.0	1008.0	1005.0	1002.0	1060.0	1057.0	1066.0	1051.0	1048.0	1046.0	1043.0	1040.0
14	1040.0	1120.0	1230.0	1200.4	1247.0	1175 0	1105 0	1145 0	1125 0		1105 0		1105 0	1100 0	1005 0
14	1200.0	1200.0	1200.0	1200.0	1200.0	1002 0	100.0	1145.0	1136.0	1130.7	1125.0	1115.0	1105.0	1100.0	1095.0
	1098.0	1095.0	1090.0	1070.0	1065.0	1003.0	1001.0	1060.0	1066.0	1063.0	1060.0	1048.0	1046.0	1040.0	1040.0
16	1040.0	1180.0	1230.0	12/1.0	1209.4	1201.4	1175 0	1155 0	1145 0						
19	1242.0	1230.0	1201.0	1207.2	1212.1	1190.0	11/6.0	1166.0	1145.0	1135.4	1125.0	1115.0	1110.0	1100.0	1095.0
	1098.0	1098.0	1088.0	10/8.0	10/3.0	1070.0	1005.0	1000.0	1022.0	1051.0	1049.0	1047.0	1045.0	1040.0	1040.0
10	1047.0	1160.0	1230.0	1207.0	1200.4	1277.5	1100 0	1105 0							
10	1247.0	1230.0	1206.3	1205.2	1200.0	1200.0	1180.0	1165.0	1160.0	1136.2	1130.0	1125.0	1115.0	1110.0	1100.0
	1095.0	1095.0	1085.0	1075.0	10/3.0	1070.0	1080.0	1058.0	1052.0	1050.0	1048.0	1048.0	1044.0	1040.0	1040.0
	1049.0	1230.0	1258.9	1260.2	12/3.9	1330.8									
17	1245.8	1230.0	1209.1	1204.9	1208.3	1210.0	1190.0	1175.0	1150.0	1135.4	1130.0	1120.0	1115.0	1110.0	1100.0
	1095.0	1095.0	1085.0	10/5.0	1071.0	1065.0	1080.0	1055.0	1053.0	1050.0	1048.0	1045.0	1040.0	1040.0	1042.0
	1055.0	1220.0	1262.2	1289.1	1284.4	1340.4									
18	1250.0	1230.0	1207.5	1203.6	1225.8	1220.0	1200.0	1180.0	1165.0	1140.7	1135.0	1130.0	1120.0	1110.0	1105.0
	1095.0	1095.0	1090.0	1075.0	1072.0	1068.0	1082.0	1055.0	1052.0	1049.0	1047.0	1043.0	1040.0	1040.0	1044.0
	1060.0	1220.0	1274.0	1277.9	1287.3	1349.0									
19	1250.0	1230.0	1211.3	1202.4	1214.2	1230.0	1200.0	1180.0	1160.0	1140.0	1135.0	1130.0	1120.0	1115.0	1105.0
	1095.0	1095.0	1090.0	1075.0	1072.0	1065.0	1080.0	1055.0	1052.0	1049.0	1047.0	1043.0	1040.0	1040.0	1047.0
	1090.0	1230.0	1255.7	1273.4	1281.5	1359.4									
20	1243.8	1230.0	1215.0	1207.3	1208.5	1230. <b>0</b>	1230.0	1180.0	1160.0	1140.2	1135.0	1125.0	1120.0	1110.0	1100.0
	1095.0	1095.0	1090.0	1075.0	1071.0	1067.0	1060.0	1055.0	1051.0	1048.0	1044.0	1040.0	1040.0	1043.0	1047.0
	1100.0	1230.0	1267.8	1268.0	1281.3	1368.8									
21	1242.2	1230.0	1218.8	1215.8	1224.1	1230.0	1220.0	1180.0	1150.0	1140.5	1130.0	1125.0	1115.0	1105.0	1100.0

ande gener ander ander dens verde ander dens ander ander ander ander ander

	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1,0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
58	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
59	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
60	1.0000E-03									
	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03				
61	1.0000E-03									
	1.0000E-03									
	1.0000E-03	1 0000E-03								
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03			1.00002-00	1.000E-00
62	1.0000E-03									
	1.0000E-03	1 0000E-03	1 0000E-03							
	1.0000E-03	1 0000E=03								
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1.00002 00		1.000L-00
63	1.0000E-03	1 0000E-03								
	1.0000E-03	1 0000E-03								
	1.0000E-03	1 0000E-03	1 0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1.00002 00	1.00002-00	1.0002-03
64	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000F-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 00005-03
	1.0000E-03	1.0000E-03	1.0000F-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1.0000E-03
	1.0000E-03	1 0000E-03	1 0000E-03	1.0000E-03						
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1.00002 00	1.00005-00	1.00002-03
65	1.0000E-03	1 0000E-03	1 0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1.0000E-03
	1.0000E-03	1.0000E=03	1.0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.00002.00	1.00005-00	1.0002-03	1.0002-03
66	1.0000E-03	1 0000E-03	1 0000E-03							
	1.0000E-03	1 0000E-03	1.0000E-03							
	1.0000E-03	1 0000E-03	1.0000E-03							
	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03		1.00000	1.00002-00	1.0002-03
67	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03						
	1.0000E-03	1 0000E-03	1.0000E-03	1.0000E-03						
	1.0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03					
	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1.00002-00	1.00002-03	1.0002-03	1.00002-03
68	1.0000E-03	1.0000E-03	1 0000E-03	1 00005-02	1 00005-02					
•••	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1.0000E-03	1.0000E-03	1.0000E-03
	1.0000E-03	1 0000E-03	1 0000E-03	1.0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1.00002-03
	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-02	1 0000E-03		······E-03		1.000E-03
69	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1 00005-02	1 00005-02	1 00005-03	1 00005-03
	1.0000E-03	1 0000E-03	1 0000E-03	1 0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1 0000E-03	1.0000E-03	1 00005 03
	1.0000E-03	1.0000E-03	1 0000E-03	1 0000E-03	1.0000E_02	1 0000E-03	1 0000E-03	1.00005-03	1 00005-03	1.0000E-03
	1 00005-02	1 00005-03	1 00005-03	1 00005-03	1 00005 03	1 00005-03	*	1.00002-03	1.00002-03	1.0002-03
		1.000E-03	T. WWE-03	1.000E-03	1.00005-03	1.0002-03				

. . .

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36			-			BOTTOM	FOR LAYER	1 WII	LL BE READ	ON UNI	T 28 USI	NG FORMAT:	(10	f8.0) 	
16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	. 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
31 32 33 34 35 38	16	17	18	19	20	21	22	23	24	25	28	27	28	29	30
	31	32	33	34	35	36									

	1095.0	1090.0	1085.0	1075.0	1070.0	1065.0	1058.0	1052.0	1050.0	1048.0	1044.0	1040.0	1040.0	1043.0	1048.0
~~	1125.0	1230.0	1284.4	1268.7	1277.8	1390.0									
22	1244.0	1230.0	1222.8	1223.0	1221.9	1230.0	1215.0	1175.0	1150.0	1135.8	1125.0	1120.0	1115.0	1110.0	1100.0
	1150.0	1090.0	1005.0	1073.0	10/0.0	1085.0	1057.0	1052.0	1049.0	1047.0	1044.0	1040.0	1040.0	1044.0	1049.0
23	1238 5	1230.0	1207.3	1270.0	1292.7	1390.0	1000.0	1170 0	1150 0	1125 5	1105 0	1100 0			
20	1095 0	1090.0	1078 0	1070 0	1085 0	1020.0	1200.0	1049.0	1049 0	1130.0	1042 0	1120.0	1115.0	1105.0	1095.0
	1160.0	1230.0	1275.9	1268.3	1357 9	1390.0	1082.0	1049.0	1048.0	1040.0	1043.0	1040.0	1040.0	1048.0	1075.0
24	1238.6	1230.0	1230.0	1230.0	1230.0	1230 0	1180.0	1180 0	1135 0	1125 3	1115 0	1105 0	1100.0	1005 0	1005 0
	1080.0	1075.0	1070.0	1085.0	1060.0	1055.0	1050.0	1048.0	1047.0	1044.0	1040.0	1040 0	1043 0	1048 0	1095.0
	1180.0	1230.0	1254.3	1277.5	1359.5	1390.0		104010	1047.0	1044.0	1040.0	1040.0	1043.0	1040.0	1090.0
25	1230.0	1230.0	1230.0	1230.0	1230.0	1215.0	1170.0	1140.0	1125.0	1110.9	1100.0	1095.0	1095.0	1090.0	1085 0
	1077.0	1072.0	1070.0	1060.0	1055.0	1050.0	1049.0	1047.0	1043.0	1040.0	1040.0	1043.0	1048.0	1055.0	1150 0
	1200.0	1230.0	1278.8	1278.7	1345.0	1390.0								100010	
28	1230.0	1230.0	1230.0	1230.0	1222.8	1215.0	1150.0	1120.0	1105.0	1095.0	1080.0	1075.0	1075.0	1070.0	1070.0
	1065.0	1060.0	1055.0	1050.0	1049.0	1047.0	1045.0	1043.0	1040.0	1040.0	1043.0	1048.0	1080.0	1090.0	1180.0
	1230.0	1237.8	1274.2	1290.0	1375.8	1390.0									
27	1240.8	1230.0	1230.0	1230.0	1225.4	1195.0	1125.0	1100.0	1080.0	1075.0	1070.0	1060.0	1058.0	1054.0	1051.0
	1050.0	1049.0	1048.0	1048.0	1044.0	1042.0	1040.0	1040.0	1043.0	1047.0	1050.0	1060.0	1090.0	1125.0	1185.0
00	1230.0	1247.8	1280.2	1290.0	1390.0	1390.0									
28	1240.0	1230.0	1230.0	1222.2	1218.1	1180.0	1115.0	1085.0	1075.0	1085.2	1053.0	1050.0	1049.0	1048.0	1047.0
	1040.0	1043.0	1041.0	1040.0	1040.0	1040.0	1043.0	1047.0	1050.0	1080.0	1085.0	1080.0	1120.0	1140.0	1190.0
29	1250.0	1210.0	1290.0	1290.0	1390.0	1390.0	1100 0	1000 0	1000 0	1050 5	10/0 0	1017 0			
2.4	1041 0	1040 0	1040 0	1042 0	1045 0	1049 0	1050.0	1050.0	1060.0	1080.8	1048.0	1047.0	1046.0	1048.0	1043.0
	1238.7	1282.7	1290.0	1290 0	1348 3	1390.0	1080.0	1088.0	1008.0	1080.0	1090.0	1115.0	1126.0	1160.0	1200.0
30	1250.0	1208.1	1230.0	1215.8	1211 2	1150 0	1100.0	1075 0	1050 0	1048 3	1048 0	1044 0	1042 0	1040 0	1040 0
	1040.0	1042.0	1045.0	1047.0	1049.0	1051.0	1065.0	1080.0	1085.0	1100.0	1110.0	1125 0	1135 0	1185 0	1200.0
	1232.0	1278.9	1275.0	1290.0	1358.8	1390.0		100010	100010				1100.0	1100.0	1200.0
31	1250.0	1207.4	1225.2	1230.0	1221.4	1160.0	1100.0	1070.0	1049.0	1047.8	1044.0	1041.0	1040.0	1040.0	1040 0
	1042.0	1047.0	1049.0	1050.0	1060.0	1070.0	1080.0	1090.0	1100.0	1110.0	1120.0	1130.0	1140.0	1160.0	1200.0
	1241.7	1259.8	1272.9	1290.0	1349.4	1390.0									
32	1250.0	1200.0	1223.2	1230.0	1228.5	1160.0	1110.0	1070.0	1048.0	1045.4	1042.0	1040.0	1040.0	1042.0	1044.0
	1047.0	1049.0	1060.0	1085.0	1075.0	1080.0	1090.0	1105.0	1110.0	1115.0	1120.0	1130.0	1140.0	1150.0	1170.0
~~	1220.0	1238.6	1262.0	1290.0	1290.0	1390.0									
33	1250.0	1200.0	1212.5	1230.0	1230.0	1150.0	1090.0	1050.0	1045.0	1040.9	1040.0	1040.0	1040.0	1045.0	1050.0
	1060.0	1060.0	1065.0	1075.0	1080.0	1090.0	1100.0	1105.0	1110.0	1115.0	1120.0	1130.0	1140.0	1150.0	1180.0
34	1200.0	1213.3	1201.7	1290.0	1290.0	1390.0	1075 0	1015 0							
04	1080.0	1085 0	1070 0	1020.0	1230.0	1005 0	1075.0	1046.0	1040.0	1040.1	1040.0	1040.0	1045.0	1050.0	1055.0
	1210.0	1230 0	1287 4	1290.0	1290.0	1200.0	1108.0	1110.0	1119.0	1120.0	1125.0	1135.0	1145.0	1180.0	1200.0
35	1250.0	1200.0	1203.4	1228.0	1222.0	1125 0	1080 0	1045 0	1040 0	1040 5	1040 0	1040 0	1045 0	1050 0	1055 0
	1065.0	1070.0	1075.0	1080.0	1090.0	1095.0	1105 0	1110 0	1115 0	1125 0	1125 0	1140.0	1150 0	1180.0	1066.0
	1225.0	1240.8	1279.3	1290.0	1290.0	1364.9				1120.0	1120.0	1140.0	1100.0	1100.0	1210.0
38	1250.0	1200.0	1185.4	1212.9	1216.8	1110.0	1050.0	1045.0	1040.0	1040.5	1040.0	1040.0	1045.0	1055.0	1055 0
	1060.0	1070.0	1075.0	1080.0	1090.0	1095.0	1105.0	1110.0	1115.0	1125.0	1130.0	1150.0	1175.0	1200.0	1210.0
	1220.0	1240.0	1281.1	1285.7	1290.0	1374.3									
37	1250.0	1200.0	1177.8	1204.3	1184.1	1105.0	1060.0	1045.0	1040.0	1040.4	1040.0	1040.0	1040.0	1045.0	1045.0
	1050.0	1080.0	1065.0	1075.0	1075.0	1080.0	1090.0	1095.0	1100.0	1115.0	1120.0	1155.0	1180.0	1202.0	1210.9
	1208.4	1247.3	1279.7	1268.1	1290.0	1366.4									
38	1250.0	1204.0	1171.5	1193.2	1170.2	1100.0	1060.0	1045.0	1040.0	1040.0	1040.0	1040.0	1040.0	1045.0	1045.0
	1050.0	1055.0	1080.0	1070.0	1080.0	1085.0	1085.0	1095.0	1105.0	1110.0	1120.0	1180.0	1180.0	1202.0	1210.0
20	1220.0	1242.6	12/4.4	1253.5	1290.0	1367.5									
38	1240.9	1204.2	1166.2	11//.2	1159.4	1085.0	1055.0	1045.0	1040.0	1040.3	1040.0	1040.0	1040.0	1040.0	1045.0
	1220 0	1000.0	1080.0	1005.0	1075.0	1080.0	1080.0	1082.0	1100.0	1110.0	1120.0	1185.0	1180.0	1201.0	1210.0
40	1248 9	1200 0	1160 0	12/0./	1151 0	1000 0	1055 0	1045 0	1040 0	1040 0	1010 0				
-0	1050 0	1055 0	1080 0	1080 0	1075 0	1080.0	1005.U	1046.U	1040.0	1040.0	1040.0	1040.0	1040.0	1040.0	1045.0
	1215.0	1225.0	1255 8	1288 4	1290 0	1382 4	1000.0	1030.0	1100.0	1110.0	1130.0	1180.0	11/5.0	1200.0	1205.0
41	1248.8	1200.0	1150.0	1157.0	1125 0	1080 0	1050 0	1045 0	1040 0	1040 0	1040 0	1040 0	1040 0	1040 0	1045 0
	1045.0	1055.0	1060.0	1070.0	1075.0	1080.0	1085.0	1090.0	.1100.0	1105.0	1130 0	1155 0	1175 0	1195 0	1205 0
				<b>.</b>				100010				1100.0	1110.0	1130.0	1200.0
								-							

÷ 1

ander band ander samt samt samt mille under samt samt sind sind ander samt samt ander a

·

1

	1210.0	1220.0	1243.0	1240.8	1290.0	1365.3									
42	1247.8	1200.0	1150.0	1130.0	1110.0	1085.0	1055.0	1045.0	1040.0	1040.0	1040.0	1040.0	1040.0	1040.0	1040 0
	1045.0	1050.0	1060.0	1065.0	1075.0	1080.0	1085.0	1095.0	1100.0	1105.0	1115.0	1150.0	1185 0	1185 0	1200.0
	1210.0	1215.0	1220.0	1249.5	1290.0	1368.9							1100.0	1100.0	1200.0
43	1245.6	1200.0	1150.0	1130.8	1111.7	1090.0	1085.0	1045.0	1040.0	1040.0	1040 0	1040 0	1040 0	1040 0	1040.0
	1045.0	1050.0	1060.0	1085.0	1075.0	1080.0	1090.0	1095 0	1100.0	1105 0	1115 0	1140.0	1140.0	1175 0	1040.0
	1205.0	1215.0	1220.0	1242.3	1290.0	1376 B	1000.0	1000.0	1100.0	1100.0	1110.0	1140.0	1100.0	11/5.0	1190.0
44	1243 1	1200 0	1150 0	1134 2	1110 3	1100.0	1075 0	1045 0	1040 0	1040.0	1040 0	1010 0			
••	1045 0	1050.0	1055 0	1085 0	1075 0	1095 0	1000.0	1100.0	1105.0	1040.0	1040.0	1040.0	1040.0	1040.0	1040.0
	1200 0	1000.0	1000.0	1000.0	1078.0	1000.0	1050.0	1100.0	1108.0	1110.0	1120.0	1130.0	1150.0	1165.0	1185.0
46	1200.0	1220.0	1100.0	1244.0	1250.0	1330.0	1000 0								
40	1207.4	1200.0	1160.0	1160.0	1160.0	1125.0	1080.0	1060.0	1045.0	1040.0	1040.0	1040.0	1040.0	1040.0	1040.0
	1040.0	1046.0	1060.0	10/6.0	1080.0	1080.0	1100.0	1105.0	1110.0	1115.0	1120.0	1135.0	1150.0	1165.0	1180.0
	1200.0	1220.0	1237.3	1264.0	1285.4	1347.3									
46	1263.4	1200.0	1150.0	1117.5	1109.5	1100.0	1100.0	1080.0	1050.0	1045.0	1040.0	1040.0	1040.0	1040.0	1040.0
	1040.0	1045.0	1055.0	1070.0	1080.0	1085.0	1095.0	1105.0	1110.0	1115.0	1120.0	1140.0	1150.0	1165.0	1180.0
	1202.0	1222.0	1239.4	1276.9	1281.4	1315.2									
47	1268.0	1206.8	1190.0	1180.0	1170.0	1160.0	1135.0	1090.0	1060.0	1045.0	1040.0	1040.0	1040.0	1040.0	1040.0
	1040.0	1045.0	1060.0	1070.0	1080.0	1085.0	1095.0	1105.0	1110.0	1115.0	1120.0	1125.0	1150.0	1165 0	1180 0
	1200.0	1225.0	1236.9	1272.7	1282.1	1284.0							1100.0	1100.0	1100.0
48	1270.7	1205.8	1190.0	1180.0	1170.0	1160.0	1150.0	1100.0	1075.0	1050.0	1045.0	1040 0	1040 0	1040 0	1040 0
	1040.0	1045.0	1055.0	1085.0	1075.0	1085.0	1095.0	1100.0	1110.0	1115 0	1120 0	1125 0	1120.0	1140.0	1040.0
	1180.0	1215.0	1239.5	1282.0	1282.6	1278.4	1000.0			1110.0	1120.0	1120.0	1130.0	1140.0	1160.0
49	1275.0	1204 9	1190 0	1180 0	1170 0	1180 0	1150 0	1110.0	1090 0	1050 0	1045 0	1040 0	1010 0		
	1040 0	1045 0	1055 0	1070 0	1090 0	1000.0	1095 0	1105.0	1110 0	1115 0	11040.0	1040.0	1040.0	1040.0	1040.0
	1195 0	1220 0	1242 0	1070.0	1080.0	1000.0	1000.0	1105.0	1110.0	1115.0	1120.0	1125.0	1135.0	1140.0	1160.0
50	1977 4	1220.0	1100.0	1190 0	1170.0	1100.0	1100 0	1140.0		1075 0					
00	1040.0	1204.0	1150.0	1070.0	1000.0	1100.0	1160.0	1140.0	1110.0	10/6.0	1060.0	1045.0	1040.0	1040.0	1040.0
	1190.0	1045.0	1055.0	1070.0	1080.0	1090.0	1082.0	1100.0	1110.0	1115.0	1120.0	1125.0	1130.0	1140.0	1150.0
E1	100.0	1218.0	1242.0	12/1.1	12/3.0	1205.0									
91	1200.1	1203.0	1140.0	1185.0	1180.0	1175.0	1160.0	1160.0	1120.0	1090.0	1060.0	1045.0	1040.0	1040.0	1040.0
	1040.0	1045.0	1065.0	1085.0	1075.0	1085.0	1095.0	1100.0	1105.0	1110.0	1115.0	1120.0	1130.0	1135.0	1150.0
50	1180.0	1215.0	1242.8	1257.0	1278.3	1281.8									
62	12/5.9	1201.9	1195.0	1185.0	1180.0	1175.0	1165.0	1155.0	1130.0	1115.0	1075.0	1050.0	1045.0	1040.0	1040.0
	1040.0	1045.0	1055.0	1065.0	1075.0	1085.0	1095.0	1100.0	1105.0	1110.0	1115.0	1120.0	1125.0	1135.0	1145.0
	1180.0	1215.0	1241.6	1257.9	1284.6	1243.5									
53	1277.1	1204.0	1195.0	1185.0	1180.0	1175.0	1170.0	1155.0	1140.0	1120.0	1080.0	1050.0	1045.0	1040.0	1040.0
	1040.0	1045.0	1050.0	1070.0	1075.0	1085.0	1090.0	1095.0	1105.0	1110.0	1115.0	1120.0	1125.0	1135.0	1145.0
	1180.0	1215.0	1243.1	1254.5	1264.7	1234.7									
54	1280.0	1213.7	1195.0	1185.0	1175.0	1170.0	1160.0	1150.0	1125.0	1100.0	1060.0	1045.0	1040.0	1040.0	1040.0
	1040.0	1045.0	1050.0	1060.0	1075.0	1080.0	1085.0	1095.0	1100.0	1110.0	1115.0	1120.0	1125.0	1135.0	1145 0
	1175.0	1215.0	1231.6	1245.9	1242.6	1235.1								1100.0	1140.0
55	1284.7	1231.2	1200.0	1185.0	1165.0	1150.0	1100.0	1050.0	1050.0	1050.0	1050.0	1050 0	1050 0	1050 0	1082 2
	1061.3	1060.2	1055.9	1062.7	1089.4	1078.1	1084.0	1090.1	1100.9	1101.9	1100.6	1102 3	1103 7	1125 4	1150 0
	1150.0	1177.0	1214.2	1238.2	1234.2	1273.5					1100.0	1101.0	1105.7	1120.7	1160.0
56	1290.0	1236.9	1190.0	1170.0	1150.0	1140.0	1080.0	1050.0	1050.0	1050 0	1050 0	1050 0	1050 0	1050 0	1050 0
	1050.0	1050.0	1050.3	1057.0	1083 5	1089 7	1075 8	1081 5	1087 4	1002.2	1100.1	1100.0	1000.0	1080.0	1060.0
	1150.0	1172.9	1211.0	1240 2	1238 2	1275 A	1010.0	1001.0	1007.4	1053.3	1100.1	1100.0	1100.0	1123.0	1130.8
57	1290.0	1247 1	1200.0	1180 0	1150 0	1100.0	1050 0	1050 0	1050 0	1050 0	1050 0	1050 0	1050 0		
••	1050 0	1050 0	1050.0	1051 4	1057 1	1082 0	1080.0	1000.0	1080.0	1080.0	1060.0	1060.0	1050.0	1050.0	1050.0
	1150 0	1172 0	1205.0	1047 0	1057.1	1002.9	1000.0	10/4.3	1001.0	1000.7	1100.0	1100.0	1109.8	1118.2	1131.2
60	1975 7	1202 0	1200.3	1140 0	1204.0	12/9.7	1050 0	1050 0	1050 0						
00	1270.7	1202.9	1221.0	1140.0	1125.0	1050.0	1060.0	1060.0	1060.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0
	1050.0	1060.0	1050.0	1050.0	1064.2	1059.7	1065.8	1072.0	1078.1	1084.2	1100.0	1100.0	1107.9	1119.7	1136.5
	1109.0	1187.3	1218.5	12/3.8	1324.5	1309.1									
23	1237.0	1290.0	1247.9	1162.8	1095.9	1059.7	1061.7	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1061.2	1059.1
	1057.1	1061.0	1059.5	1057.9	1054.0	1061.1	1068.2	1078.6	1082.3	1089.9	1097.5	1106.7	1117.7	1130.3	1147.7
	1172.1	1204.3	1242.9	1281.7	1371.8	1385.5									
60	1237.4	1282.9	1267.3	1207.9	1093.9	1050. <b>0</b>	1059.4	1062.8	1050.0	1050.0	1050.0	1050.0	1083.9	1061.7	1059.4
	1057.2	1054.9	1061.3	1059.5	1058.8	1064.6	1072.8	1080.6	1089.7	1096.3	1103.6	1112.5	1123.5	1136 0	1156 1
	1194.3	1217.1	1249.0	1322.6	1390.0	1390.0		-							
61	1234.8	1270.0	1290.0	1200.2	1116.3	1050. <b>0</b>	1061.8	1082.7	1050.0	1050.0	1050.0	1050.0	1050 0	1050 0	1058 9
	1056.5	1061.3	1062.5	1056.7	1066.7	1066.9	1074.9	1083.0	1091.1	1099.1	1108.8	1118 4	1128 3	1180 3	1184 9
	1182.0	1223.8	1251.3	1290.0	1347.8	1390.0								1100.3	1104.0

nen inni 4000 milli nali (1000 dini 1000 dini 1000 dini 1000 dini 4000 dini 4000 dini 4000 dini 4

:

62	1241.1	1241.2	1271.0	1208.3	1108.2	1050.0	1062.1	1063.8	1050.0	1050.0	1050.0	1050.0	1062.7	1060.5	1058.2
	1058.0	1053.7	1062.8	1052.7	1060.8	1068.8	1078.8	1089.4	1092.9	1100.9	1108.6	1118.2	1129.7	1153.0	1189.5
	1186.1	1222.1	1239.2	1276.5	1348.3	1386.0									
63	1208.8	1238.9	1237.1	1208.5	1080. <b>8</b>	1058.1	1064.3	1050.0	1050.0	1050.0	1050.0	1050.0	1061.7	1059.5	1057.4
	1055.5	1059.8	1057.8	1054.5	1062.5	1070.6	1077.7	1080.2	1094.6	1125.9	1119.0	1124.5	1132.5	1154.1	1171.3
	1195.8	1221.0	1238.7	1279.7	1326.1	1363.1									
64	1200.0	1227.8	1217.8	1164.2	1076.0	1059.6	1085.2	1066.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0
	1050.0	1053.9	1082.3	1055.2	1063.3	1070.5	1077.6	1084.8	1091.9	1128.7	1107.7	1118.8	1130.0	1155.9	1173.1
	1198.6	1214.1	1245.2	1281.9	1271.7	1339.7									
65	1200.0	1215.4	1200.8	1138.4	1074.8	1060.2	1067.8	1050.0	1050.0	1050.0	1050.0	1050.0	1061.3	1059.1	1058.9
	1054.8	1063.0	1060.6	1055.7	1082.7	1069.8	1076.8	1080.0	1092.2	1117.4	1114.2	1117.6	1129.9	1144.4	1166.7
	1199.5	1200.0	1235.9	1287.8	1286.4	1280.5									
66	1200.0	1203.8	1180.3	1079.3	1075.0	1065.1	1072.8	1050.0	1050.0	1050.0	1063.9	1062.0	1061.4	1059.2	1057.1
	1058.3	1057.0	1055.8	1055.3	1062.4	1069.4	1078.5	1083.2	1089.4	1104.4	1102.3	1112.8	1125.4	1147.8	1160.7
	1189.7	1200.0	1233.6	1278.2	1285.8	1286.2									
67	1200.0	1180.3	1150.7	1091.3	1050.0	1065.8	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0
	1050.0	1066.3	1050.0	1050.0	1058.1	1062.7	1069.3	1075.8	1082.4	1088.8	1093.8	1103.2	1114.9	1127.8	1144.4
	1173.5	1196.1	1218.2	1236.0	1230.4	1258.0									
68	1200.0	1166.2	1129.3	1070.7	1082.8	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0
	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1051.1	1056.6	1065.3	1071.9	1078.5	1086.7	1095.5	1116.9	1128.5
	1155.5	1186.0	1200.0	1238.1	1263.3	1290.0									
69	1169.2	1150.0	1118.8	1067.9	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0
	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1050.0	1067.2	1065.7	1058.5	1067.3	1084.1	1101.5
	1124.5	1166.9	1210.5	1231.7	1279.4	1335.3									

.

SOLUTION BY THE STRONGLY IMPLICIT PROCEDURE

MAXIMUM ITERATIONS ALLOWED FOR CLOSURE = 100 ACCELERATION PARAMETER = 1.0000 HEAD CHANGE CRITERION FOR CLOSURE = 0.60000E-01 SIP HEAD CHANGE PRINTOUT INTERVAL = 1 CALCULATE ITERATION PARAMETERS FROM MODEL CALCULATED WSEED

STRESS	PERTOD	NO.	1.	LENGTH =	2629800
OTILEOU	I CUTOD	110.	÷.,		2020000.

NUMBER OF TIME STEPS = 1

MULTIPLIER FOR DELT = 1.500

INITIAL TIME STEP SIZE = 2629800.

8 WELLS

.

٠

LAYER	ROW	COL	STRESS RATE	WELL NO.
1	40	20	-1.0800	1
1	49	15	0.00000E+00	2
1	21	17	-2.7700	3
1	16	24	-1.8000	4
1	12	15	-1.0400	5
1	12	29	0.00000E+00	6
1	46	15	0.00000E+00	7
1	42	20	0.00000E+00	8

## RECHARGE WILL BE READ ON UNIT 10 USING FORMAT: (36f3.0)

	1	2	3	4	Б	6	7	8	9	10
	11	12	13	14	15	16	17	18	19	20
	21	22	23	24	25	26	27	28	29	30
	31	32	33	34	35	36				•••
• • • •										
1	0.0000E+00									
	0.0000E+00									
	0.0000E+00	2.3850E-07	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08
_	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
2	0.0000E+00									
	0.0000E+00									
	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
_	2.6500E-08	2.8500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
3	0.0000E+00									
	0.0000E+00									
	0.0000E+00	2.3850E-07	2.8500E-08							
	2.8500E-08	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00				
4	2.3850E-07	2.6500E-08	2.8500E-08							
	2.6500E-08									
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
_	2.6500E-08	2.8500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00				
5	2.3850E-07	2.6500E-08								
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
_	2.8500E-08	2.8500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00				
6	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08
	2.6500E-08									
	2.8500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
7	2.3850E-07	2.6500E-08								
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
8	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08

_	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
9	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00				
10	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	<b>-</b> -			
11	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.8500E-08	2.8600E-08	2.8600E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.3860E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
12	2.3860E-07	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6600E-08	2,6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6600E-08	2.8500E-08	2.6500E-08	2.6500E-08
10	2.6500E-08	2.3850E-07	0.000E+00	0.000E+00	0.0000E+00	0.0000E+00				
13	2.300UE-U/	2.0000E-00	2.00002-00	2.00UUE-U8	2.00UE-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.000000000	2.00UUE-00	2.00002-00	2.00002-08	2.0500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.00000000000	2.00002-00	2.0000000000	2.00002-00	2.00005.00	2.000000-00	2.00005-08	2.8500E-08	2.8500E-08	2.8500E-08
14	2.00002-00	2.30000-07		2 85005-09			0 05005 00			
14	2.3000E-07	2.0000000000	2.00000000000	2.00002-00	2.00002-08	2.00002-08	2.000UE-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.0000E-08	2.0000E-08	2.0500E-08	2.0000E-08	2.0000E-00	2.0000E-00	2.0000E-08	2.0000E-08	2.6500E-08	2.8500E-08
	2 8500E-08	2 3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	2.0000E+00	2.00002-00	2.0000E-00	2.00002-08	2.00002-08
15	0.0000E+00	2.3850E-07	2.8500E-08	2.8500E-08	2.8500E-08	2 8500E+08	2 8500E-08	2 85005-09	2 85005-09	2 85005-00
	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.0000E-08	2.0000E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
16	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.3850E-07	0,0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
17	0.0000E+00	2.3850E-07	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.8500E-08
	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
••	2.6500E-08	2.3860E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
10		2.3860E-07	2.00UE-08	2.38602-07	0.000E+00	0.0000E+00	2.3860E-07	2.8500E-08	2.8500E-08	2.6500E-08
	2.000000000	2.00002-00	2.0000E-08	2.00002-08	2.00UUE-U8	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.0000E-00	2.0000E-00	2.0000E+00	2.000000	2.000000-00	2.000000-00	2.00002-08	2.0500E-08	2.6500E-08	2.8500E-08
19	0.0000E+00	2.3000E=07	2 8500E+00	2 38505-07		0.0000E+00	2 29505-07	2 85005 00	0 05005 00	0 05005 00
	2.6500E-08	2.8500E-08	2.6500E=00	2.8500E-07	2 8500E-08	2 8500E-08	2.3000E-07	2.00002-00	2.00002-08	2.00002-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.0000E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	LICCOCL CO	2.00002-00	2.00002-00	2.00002-00
<b>20</b> ်	0.0000E+00	2.3850E-07	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500F-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
21	0.0000E+00	2.3850E-07	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
22	0.0000E+00	0.0000E+00	0.0000E+00	0,0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
<b>.</b>	2.3850E-07	0.0000E+00	0.0000E+00	U.0000E+00	U.0000E+00	0.0000E+00				
23		0.000E+00	0.000E+00		0.000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08
		2.00UUE-U8	2.00UUE-U8		2.000UL-08	2.00UUE-08	2.0500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.000000-00	2.0000E-08	2.000000-08	2.000000-08	2.0000E-08	2.00UL-08	2.6POOF-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.300UE-U/	V.UUUE+UU	$\mathbf{U}$			v.u.u.t+u				

and and the test 
24	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500F-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
25	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
26	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
27	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
28	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
29	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.3850E-07	0.0000E+00
••	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
30	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.6600E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.3850E-07
21	0.000E+00	0.000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
31	0.000E+00	0.000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.00000000	2.00UE-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.000000-08	2.00002-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.3850E-07
20	0.0000E+00	0.0000E+00	0.000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
32			0.000E+00	0.000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08
	2.0000000000	2.00000000	2.00002-08	2.000UE-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.0000E+00	2.0000E+00	2.000000-08	2.05002-08	2.6600E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.3850E-07
33	0.0000E+00		0.0000E+00	0.0000E+00	0.0000E+00	0.000E+00		0 05005 00		
55	2 8500E-08	2 8500E-08	2 8500E+00	2 8500E-09	0.0000E+00	2.3860E-07	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2 8500E-08	2.8500E-08	2.00002-00	2.00002-08	2.0000E-00	2.0000E-08	2.00UL-U8	2.6500E-08	2.8500E-08	2.6500E-08
	0.0000E+00	0.0000E+00	2.0000E-00	2.00000000	2.000000-00	2.000000-08	2.00002-08	2.65002-08	2.6500E-08	2.3850E-07
34	0.0000E+00	0.0000E+00	0.0000E+00			2 29505-07	0 05005 00	0 0 00 0 00	0 05005 00	0 05005 00
••	2.6500E-08	2.6500E-08	2.8500E-08	2 8500E-08	2 8500E-09	2.300UE-U/	2.0000E-08	2.0500E-08	2.6500E-08	2.6500E-08
	2.8500F-08	2.8500E-08	2 8500E-08	2.0000L-00	2.0000000000	2.00000000000	2.0000E-00	2.00002-08	2.00002-08	2.0000E-08
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.0000E+00	2.0000E+00	2.00002-00	2.00002-00	2.000000-08	2.3860E-07
35	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2 3850E-07	2 85005-09	2 85005-00	2 85005 00	0 85005 00
••	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2 8500E-08	2.36500E-07	2.0000E-00	2.0000E-08	2.000000000	2.0500E-08
	2.6500E-08	2.6500F-08	2.6500E-08	2.6500E-08	2.8500E-08	2.0000E-08	2.0000000000	2.0000000000	2.000000000	2.00UUE-U8
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.00002-00	2.00002-00	2.00002-00	2.30002-07
36	0.0000E+00	0.0000E+00	2.3850E-07	0.0000E+00	0.0000E+00	2 3850E-07	2 8500E-08	2 85005-09	2 85005-09	2 85005-00
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500F-08	2.6500E-08	2 8500E-08	2.8500E-08	2.0000E-00	2.0000E-08	2.0000000000
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.0000L-00	2.0000E-00	2.0000000000	2.0000000000
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.00002-00	2.00002-00	2.00002-00	2.30002-07
37	0.0000E+00	0.0000E+00	2.3850E-07	0.0000E+00	0.0000E+00	2.3850E-07	2 8500E-08	2 8500E-08	2 8500E-08	2 8500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.0000E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2 3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000F+00		2.0000L-00	F.0000E-00	
38	0.0000E+00	0.0000E+00	2.3850E-07	0.0000E+00	2.3850E-07	2.8500F-08	2.6500F-08	2.8500F-08	2.8500F-09	2.8500F-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500F-08	2.6500F-08	2.8500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500F-08	2.6500E-08	2.8500F-08	2.8500F-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				2100002 00
39	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500F-08
			-	-						

nan daan yang ping unit daan daan yang unit yang yang y

.

•

	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.3850E-07
	2.6500E-08	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	- -			
40	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500F-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2 8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.3850E-07	2 8500E-08
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00			2.00002 0/	2.0000L-00
41	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500F-08	2.8500E-08	2 8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2 8500E-00	2.00002-00
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2 3850E-07	2.00002-00
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00		1.00002 00	1.00000-07	2.00002-00
42	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.8500F-08	2.8500F-08	2 8500E-08	2 85005-09	0 85005 00
	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2 8500E-08	2.00002-08	2.00002-00	2.0500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500F-08	2.6500E-08	2 8500E-08	2 8500E-00	2.000000000000	2.0000E-08	2.000UE-08
	2.6500E-08	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.00002-00	2.00002-00	2.00002-08	2.3860E-07
43	0.0000E+00	0.0000E+00	2.3850F-07	2 8500E-08	2 8500E-08	2 8500E-08	2 85005-00	0 85005 00	0 05005 00	
	2.6500E-08	2 8500E-08	2 AEOOE_09	2.00002-00	2.00000000000	2.00000000000		2.00UUE-U8	2.8500E-08	2.8500E-08
	2 8500E-08	2 85005-09	2.0000L-00	2.00002-00	2.000000000	2.05002-08	2.00002-08	2.6500E-08	2.8500E-08	2.8500E-08
	0.0000E+00		0.0000E+00		2.0000000000	2.000000-00	2.000UE-08	2.0000E-08	2.3860E-07	2.6500E-08
44	0.0000E+00		2 2950E-07			0.000E+00	A AF005 00			
	2 8500E-08	2 8500E-09	2.30000-07	2.0000E-00	2.00000000	2.00002-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08
	2.0000E-08	2.0000E-00	2.000000000	2.00UUE-U8	2.0500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.00000000000	2.0000E-00	2.0000E-00	2.000000-00	2.00UUE-08	2.0000E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.3850E-07
45			0.000E+00	0.00002+00	0.000E+00	0.0000E+00				
40			2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.65002-08	2.0500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.00002-08	2.0500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
40	2.38802-07	2.6500E-08	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
40		0.000E+00	2.3850E-07	2.8500E-08	2.8600E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.00UE-U8	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.05002-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
47	2.38802-07	2.6600E-08	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
47	0.00002+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
40	2.3860E-07	2.6500E-08	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	_			
40	0.0000E+00	0.000E+00	2.3850E-07	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
49	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
50	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
51	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500F-08
	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00		•		
52	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500F-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
53	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2 8500E-09	2 85005-09
	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500F-08	2.8500F-09	2 85005-00	2 85005-00
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500F-08	2.8500F-08	2 85005-09	2 85005-09
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000F+00				2.000000-08
54	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.8500F-08	2.85005-02	2 85005-09	2 85005-00
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500F-08	2.8500F-08	2 85005-09	2 85005-00	
										2.000000-00

.
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
55	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
56	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
57	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
58	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
59	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500F-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
60	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.3850F-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	_			
61	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
62	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
83	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
64	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
65	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
66	0.0000E+00	0.0000E+00	0.0000E+00	2.3850E-07	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.8500E-08	2.3850E-07
	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
67	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.3850E-07
_	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00				
68	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08
_	2.3850E-07	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00		_		
69	0.0000E+00	0.0000E+00	2.3850E-07	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08	2.8500E-08
	2.6500E-08	2.8500E-08	2.6500E-08	2.8500E-08						
	2.6500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.6500E-08	2.6500E-08	2.6500E-08	2.8500E-08	2.8500E-08

nay was sure while was sure that the same same

.

1	12	32	1188.	0.9868	1178.	56
1	12	33	1188.	0.5263E-01	1178.	57
1	13	31	1188	1 053	1179	50
	12	20	1100.	1.003	1178.	88
1	13	32	1188.	0.9868	1178.	59
1	14	31	1188.	1.053	1178.	60
1	- 14	32	1188.	1.579	1178.	61
1	15	31	1188	1 250	1179	80
	16	20	1100.	1.200	1170.	02
1	10	32	1100.	0.9868	11/8.	63
1	16	30	1188.	0.9868E-01	1178.	64
1	16	31	1188.	1.318	1178.	85
1	18	32	1199	0 5021	1170	00
-	17	20	1100.	0.0921	1170.	66
1	17	30	1100.	0.1974	1178.	87
1	17	31	1188.	1.316	1178.	68
1	17	32	1188.	0.3947	1178.	69
1	18	30	1188	0 2981	1179	70
1	19	21	1100	1 210	1170.	70
1	10	91	1100.	1.310	11/8.	/1
1	19	30	1188.	0.6908	1178.	72
1	19	31	1188.	0.7895	1178.	73 .
1	20	30	1188.	0 7401	1178	74
1	20	31	1188	0 7905	1170	75
▲	20	97	1100.	0.1030	11/8.	16
1	21	30	1188.	0.8882	1178.	78
1	21	31	1188.	0.6579	1178.	77
1	22	29	1188.	0.1845	1178	79
- 1	22	30	1189	0 0880	1170	70
±	~~	21	1100.	0.3000	11/0.	19
1	22	31	1198.	0.5283	1178.	80
1	23	29	1188.	0.5921	1178.	81
1	23	30	1188.	1.480	1178.	82
1	23	31	1188	0 4934	1179	02
	24	00	1100	0.7007	1170.	03
L	24	28	1100.	0.4441	11/8.	84
1	24	29	1188.	0.9868	1178.	85
1	24	30	1188.	1.332	1178.	86
1	25	28	1188	0 1318	1179	97
- 1	05	27	1100	0.1010	1170.	07
±	20	21	1100.	0.4834	11/8.	88
1	25	28	1188.	O.9868	1178.	89
1	25	29	1188.	1.316	1178.	90
• 1	25	30	1188	0.7895	1179	01
		20	1100	0.1000 0.0001E 01	1170	91
	20	~~	1100.	0.2401E-01	11/8.	92
1	26	23	1188.	0.4934E-01	1178.	93
1	26	24	1188.	0.7895E-01	1178.	94
1	26	25	1188	0.9868F-01	1179	05
	20	26	1100	0.0000L-01	1170	<i>00</i>
1	20	20	1199.	O'ARCAF-OI	1178.	96
1	26	27	1188.	0.1480	1178.	97
1	26	28	1188.	0.1480	1178.	98
1	28	29	1188	0 98685-01	1179	00
	07		1100		1170.	77 100
1	21	20	1198.	0.2632E-01	1178.	100
1	27	21	1188.	0.5921E-01	1178.	101
1	27	22	1188.	0.8579E-01	1178	102
- 1	27	23	1189	0 8570E_01	1170	102
	£1 07	23	1100.		11/0.	103
1	27	24	1188.	0.6579E-01	1178.	104
1	27	25	1188.	0.8579E-01	1178.	105
1	27	28	1188.	0.8579F-01	1179	108
		27	1199	0.00000-01	1170	107
±	41	21	1100.	0.300000-01	11/8.	10/
1	27	28	1188.	0.3947E-01	1178.	108
1	28	19	1188.	0.1974E-01	1178.	109
1	28	20	1188	0.8579F-01	1179	110
± 1	20	2.0	1100.		11/0.	110
L	20	21	1100.	0.00/45-01	11/8.	111
1	28	22	1188.	0.6579E-01	1178.	112
1	28	23	1188.	0.6579E-01	1178	113
- 1	29	24	1188	0 85795-01	1179	114
±	20	<u>4</u> 7	1100.	0.00/92-01	11/8.	114
1	28	26	1198.	0.6679E-01	1178.	115
1	28	26	1188.	0.9868E-01	1178.	116

inge sinde state with sinde sinde sinde sinde state sinde same

.

1	44	13	1188.	0.3289E-01	1178.	239
1	45	8	1188.	0.4934F-01	1178.	240
1	45	9	1188	0 3701E-01	1178	241
1	45	10	1199	0.3701E-01	1170.	. 040
1	40	11	1100.	0.37012-01	1170.	242
	40	10	1100.	0.24676-01	11/8.	243
1	• 40	12	1100.	0.246/E-01	11/8.	244
1	45	13	1188.	0.1234E-01	1178.	245
1	46	8	1188.	0.3947E-01	1178.	246
1	46	9	1188.	0.3701E-01	1178.	247
1	48	10	1188.	0.3701E-01	1178.	248
1	46	11	1188.	0.2467E-01	1178.	249
1	48	12	1188.	0.2467E-01	1178	250
ī	48	13	1188	0 12345-01	1179	251
1	47		1199	0.12346-01	1170.	201
-	47	ŏ	1100.		1170.	202
	47	10	1100.	0.24672-01	1178.	263
1	4/	10	1188.	0.2487E-01	1178.	264
1	47	11	1188.	0.1845E-01	1178.	255
1	47	12	1188.	0.1645E-01	1178.	256
1	48	8	1188.	0.1316E-01	1178.	257
1	48	9	1188.	0.2467E-01	1178.	258
1	48	10	1188.	0.2467E-01	1178.	259
1	48	11	1188	0.1845E-01	1178	280
1	48	12	1188	0.1845E-01	1179	281
1	40	ā	1188	0.24875-01	1170.	201
	40	10	1100.	0.24076-01	1170.	202
1	40	10	1100.	0.24072-01	11/0.	203
	49	11	1100.	0.16452-01	11/8.	264
1	49	12	1188.	0.1845E-01	11/8.	265
1	49	13	1188.	0.8220E-02	1178.	266
1	50	9	1188.	0.2487E-01	1178.	267
1	50	10	1188.	0.2487E-01	1178.	268
1	50	11	1188.	0.1845E-01	1178.	269
1	50	12	1188.	0.1845E-01	1178.	270
1	50	13	1188.	0.8220E-02	1178.	271
1	51	9	1188.	0.2467E-01	1178	272
ī	51	10	1188	0 2487E-01	1178	272
1	51	11	1100.	0.18455-01	1170.	275
1	51	10	1100.	0.10462-01	11/0.	2/4
4	51	12	1100.	0.10462-01	11/8.	275
Ţ	51	13	1198.	0.8220E-02	11/8.	278
1	52	9	1188.	0.2981E-01	1178.	277
1	52	10	1188.	0.3701E-01	1178.	278
1	52	11	1188.	0.2467E-01	1178.	279
1	52	12	1188.	0.2487E-01	1178.	280
1	52	13	1188.	0.1234E-01	1178.	281
ĩ	53	9	1188.	0.2981E-01	1178	282
1	53	10	1188	0.37015-01	1179	202
1	E 2	11	1100.	0.3/016-01	1170.	203
4	53	10	1100.		11/8.	284
1	53	12	1188.	0.2467E-01	1178.	285
1	63	13	1168.	0.1234E-01	1178.	286
1	54	9	1188.	0.4441E-01	1178.	287
1	54	10	1188.	0.4934E-01	1178.	288
1	54	11	1188.	0.3289E-01	1178.	. 289
1	54	12	1188.	0.3289E-01	1178.	290
1	Б4	13	1188	0.1845F-01	1178	201
1	55	-0	1189	0 4441E_01	1179	200
1	55	10	1100.	0.40245 01	1170.	232
1	00 EE	10	1100.	0.49346-01	11/8.	293
1	55	11	1188.	0.4934E-01	1178.	294
1	55	12	1188.	0.4934E-01	1178.	295
1	55	13	1188.	0.2467E-01	1178.	296
1	56	9	1188.	0.5921E-01	1178.	297
1	56	10	1188.	0.7401E-01	1178.	298
1	56	11	1188.	0.4934E-01	1178.	299
-						

						,
1	34	16	1188.	0.3289E-01	1178.	178
1	34	17	1188.	0.1645E-01	1178.	179
1	35	8	1188.	0.9870Ė-02	1178.	180
1	35	9	1188.	0.4934E-01	1178.	181
1	35	10	1188.	0.4934E-01	1178.	182
1	- 35	11	1188.	0.3289E-01	1178.	183
1	35	12	1188.	0.3289E-01	1178.	184
1	35	13	1188.	0.16466-01	1178.	185
1	30	10	1100.	0.3289E-01	11/8.	188
1	30	10	1100.	0.1046E-01	11/8.	187
1	38	0	1188	0.37015-01	1170.	100
1	36	10	1188	0.3701E-01	1179	109
i	36	11	1188.	0.2467E-01	1178.	190
1	38	14	1188.	0.9870E-02	1178	191
ī	36	15	1188.	0.1480E-01	1178.	193
1	37	8	1188.	0.3947E-01	1178.	194
1	37	9	1188.	0.3701E-01	1178.	195
1	37	10	1188.	0.3701E-01	1178.	196
1	37	11	1188.	0.1234E-01	1178.	197
1	37	14	1188.	0.1974E-01	1178.	198
1	38	8	1188.	0.3289E-01	1178.	199
1	38	9	1188.	0.2487E-01	1178.	200
1	38	10	1188.	0.2487E-01	1178.	201
1	38	12	1188.	0.8220E-02	1178.	202
1	38	14	1188.	0.1645E-01	1178.	203
1	38	Ö	1100.	0.32892-01	11/8.	204
1	30	10	1188	0.2407E-01	1170.	205
1	39	11	1188.	0.3290E-01	1178	200
ī	39	12	1188.	0.1316E-01	1178	207
ī	39	14	1188.	0.1845E-01	1178.	209
1	40	8	1188.	0.3289E-01	1178.	210
1	40	9	1188.	0.2467E-01	1178.	211
1	40	10	1188.	0.1974E-01	1178.	212
1	40	11	1188.	0.1645E-01	1178.	213
1	40	12	1188.	0.1316E-01	1178.	214
1	40	14	1188.	0.1645E-01	1178.	215
1	41	8	1188.	0.3289E-01	1178.	216
1	41	9	1188.	0.2467E-01	1178.	217
1	41	10	1188.	0.1860E-01	1178.	218
1	41	12	1100.	0.10466-01	1178.	219
1	41	13	1188	0.13185-01	1170.	220
i	42		1188	0.4934E-01	1178	221
ī	42	9	1188.	0.3701E-01	1178	222
ī	42	10	1188.	0.2220E-01	1178.	224
ī	42	11	1188.	0.2467E-01	1178.	225
1	42	12	1188.	0.2487E-01	1178.	228
1	42	13	1188.	0.2467E-01	1178.	227
1	43	8	1188.	0.4934E-01	1178.	228
1	43	9	1188.	0.3701E-01	1178.	229
1	43	10	1188.	0.2590E-01	1178.	230
1	43	11	1188.	0.2487E-01	1178.	231
1	43	12	1188.	0.2487E-01	1178.	232
1	43	13	1188.	0.2467E-01	1178.	233
1	44	8	1188.	0.6579E-01	1178.	234
1	44	10	1108.	U.4934E-U1	11/8.	235
1	44	10	1100. 1100	U.4334E-UI A 22805 A1	11/8.	238
1	74 A A	10	1100.	0.32095-01	1170.	237
-			1100.	0.32036-01	11/0.	238

and and the same with the same t

.

.

.

1	28	27	1188	0 5921E-01	1178	117
ī	20	12	1100	0 85905 00	1170	110
-	23	12	1100.	0.000000-02	1170.	110
1	29	13	1188.	0.1320E-02	1178.	119
1	29	18	1188.	0.3947E-01	1178.	120
1	29	19	1188.	0.6579E-01	1178.	121
1	. 29	20	1188	0 8579E-01	1178	122
-	20	21	1100	0.85705 01	1170.	122
-	29	21	1100.	0.66792-01	11/8.	123
1	29	22	1188.	0.6579E-01	1178.	124
1	29	23	1188.	0.6579E-01	1178.	125
1	29	24	1188.	0.6579E-01	1178	*128
1	20	25	1100	0 48055 01	1170	107
	23	20	1100.	0.40082-01	11/0.	127
1	29	20	1188.	0.2961E-01	11/8.	128
1	. 30	13	1188.	0.1645E-01	1178.	129
1	30	14	1188.	0.3947E-01	1178.	130
1	30	15	1188	0 9870E-02	1178	121
-	20	10	1100	0.0000000000	1170	101
-	30	10	1100.	0.32892-01	11/8.	132
1	30	17	1188.	0.5592E-01	1178.	133
1	30	18	1188.	0.6579E-01	1178.	134
1	30	19	1188.	0.8579E-01	1178	135
ĩ	30	20	1199	0 85795-01	1170	120
:	30	20	1100.		1178.	130
1	30	21	1188.	0.62/9E-01	1178.	137
1	30	22	1188.	0.6579E-01	1178.	138
1	30	23	1188.	0.3947E-01	1178.	139
1	30	24	1188	0 1316E-01	1178	140
1	21	10	1100		1170	140
-	31	12	1100.	0.8220E-02	11/8.	141
1	31	13	1188.	0.3289E-01	1178.	142
1	31	14	1188.	0.3289E-01	1178.	143
1	31	15	1188.	0.3289E-01	1178.	144
1	31	16	1188	0 3289F-01	1178	145
	21	17	1100.		1170.	140
-	31	17	1100.	0.32892-01	11/8.	146
1	31	18	1188.	0.3289E-01	1178.	147
1	31	19	1188.	0.3289E-01	1178.	148
1	31	20	1188.	0.3289E-01	1178.	149
ī	31	21	1198	0 2303E-01	1178	150
-	20		1100.	0.23032-01	1170.	100
1	32	10	1188.	0.1480E-01	1178.	151
1	32	11	1188.	0.3701E-01	1178.	152
1	32	12	1188.	0.4934E-01	1178.	153
1	32	13	1188.	0.4934E-01	1178.	154
1	32	14	1188	0 4934E-01	1179	155
-	20	16	1100.	0.4004E 01	1170.	100
-	92	10	1100.	0.49342-01	11/8.	190
1	32	16	1188.	0.4934E-01	1178.	157
1	32	17	1188.	0.4934E-01	1178.	158
1	32	18	1188.	0.4934E-01	1178.	159
1	32	19	1188	0.2467F-01	1178	180
-	20		1100		1170.	100
	32	20	1100.	0.14802-01	11/8.	101
1	33	9	1188.	0.7400E-02	1178.	162
1	33	10	1188.	0.4934E-01	1178.	163
1	33	11	1188.	0.3289E-01	1178.	164
1	33	12	1188	0 3289E-01	1179	165
-	22	12	1100.		1170.	100
1	33	13	1188.	0.3289E-01	11/8.	166
1	33	14	1188.	0.3289E-01	1178.	167
1	33	15	1188.	0.3289E-01	1178.	168
1	33	16	1188.	0.3289F-01	1178.	189
1	33	17	1188	0 3289E-01	1179	170
-	20	10	1100.	0.32032-01	11/0.	170
1	33	18	1198.	0.8220E-02	11/8.	171
1	34	9	1188.	0.3454E-01	1178.	172
1	34	10	1188.	0.4934E-01	1178.	173
1	34	11	1188	0.3289F-01	1178	174
1	24	10	1100	0 32905 01	1170	477
	34	12	1100.	0.32092-01	11/8.	1/5
T	34	13	1188.	0.3289E-01	1178.	176
1	34	14	1188.	0.2632E-01	1178.	177

. . .

2.6500E-08 2.3850E-07 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

.

.

.

357 RIVER REACHES

LAYER	ROW	COL	STAGE	CONDUCTANCE	BOTTOM ELEVATION	RIVER REACH
1	1	22	1188.	2.961	1178.	1
1	1	23	1188.	5.329	1178.	2
1	1	24	1188.	5.921	1178.	3
1	1	25	1188.	5.921	1178.	4
1	1	28	1188.	2.961	1178.	5
1	1	27	1188.	2.664	1178.	8
1	1	29	1188.	1.184	1178.	7
1	1	30	1188.	3.553	1178.	8
1	1	31	1188.	7.105	1178.	9
1	2	23	1188.	0.1974	1178.	10
1	2	24	1188.	0.7895	1178.	11
1	2	25	1188.	1.184	1178.	12
1	2	28	1188.	1.579	1178.	13
1	2	27	1188.	2.368	1178.	14
1	2	28	1188.	4.145	1178.	15
1	2	29	1188.	6.316	1178.	16
1	2	30	1188.	8.289	1178.	17
1	2	31	1188.	12.63	1178.	18
1	2	32	1188.	7.105	1178.	19
1	3	29	1188.	3.684	1178.	20
1	3	30	1188.	6.316	1178.	21
1	3	31	1188.	8.421	· 1178.	22
1	3	32	1188.	7.895	1178.	23
1	4	31	1188.	7.105	1178.	24
1	4	32	1188.	8.289	1178.	25
1	4	33	1188.	0.3158	1178.	26
1	4	34	1188.	0.4737	1178.	27
1	4	35	1188.	0.6316	1178.	28
1	5	30	1188.	0.3947	1178.	29
1	5	31	1188.	4.211	1178.	30
1	5	32	1188.	7.105	1178.	31
1	5	33	1188.	0.2105	1178.	32
1	5	34	1188.	0.3158	1178.	33
1	5	35	1188.	0.4211	1178.	34
1	6	31	1188.	2.763	1178.	35
1	6	32	1188.	5.329	1178.	36
1	6	33	1188.	0.1579	1178.	37
1	8	35	1188.	0.3158	1178.	38
1	7	31	1188.	1.842	1178.	39
1	7	32	1188.	3.158	1178.	40
1	7	33	1188.	0.1053	. 1178.	41
1	7	35	1188.	0.2105	1178.	42
1	8	31	1188.	1.382	1178.	43
1	8	32	1188.	2.368	1178.	44
1	8	33	1188.	0.7895E-01	1178.	45
1	9	31	1188.	1.382	1178.	48
1	9	32	1188.	1.776	1178.	47
1	9	33	1188.	0.7895E-01	1178.	48
1	10	31	1188.	0.9211	1178.	49
1	10	32	1188.	0.9868	1178.	50
1	10	33	1188.	0.5263E-01	1178.	51
1	11	31	1188.	1.053	1178.	52
1	11	32	1188.	0.9868	1178.	53
1	11	33	1188.	0.5263E-01	1178.	54
1	12	31	1188	1.053	1178	55

1	58	12	1188.	0.4934E-01	1178.	300
1	58	13	1188.	0.1480E-01	1178.	301
1	57	8	1188.	0.1053	1178.	302
1	57	9	1188.	0.9868E-01	1178.	303
1	57	10	1188.	0.9868E-01	1178.	304
1	. 57	11	1188.	0.8579E-01	1178.	305
1	57	12	1188	0 1974E-01	1178	308
1	59	Ā	1199	0.1184	1170.	300
-	50	7	1100.	0.1107	1170.	307
	50		1100.	0.2308	1170.	308
1	50		1100.	0.1974	11/8.	309
1	58	9	1188.	0.1480	1178.	310
1	68	10	1188.	0.1480	1178.	311
1	58	11	1188.	0.1974E-01	1178.	312
1	59	6	1188.	0.3158	1178.	313
1	59	7	1188.	0.8882E-01	1178.	314
1	59	9	1188.	0.1332	1178.	315
1	59	10	1188.	0.1332	1178.	316
1	60	6	1188.	0.2368	1178.	317
1	60	7	1188.	0.1184	1178.	318
1	60	9	1188.	0.8882E-01	1178.	319
1	80	10	1188.	0.1480	1178.	320
1	60	11	1188.	0.4934E-01	1178	321
1	61		1188	0 78955-01	1178	300
1	81	7	1199	0 1184	1170	302
1	81	á	1199	0.49345-01	1170.	323
1	81	10	1100.	0.49345-01	1170.	324
1	80	10	1100.	0.49342-01	1178.	325
-	02	ę	1100.	0.394/2-01	11/8.	328
	62	/	1188.	0.88822-01	11/8.	327
1	83	в	1188.	0.1579	1178.	328
1	63	7	1188.	0.1184	1178.	329
1	64	6	1188.	0.1974	1178.	330
1	64	7	1188.	0.4441E-01	1178.	331
1	85	Б	1188.	0.2961E-01	1156.	332
1	65	6	1188.	0.1382	1156.	333
1	66	5	1188.	0.1184	1158.	334
1	66	6	1188.	0.2368	1158.	335
1	67	Б	1188.	0.2961	1158.	336
1 1	67	6	1188.	0.2763	1156.	337
1	67	7	1188.	0.1184	1156.	338
ī	68	Б	1188.	0.1382	1156	339
1	68	Ā	1188	0 2303	1158	340
i		7	1188	0.3454E-01	1158	241
1	88	é	1199	0.2202E-01	1158	341
1	20	0	1100.	0.23032-01	1100.	342
-	20	10	1100.	0.43176-01	1150.	343
1	00	10	1100.	0.17272-01	1160.	344
1	00	11	1100.	0.11612-01	1160.	345
1	08	12	1188.	0.1151E-01	1166.	346
1	68	13	1188.	0.1151E-01	1168.	347
1	68	14	1188.	0.2303E-01	1158.	348
1	68	15	1188.	0.2303E-01	1156.	349
1	69	8	1188.	0.6908E-01	1158.	350
1	69	7	1188.	0.1382	1156.	351
1	69	8	1188.	0.1038	1156.	352
1	69	9	1188.	0.1727E-01	1156.	353
1	69	13	1188.	0.1151E-01	1158.	354
ī	69	14	1188.	0.2303E-01	1158	355
ī	69	15	1188	0.9211E-01	1158	358
ĩ	89	18	1188	0.80595-01	1158	355
•		••		0.0000L-01		307

÷

# APPENDIX K

••

,

. .

# OBSERVED VS. SIMULATED WATER LEVELS USED IN FLOW MODEL CALIBRATION

WELL MW9 (EPA9)





WELL C2S OBSERVED VS. SIMULATED HEADS 1.19 ٠ 1.189 1.188 -1.187 (1.186 -(1.186 -(Thousands) (Thousands) (Thousands) (1.184 -1.183 1.182 1.181 1.18 -+ 87 87.4 85.4 85.8 86.6 86.2 87.8 DATE (years) OBSERVED SIMULATED +

WELL R2D OBSERVED VS. SIMULATED HEADS 1.19 1.189 -Ø 1.188 1.187 (1.186 -(1.186 -(1.185 -(1.185 -1.185 -1.184 -1.183 -1.182 -1.181 -1.18 -86.2 87.8 85.8 87.4 85.4 86.6 87 DATE (years) SIMULATED OBSERVED 



.

OBSERVED VS. SIMULATED HEADS 1.195 ŧ 1.194 -1.193 -1.192 -ELEVATION (feet) (Thousands) (Thousands) (Thousands) (Thousands) (Thousands) (Thousands) (Thousands) (Thousands) B 1.188 -1.187 -1.186 -1.185 -86.2 87.4 87.8 85.4 85.8 86.6 87 DATE (years) OBSERVED SIMULATED +

PLUM ST. TEST WELL

WELL TCT44



WELL MW12 (EPA12) OBSERVED VS. SIMULATED HEADS 1.19 e 1.189 1.188 · 1.187 -(1.186 -(1.186 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -(1.185 -1.183 1.182 1.181 · 1.18 -85.8 86.2 87.4 87.8 85.4 86.6 87 DATE (years) SIMULATED OBSERVED +

WELL MW11 (EPA11) OBSERVED VS. SIMULATED HEADS 1.19 ٠ 1.189 1.188 1.187 ELEVATION (Thousands) (Thousan 1.183 1.182 -1.181 -1.18 -85.8 87 87.4 87.8 85.4 86.2 86.6 DATE (years) SIMULATED OBSERVED +





WELL MW11 (EPA11) OBSERVED VS. SIMULATED HEADS 1.19 1.189 1.188 1.187 ELEVATION (Thousands) (Thousands) (Thousands) (Thousands) (Thousands) 1.183 -1.182 -1.181 -1.18 87 87.4 7 87.8 85.8 86.2 86.6 85.4 DATE (years) OBSERVED SIMULATED 

WELL GM4D OBSERVED VS. SIMULATED HEADS 1.19 1.189 -1.188 -1.187 -(1.186 -(1.186 -(1.185 -(1.185 -(1.185 -1.185 -1.184 -1.183 -1.182 -1.181 -1.18 + 87 87.4 7 87.8 85.8 86.2 86.6 85.4 DATE (years) OBSERVED SIMULATED 



. .

# INDUSTRIAL SURVEY WAUSAU NPL SITE

## **1.0 GENERAL INFORMATION**

An Industrial Survey (Survey) of Potentially Responsible Parties (PRPs) and other businesses and industries located in the vicinity of the Wausau municipal well field was initiated in August, 1987.

The purpose of the Survey was to acquire information on the operations and activities of industries and facilities in the vicinity of the Wausau well field. Emphasis was placed on identifying past and present storage and disposal practices of products or wastes which may have resulted in the release of chemicals, petroleum products and/or solvents to soil or groundwater. Industries and businesses were chosen for the Survey based on type of operation or product produced, location of the facility with respect to probable groundwater flow direction, and documented points of groundwater contamination. Information obtained during the Survey was evaluated and used to complete planning for the Phase I field investigation.

The Survey consisted of a brief interview with entity representatives and a tour of the facility operations and grounds. Photographs were taken in order to determine the status of facilities and operations at the time of the Survey. The Survey also permitted an opportunity to provide information to, and obtain input from, the various entities relating to the Phase I field investigation at their facilities and to determine what measures would be necessary to obtain access to their properties.

A total of eight facilities were included in the August 6 and 7, 1987 Survey. Industries and facilities interviewed and toured during the August 6 and 7 Survey included the following:

Wausau Energy Co. - (Formerly Rush Distributing - Amoco Oil) Steel Flite Scaffolding Marathon Press (Marathon Pilot Graphics) Wergin Construction

C.M. St. P. & P. Railroad (Soo Railroad) Wausau Chemical Co. Marathon Electric Inc. Marathon Box Co.

Several additional area facilities, both closed and active, were added to the Survey during the course of the Phase I field investigation.

These facilities were included due to their strategic locations and recent information (provided by others) which justified reason for inclusion.

Refer to Drawing 13076-B10 for location of surveyed industries and businesses.

2.0 AUGUST 6 and 7, 1987 SURVEY The survey team consisted of the following persons:

Margaret Guerriero - U.S. EPA Project Officer Michelle Debrock - Owens - WDNR Project Hydrogeologist Dennis Iverson - Warzyn Project Manager Craig Rawlinson - Warzyn Project Hydrogeologist

Of the eight facilities surveyed, four reported they currently use chlorinated organic solvents and have reportedly submitted material safety data sheets to the WDNR and/or the U.S. EPA during previous industrial surveys. Facilities in the immediate vicinity of the municipal well field currently using or storing halogenated solvents include:

Wausau Chemical Co. Marathon Press Co. Marathon Electric Inc. Wergin Construction Co.

A summary of information gained from the Survey is presented in the following sections.

## 2.1 WAUSAU ENERGY - 2102 2ND STREET

1

This facility has historically operated as a bulk oil facility and has undergone several changes of ownership during the past 15 years. According to Mr. Daniel K. LaCerte, General Manager, Wausau Energy acquired the bulk oil

facility from Rush Distributing in 1983. Rush Distributing purchased the facility from Amoco Oil in 1975 and operated it as a bulk oil distribution plant. Prior to 1975, Amoco Oil operated the bulk distribution facility for approximately 30 years. Mr. LaCerte indicated Wausau Energy acquired the facility as part of a buyout of Rush Distributing that was designed to expand their customer base. The facility has reportedly not been used as an industrial facility by Wausau Energy, but is currently leased to Marathon Press for warehouse purposes. However, during the course of field work, several Wausau Energy tank trucks were observed at the facility.

The property includes a one story brick framed office and storage building and attached three bay garage located on the north side of the structure (Photo 1). The southernmost bay had an earthern floor which exhibited some soil staining. A former bulk tank farm was located directly south of the building (Photo 2). A railroad spur and loading docks are located on the west side of the building (Photo 3).

Mr. LaCerte indicated the above ground tanks were removed in 1983, shortly after Wausau Energy acquired the property. He was not aware of buried tanks being located at the site. According to Mr. Areland Rush (Rush Distributing), Amoco operated the facility as a bulk oil facility which received oil and petroleum products by rail. Review of the Soo Railroad manifests confirm several bulk petroleum product shipments to Amoco Oil during this time. The products were unloaded at the spur area on the west side of the building and were either stored or repackaged for distribution in the Wausau area. This process continued until 1969 when rail service deliveries were discontinued. Subsequent to 1969 deliveries were made by truck. Based on inventory of records, the following products were reportedly handled by Rush Distributing and Amoco: No. 1 fuel oil, No. 2 fuel oil, lead free gasoline, premium gasoline, regular gasoline, kerosene, diesel fuel, hydraulic fluids, and motor oils (Foth and Van Dyke, June, 1986).

Mr. Rush indicated in addition to petroleum products, Amasol, a degreasing compound, was also stored and sold. The composition of this compound is not presently known. Mr. Rush also indicated a fuel oil leak occurred during the early 1970's, while he was an employee of Amoco. The leak reportedly occurred along the east side of the building and drained into the storm sewer on Second

-3-

Street. During a 1984 hydrogeologic investigation of the East Wausau Well Field, the WDNR detected PCE and Toluene contamination in soil samples collected from near the southwest loading dock. Neither Mr. Rush or Mr. LaCerte was aware of any spills or leaks in this area.

At the request of the WDNR, Wausau Energy contracted a consultant (Foth and Van Dyke) to perform a hydrogeologic investigation of the facility. Soil samples from eight test borings were collected and analyzed for VOCs. Analyses of these soil samples indicated detectable concentrations of several hydrocarbon related compounds including: benzene, ethylbenzene, toluene and xylenes (BETX). Based on the borings, soil impact appears to be greatest in the vicinity of borings 2, 3 and 4 located southwest of the Wausau Energy building. Generally, the greatest soil impact was detected at a depth of 15 feet (just above the water table). In addition to BETX impact on soils southwest of the Wausau Energy building, PCE was detected in soil samples obtained from Borings TB-7, TB-104 and TB-105 located northeast of the Wausau Energy building (Foth and Van Dyke, June, 1986 and December, 1986). PCE detected in soil samples along the North side of Wausau Energy may be related to past storage of waste products in this area (see Foth and Van Dyke, December 1986). Groundwater monitoring conducted by Foth and Van Dyke indicate total elevated BETX concentrations in Monitoring Wells TB-5 and TB-2, located south of the main building. These wells also indicate elevated concentrations of PCE and TCE. However, upgradient Monitoring Well WC5A also indicates substantial concentrations of PCE and TCE. Therefore, the observed PCE and TCE concentrations in the groundwater may be the result of on upgradient source.

Mr. Rush indicated that during the bulk facility operation period (1960's to 1983), solid waste disposal was contracted to a solid waste hauler for disposal at the city landfill. Liquid wastes were commonly discharged to the City sanitary sewer system. Mr. LaCerte indicated since the facility is presently leased to Marathon Press for storage purposes, very little waste is currently generated at this facility. The waste that is generated at the site consists of light commercial type refuse including: boxes, crates, paper goods, etc.

## 13076.21

# 3.2 STEEL FLITE SCAFFOLDING - 2308 N. THIRD STREET

The survey initiated with an interview with Irving R. Jacobson (owner). Mr. Jacobson indicated the Company manufactures and leases tubular steel scaffolding. The property was purchased in 1959, and operations were moved from Schofield in 1962. The business operated from a building on the north portion of the site until 1970, after which operations were moved to their present location on the south side of the site. According to Mr. Jacobson, the site was formerly used for lumber storage during the Works Progress Administration (WPA) days of the 1930's. The site was also previously used for sand and gravel excavation and was reportedly filled with miscellaneous debris including construction debris and cuttings from area granite polishing operations.

Mr. Jacobson indicated only minor quantities of solvents are used in his company's operations and material safety data sheets had been provided to the WDNR and/or U.S. EPA during previous industrial surveys. According to Mr. Jacobson, a phosphate detergent (Oakite 31, Cryscoat 187) is used to clean the tubular steel prior to welding. Waste cleaning solution is discharged to the City sanitary sewer through a floor drain. Mr. Jacobson indicated a solvent type paint thinner is added to the paint tank to control paint viscosity. In addition to these materials, approximately 1 gal/month of solvent (brand name Aquasol) is used as a grease cutter and cleaner.

With the exception of the paint dip tank and detergent dip tank, Mr. Jacobson was not aware of any above or below ground tanks on his property. The north building at the site is used to store electrical supplies and no manufacturing operations occur in this building. Manufacturing, painting and management activities are also located in the south building (Photos 4 and 5). Liquid wastes from the south building are disposed to the sanitary sewer and solid waste disposal is handled by a private contractor. Mr. Jacobson was aware of only one spill during the time he has operated the facility. He indicated that a City employee observed one of his employees relatively recently dumped 1 quart of gasoline on soil west of the main building. A sample of the soil was collected by the city for GC-MS analysis. Soil analysis conducted by Zimpro confirmed that gasoline had been disposed on the surface soils. Other

than BETX, no additional compounds were detected. The City notified the WDNR of the incident. The WDNR issued enforcement correspondence to Steel Flite and notified the U.S. EPA.

# 2.3 MARATHON PRESS COMPANY, INC. PARK AVENUE AT SECOND

An interview was conducted with Mr. Ronald A. Westgate, Jr. (President of marathon Press Company). Mr. Westgate indicated Marathon Press has operated at the current address for approximately 30 years. Prior to operations as Marathon Press, the property was owned by the Alexander family (local developers). Marathon Press provides printing and graphics services for commercial and industrial clients.

Marathon Press facilities consists of two buildings separated by a loading dock and transport staging area (Photo 6). The southern building is located on the corner of Park and 2nd Street. This building houses the printing and graphics operations (Photo 7). A tour of the facility indicated the following processes and materials usage:

<u>Process</u>	<u>Material Usage</u>
Type Setting	Developer and activator
Plate Making	Plate developer and fixer
Developing Room	Photo developing agents and fixer
Letter Press	Rubber based ink, Hanculite (C-247 solvent) is used to clean machinery
Offset Printing	Various inks, alcohol and mineral spirits

Mr. Westgate indicated small quantities of alcohol and solvents (primarily acetone) were used to clean equipment. These materials are delivered to the loading dock on the north side of the main building.

Solvents and other bulk liquids are stored in a fenced concrete pad and curbing area located at the northeast corner of the main building. Mr. Westgate has reportedly supplied the WDNR and U.S. EPA with material safety data sheets. According to Mr. Westgate, the solvents are received in bulk quantity (55 gallon drums) and are transferred to smaller containers (1 gallon) which are stored near the printing presses. Photo 6 shows the loading dock and drum storage area. The solvents are applied to rags used to clean and degrease equipment and machinery. Mr. Westgate estimated Marathon Press uses approximately one 55 gallon drum of solvent per year.

Mr. Westgate indicated solid wastes including solvent applying rags are collected by a private contractor for disposal at the City landfill. Some liquid wastes are disposed through floor drains into the city sanitary sewer system. Other liquid wastes, including developing chemicals, are stored near the loading dock and are collected by a private recycling firm. Mr. Westgate was aware of only one underground tank located at the facility. This tank is located near the south side of the main building and is used to store fuel oil. Mr. Westgate indicated that Marathon Press stores dry goods (paper and printing supplies) in the buildings north of the main facility and at the property owned by Wausau Energy. Mr. Westgate was not aware of any spills during the course of Marathon Press operations at the Wausau Energy facility.

## 2.4 C.M. ST. P&P RAILROAD

The Survey of the railroad consisted of an interview with Mr. Herbert Hentze at the local railroad yard. Mr. Hentze indicated he has been a railroad employee for approximately 40 years and currently holds the position of Roadmaster. Mr. Hentze discussed railroad operations and reviewed manifests dating back to 1979. According to Mr. Hentze, the railroad made bulk deliveries of oil and petroleum products to the former Amoco Oil facility and to Riiser Oil (a former bulk oil facility located north of Wausau Chemical). The rail deliveries of oil discontinued approximately 20 years ago. Bulk deliveries of chlorine and stabilizing compounds including soda ash and potash were made to Wausau Chemical. The rail deliveries were discontinued in 1982. Presently, all shipments to Wausau Chemical are by truck. Mr. Hentze was not aware of any bulk shipments of solvents made to or from any businesses in the Wausau well field vicinity. Mr. Hentze was also not aware of any railcar leaks or spills during his employment by the railroad.

Mr. Hentze indicated a former city landfill was located near the east bank (south side) of the Wisconsin River near Bridge Street. This landfill reportedly closed approximately 45 years ago. Mr. Hentze also pointed out several railroad spurs were used for product transfer areas. One such spur formerly extended along the north side of Marathon Electric.

-7-

#### -8-

# 2.5 WERGIN CONSTRUCTION - 200 E. WAUSAU AVENUE

A brief interview and tour of Wergin construction facility was conducted with Mr. Phil Wergin (owner) and Mr. Joe Malak (Maintenance Foreman). Mr. Wergin indicated the City garage previously occupied the location where Wergin Construction is presently situated. The site was purchased from the City in 1959. Prior to service as a city garage, the east portion of the site was used to store lumber during the 1930's. The site is presently used as base of operations for the construction company and consists of a maintenance building, offices, and equipment and supply storage (Photos 8 and 9). In addition to these structures, much of the site is covered by miscellaneous construction debris, equipment and trailers (Photo 10). Mr. Wergin indicated the Company provides construction services for industrial, commercial and institutional clients.

Mr. Malak indicated limited quantities of solvents are used in cleaning and degreasing operations. He estimated approximately 55 to 75 gallons of solvents are used per year. Phosphate detergents (Johnson Forward and Midwest Fleet Clean) are the primary cleaning compounds used on site. Mr. Wergin indicated Material Safety Data sheets had been supplied to the U.S. EPA. Cleaning solutions and solvents are primarily used in the maintenance building. Mr. Wergin was not aware of any spills or leaks of solvent type material. However, Mr. Malak indicated that a small hydraulic fluid release occurred a couple of years ago. Mr. Wergin indicated the majority of the construction waste generated was disposed by Lloyd Bros. Inc. Surplus materials and salvage materials from construction operations are occasionally stockpiled at the site. Solid wastes generated at the site are either incinerated or disposed by a contracted waste hauler.

Mr. Wergin indicated three underground tanks are present at the site. The tanks are located just west of main building (Refer to Photo 11) and are used to store regular gasoline, unleaded gasoline and diesel fuel for company vehicles. Mr. Malak also indicated an elevated above ground storage tank is used to store waste oil and solvents until they are picked up by a recycling firm. This storage tank is located approximately 150 feet southwest of City Well 3.

## 2.6 WAUSAU CHEMICAL - 2001 N. RIVER DRIVE

The Survey of Wausau Chemical Corporation (Wausau Chemical) consisted of an interview with Mr. James Cherwinka (president) and a tour of facility operations. Mr. Cherwinka indicated the company was established in the 1960's. The southern portion of the property was acquired from the City of Wausau. An additional parcel located just south of E. Wausau Avenue was acquired from Riiser Oil during the early 1970's. This facility formerly operated as a bulk oil distribution plant (Photo 12). Wausau Chemical property extends from E. Wausau Avenue to the north, to the City of Wausau Water Treatment Plant to the south. The facility is bounded on the east by the C.M. ST P&P Railroad and on the west by North River Drive.

Mr. Cherwinka emphasized that Wausau Chemical is not a manufacturing facility. The primary functions of the company are two fold. They act as a transfer station for the collection and shipment of waste chemicals and solvents from area businesses to Waste Research and Reclamation (WRR) in Eau Claire, Wisconsin. Secondly, Wausau Chemical is a distributor for various chemicals and solvents. Mr. Cherwinka indicated Wausau Chemical operates several tractor trailer rigs and one tank truck that is federally and state licensed to transport hazardous waste. According to Mr. Cherwinka, RCRA permits allow Wausau Chemical to store hazardous waste materials for up to 10 days. The permit does not limit the storage of chemicals (i.e., PCE, TCE, DCE) that are not classified as hazardous wastes. Mr. Cherwinka, indicated the WDNR approves the waste stream which can be handled by the Wausau Chemical.

The site consists of a large metal framed building on a concrete slab foundation. Four loading docks are located on the west side of the building. Two additional loading areas are located on the east side of the building. Empty drum storage areas are located on the east and south sides of the building (Photo 13). Several empty storage tanks are located near the southeast corner of the site (Photo 14). Company offices are located in the southwest portion of the building. The remaining building space located in the west central portion of the building is leased to STS Consulting Ltd.

-9-

Wausau Chemical collects spent solvents and chemicals from local businesses and transfers the materials to the WRR recycling facility in Eau Claire, Wisconsin or to an out-of-state Rollins incineration facility. The material is collected in DOT approved 55 gallon drums. These materials are generally shipped directly to the recycling facility or incinerator without unloading or repackaging at the Wausau Chemical facility. However, Mr. Cherwinka indicated that occasionally materials are collected which fail to meet the reclamation facility specifications. These materials must be blended with other chemicals at Wausau Chemical to meet specifications.

According to Mr. Cherwinka, prior to 1984, Wausau Chemical operated a solvent bulk farm in which PCE was stored in several above ground tanks along the south side of the main building. The solvents were transferred from tank cars to the storage tanks and then to 55 gallon drums which were sold and distributed to area businesses. In 1983, the facility experienced two PCE releases and subsequently discontinued the use of the storage tanks. Tanker car deliveries of solvents are now reportedly transferred directly to 55 gallon drums which are warehoused on pallets adjacent to the north loading dock.

Mr. Cherwinka indicated he was not aware of any underground storage tanks on the property. Two of the former above ground oil storage tanks acquired from Riiser Oil are presently used for storage of calcium chloride. The remaining above ground tanks observed on the southeast side of the facility are reportedly empty (Photo 15).

Mr. Cherwinka indicated he was aware of only three spills or leakages of chemical or solvents at the Wausau Chemical facility. He stated that the WDNR was notified in each case. The first spill reportedly occurred in February 1983, near the northwest loading dock (Photo 16). Approximately 100 to 250 gallons of PCE was lost when a small tank was damaged by a fork lift. A portion of the product reportedly pooled on North River Drive and was removed using snow plows. Remaining product was flushed into storm sewers and the River during thaw events. The largest release reportedly occurred in

December, 1983 when a storage tank located south of the main building experienced a valve malfunction which resulted in the leakage of approximately 900 gallons of virgin PCE. A portion of the product reportedly pooled on the frozen ground was removed. Affected soils and storage tanks were removed during the spring of 1984. A third small spill of approximately 2 to 3 gallons of PCE occurred in late 1986. This spill occurred on the bituminous pavement area near the southwest loading dock.

Mr. Cherwinka was not aware of any additional spills. However, file information indicates soil excavations conducted for the water treatment plant expansion in 1975 encountered soils and groundwater contaminated by PCE, TCE, toluene, and xylenes along the south side of Wausau Chemical property. WDNR requested Wausau Chemical to remove contaminated soil, however, no action was reportedly taken to address the requests.

STS Consulting Ltd. of Green Bay, Wisconsin was contracted by Wausau Chemical to perform a hydrogeologic investigation of the groundwater impact from the 1983 PCE releases. Results of this investigation are presented in reports dated July 25, 1984; April 3, 1985 and in subsequent correspondence. STS was retained by Wausau Chemical to design and implement a groundwater extraction and treatment system. A groundwater extraction system consisting of 15 wells was installed during the summer and fall of 1985. An air stripper was installed during the week of October 11, 1985 for treatment of contaminated groundwater (Refer to Photo 15). The system was operated intermittently from October 31, 1985 to December 5, 1985, after which the system remained inoperative until June 24, 1986. With the exception of periodic maintenance and winterization, the system has reportedly been operated continuously since June 1986.

Groundwater extraction has been accomplished by pumping well clusters generally consisting of six extraction wells arranged in a rectangular array. Since installation in October 1985, the system has been operating an equivalent of approximately 250, 24-hour pumping days. Discharge rates have fluctuated substantially, but generally have averaged approximately 100 GPM.

## 2.7 MARATHON ELECTRIC - 100 EAST RANDOLPH STREET

The Survey of the Marathon Electric facility consisted of an interview with Mr. David Eisenreich (Vice President of Administration) and Mr. Mark Thimke (Foley and Lardner, Attorneys at Law). Following the interview a plant tour was provided by Mr. Walter Matson (Plant Manager). Mr. Eisenreich indicated Marathon Electric has been operating at the present site for approximately 45 years. The company manufactures electric motors ranging from 1/2 H.P. to 500 H.P. and generators ranging from 50 K.W. to 1000 K.W. According to Mr. Eisenreich, Marathon Electric used to manufacture washing machines. The company currently employs approximately 1000 persons. Marathon Electric's manufacturing processes can be separated into fabricating processes and assembly processes. Fabrication operations include: foundry, punch press, aluminum diecast and machining of aluminum and iron. Assembly operations include: shaft machining, frame fabrication, winding, subassembly and painting. Specific processes and materials utilized in plant operations are shown on Table 1. Refer to Drawing 13076-A16 for location of plant operations.

The Marathon Electric site occupies approximately 30 acres bounded by Randolph Street on the north, Cherry Street on the west, the Wisconsin River on the east and Employers Insurance Company and the James River Corporation on the south (Drawing 13076-B10). The site consists of two main buildings, the foundry/fabrication building located on the southern portion of the site (Photo 17), and the assembly building located in the northern part of the site. The assembly building includes corporate offices and shipping and receiving areas (Photos 18 and 19). A large parking lot separates the two buildings. Numerous small storage buildings are located south of the plant foundry. These warehouses are reportedly owned by Employers Insurance Company of Wausau and Marathon Electric. Refer to Drawing 13076-A16 for locations of plant operations.

Mr. Eisenreich indicated the present foundry facilities were constructed in 1969, over a portion of the former City of Wausau landfill. Prior to 1969, the foundry was located southwest of the main office. During a previous plant survey (WDNR 1982), Mr. Matson indicated that 55 gallon drums of waste were encountered during excavation for the foundry building foundation. Mr. Eisenreich was not familiar with Marathon Electric chemical useage, waste generation or disposal practices. However, Mr. Matson indicated that Marathon Electric operations required the useage of a wide variety of paint, varnish, stripping compounds, solvents, caustics, acids, etc. Material and chemical usage for 1974 is presented in Table 2. Based on the types of quantities of waste generated, Marathon Electric is classified as a hazardous waste generator and is RCRA permitted to store and transport hazardous materials. The company currently stores hazardous wastes in warehouse #5, located south of the foundry (See Photo 20). Prior to 1982, hazardous wastes were stored on an asphalt pad located southeast of the foundry. Marathon Electric currently stores drums of varnish adjacent to the receiving area on the southeast side of the assembly building (Refer to Drawing 13076-A16).

Mr. Matson indicated any spills occurring at the plant would be documented in company files. These files were not available during the plant survey. However, WDNR records indicate two documented releases. In October, 1980 an anonymous call was received indicating a paint spill had occurred along the southeast corner of the foundry building. Further investigation indicated a drum containing paint wastes had been ruptured during moving activities. WDNR collected soil samples for heavy metal analyses. Affected soils were subsequently disposed at the Holtz Krouse landfill. In addition, a ruptured barrel containing varnish wastes was noted during a WDNR plant survey in 1982. The company was advised to clean up contaminated soils and to have drums more thoroughly inspected prior to useage.

Mr. Matson indicated that approximately 163,200 gallons of sanitary and contact process water is discharged daily to the city sanitary sewer. Discharge is monitored at three outfalls locations. The company also discharges approximately 73,000 gallons of non-contaminated process water to a sewer which discharges to Bos Creek south of Randolph Street.

According to Mr. Matson there are presently three underground storage tanks located at the Marathon Electric facility. A 20,000 gallon diesel fuel tank is reportedly located near the southwest corner of the foundry. An

8,000 gallon fuel oil tank is located directly east of the receiving dock area. A 20,000 gallon xylene tank is located directly west of the company cafeteria (See Photo 21). Mr. Matson indicated additional tanks were located along the north side of the assembly building, beneath the present cafeteria (Photo 22). These tanks were reportedly removed in 1982 when the cafeteria was built. Mr. Matson was unsure of the contents of these tanks but felt they may have been used to store varnish and or solvents. In addition to the underground storage tanks, an above ground, horizontal, liquid nitrogen tank is located directly west of the cafeteria.

### 2.8 MARATHON BOX - 207 N. 1ST STREET

An interview and site survey was conducted with Mr. Scott Teneyck, Vice President, Marathon Box. Mr. Teneyck indicated that Marathon Box is a family run business that was established at the N. Second Street site in 1928. The company manufactures pallets and crates. According to Mr. Teneyck, Marathon Box moved its manufacturing operations from the site in 1982. A portion of the factory was subsequently removed (see Photos 23 and 24). The site presently consists of three framed buildings and an adjacent lumber storage yard (Refer to Photos 25, 26 and 27). The buildings are reportedly used to warehouse lumber and equipment. However, the survey was not conducted inside any of the structures since Mr. Teneyck did not have the keys for door locks.

Mr. Teneyck indicated no solvents had been used at the site during present or past operations. However, wood preservatives had been used. Mr. Teneyck also indicated that years ago, a private contractor had been hired to spread dust inhibiting agents at the site. The composition of the dust inhibitors is reportedly not known. According to Mr. Teneyck, no surface or below ground tanks are present at the site.

During the site survey, oil stained sawdust was observed inside a pit located in the floor of the former factory (Photo 28). A can of discarded cutting oil was also noted near Monitoring Well MW10 (EPA10). Several unlabeled discarded drums were noted along the north side of the gray frame building. Stained soils have been reported during previous investigations (Johnson, 1985).
#### 3.0 FACILITIES SUBSEQUENTLY INCLUDED IN THE SURVEY

The following are other facilities which information was gathered as part of the survey.

#### 3.1 DON FITZGERALD CLEANERS AND TAILORS - 1006 SIXTH STREET

Based on previous industrial surveys, Don Fitzgerald Cleaners and Tailors has been identified as a user of halogenated solvents. This facility is located approximately 1500 feet southeast of Municipal Well CW4. Previous interviews with Mr. Don Fitzgerald (owner) indicate the dry cleaning operations use approximately 50 gallons per month of PCE. Prior to 1984, liquid waste from the facility was disposed to the sanitary sewer system via drains and toilets. Waste solvents generated during dry cleaning operations are currently transported to Wausau Camelot Cleaners for recycling (sparging).

#### 3.2 SENIC SIGN COMPANY - 1502 FIRST AVENUE

The Senic Sign Company (see Drawing 13076-B10) has also been identified as a local user of paint thinners, and solvents. WDNR records indicate this facility is classified as a very small quantity generator of hazardous wastes. The wastes are considered hazardous due to the igniteable characteristics of lacquer thinners and mineral spirits used and stored on site. The company also uses a wide variety of paints, paint thinners, solvents and screenprinting chemicals. Inventory forms supplied to WDNR indicate delivery of bulk solvents (LAC-SOLV 300) from Wausau Chemical to Senic Sign. Liquid wastes are generally collected in 55 gallon drums that are disposed by either Rock Refining or Lloyd Brothers trucking.

#### 3.3 CORNERSTONE FURNITURE - 1310 CHERRY STREET

Cornerstone Furniture located at 1310 Cherry Street (see Drawing 13076-B10) was not included in the August 6 and 7, 1987 Survey but was subsequently contacted regarding facility operations. The owner of this facility indicated

April 22, 1988

operations consisted of furniture design, construction and antique restoration. He was not aware of the use of PCE or TCE at his facility but indicated Dimethylene Chloride was frequently used as a paint and varnish remover.

#### 3.4 CAMELOT CLEANERS - 1902 NORTH SIXTH

Camelot Cleaners located at 1902 N. 6th Street (corner of Lincoln and 6th) is a potential user of chlorinated solvents. This company performs a variety of dry cleaning operations on site. The company is located approximately 1500 feet upgradient (east) of Municipal Wells CW4 and CW3.

#### 3.5 FORMER CITY LANDFILL

During the course of Phase I field activities, the abandoned City of Wausau landfill was identified as a potential source of VOC contamination. Two former city employees who were familiar with landfilling practices were interviewed on December 9, 1987. The interview included the following persons:

Margaret Guerriero - U.S. EPA Project Officer Craig Rawlinson - Warzyn Project Hydrogeologist David Cook - Wausau City Engineer James Lonsdorf - Special Council for the City of Wausau Ervin Sigmund - Former Landfill Employee Heimrich Oswald - Former Landfill Employee

According to Mr. Sigmund and Mr. Oswald;

• The City landfill occupied a former sand and gravel pit located on the west bank of the Wisconsin River. The landfill covered approximately two acres, underlying the southeastern portion of Marathon Electric property (Refer to Drawing 13076-B10). The former landfill extended from the present Marathon Electric Main entrance road, to the electric substation. The landfill was bounded on the east by the Wisconsin River, and to the west by the former gravel pit excavation face which extended south from the present Marathon Electric shipping area. The information was obtained from review of aerial photographs at the City of Wausau, Department of Engineering.

- The landfill operated from approximately 1948 to 1955 and was the only landfill within the City of Wausau at the time. During its period of operation almost all commercial, industrial and residential wastes generated within the city was disposed at the site. Both Mr. Sigmund and Mr. Oswald indicated that no effort was made to control the type of waste accepted at the landfill. Mr. Oswald recalled several instances when bulk liquid wastes contained in 55 gallon drums were emptied directly into the fill. He could not recall the specific generator(s) of the wastes, but indicated the practice was fairly common.
- The landfilling began in the northwest portion of the sand and gravel pit and progressed south and east. A rock crusher was located near the northeast portion of the gravel pit. Crushed rock and construction debris was generally filled into the northeast portion of the sand and gravel pit. Mr. Oswald and Mr. Sigmund indicated waste was often burned in order to conserve space. Ash and cinders were disposed throughout the landfill. Mr. Sigmund recalled burning several loads of dry cleaning rags and lint soaked with a flammable liquid.
- In many cases incineration could not keep pace with the amount of waste received in a day. In such instances, waste materials were landfilled directly. Such materials were generally filled into the western portion of the former sand and gravel pit. Mr. Oswald stated drums of unknown industrial wastes were also filled into the western portion of the landfill.
- The landfill was not generally fenced or secured, allowing waste disposal to occur during nonworking hours and weekends. Mr. Oswald also indicated landfill users were charged one bulk disposal rate regardless of the size of the load or the contents. Therefore, it is difficult to characterize waste types or volumes disposed at the landfill.

April 22, 1988

- The landfill base grades were controlled by pre-existing sand and gravel operations. Generally, the deepest filled areas were located in the eastern portion of the landfill, where sand and gravel operations had excavated to within a few feet of river level. Mr. Oswald indicated that approximately 40 feet of waste materials were disposed near the west bank of the Wisconsin River. The base of the landfill sloped upward toward the west in a slightly concave manner.
- Low lying areas west of the sand and gravel pit were filled by Marathon Electric and the American Toothpick Company. Wastes reportedly disposed in this area included moldings and foundry wastes. Most of the landfilled areas were sold by the City of Wausau to Marathon Electric in 1965. The land was used for plant expansion and additional parking. Excavations conducted during the construction of the Marathon Electric Foundry reportedly encountered drummed wastes beneath the eastern portion of the foundry (Walter Matson, personal communication).
- According to Mr. Oswald and Mr. Sigmund, the former City landfill extended as far south as the present Marathon Electric substation (Refer to Drawing 13076-B10). Fill materials observed along the river bank south of Marathon Electric may have been filled by an unknown party subsequent to the closure of the City portion of the landfill in 1955.

#### 4.0 SUMMARY AND RECOMMENDATIONS

A total of eight businesses were field surveyed August 6 and 7, 1987. Subsequent to that time 5 other facilities/entities were added to the Survey for consideration. Based on information obtained from the Survey, the following facilities were investigated in varying degree during the Phase I field investigation:

- Senic Sign Company
  - Camelot Cleaners
  - Former City Landfill

.

Based on the results of the Phase I field work, it is recommended that further investigations continue at the former City landfill site.

CSR/mm1/DLI [wpmisc-104-58]



#### TABLE 1

#### MARATHON ELECTRIC OPERATIONAL PROCESSES\*

SERVICE DEPARTMENT - Trichloroethylene wire stripping to remove varnish from stator wires to facilitate easy removal

STOCK ROOM - Plating Room - zinc - cadmium plating of small parts.

ROTOR DEPARTMENT - Etch Tanks - Etching of aluminum rotors with a caustic bath and then an acid rinse.

Selas Burner - Gas fired heater with water quench for rotors.

PUNCH PRESS - Annealing Ovens - Heat treating of lamination steel.

DIE CAST - Aluminum melting - coreplating using coreplate material.

SMALL WINDING - Stator Varnishing - Varnishing and baking of stators.

BODY DEPARTMENT - Wash Tanks - Washes motor parts prior to painting. Paint Over - Dips and bakes motor parts in enamel paint and bakes in oven. Welding Booths - Welding of small motor frames using arc, inert gas welding.

SHAFT DEPARTMENT - Turning and grinding of small shafts using various coolants.

L.G. SHAFT & ROTOR - Turning and grinding of large shafts using coolants. Insulation Cutting - Cutting of fiberglass boards with saws and a grinder. Welding - Welding and braising of rotors.

FOUNDRY - Induction Furnace - Used to melt gray iron. Muller - Used to mix sand for molding. Pangborn - Dust collector.

BRACKET - Machining of cast iron motor parts.

ASSEMBLY - Assembly of small motors. Paint Booth - Spray painting of motors.

SWITCH DEPARTMENT - Assembly of switch panels, rotor exciters, cutting of insulation for motors.

LG MOTOR & GENERATOR ASSEMBLY - Paint Booths - Painting motors and generators.

MEDIUM INTEGRAL WINDING - Bake Oven - Baking varnish on stators.

LG WINDING - Bake Ovens - Baking varnish on stators.

MEDIUM INTEGRAL ASSEMBLY - Paint Booth - Spray painting of motors.

\* Source WDNR 1982 Plant Survey

[wpmisc-104-57]

MARATHON ELECTRIC CHEMICAL AND RAW MATERIAL U	<u>SAGE IN 1974</u> *
Desmutter acid deoxidizer	4,450#
Kenbrite Salts B1	8,800#
Kenvert #12 chromate	1,600#
BZ100A Cleaner	5,200#
Vortesal XE-3500 Cleaner	2,400#
Kenbrite Enveloper	185 gal
Kenbrite Regulator	200 gal
Compound Metalline F-5500	110 gal
Muriatic Acid 130#	465 gal
Trichloroethylene	770 gal
Napthrol Spirits	220 gal
Paint Stripper	110 gal
Blacking Salts (5-1/4 oz K, 3# NaOH, 5-1/2 oz NaNO2)	100#
Boric Acid Powder	300#
Ammonia	575 gal
Nitric Acid	54 gal
Phosphoric Acid	20 gal
Aluminum Etch Compound	7,900#
Mineral Spirits	110 gal
Ethyl Alcohol	2 gal
Butyl Cellosolve	410#
Methyl Cellosolve Isopropawal Toluene	15 gal
Xylol	21,500 gal
Cimplus 48A	715 gal
CX 305 Cimcool	110 gal
Die Slick	25 gal
Filstone M-28 Lube	25 gal
Kleno Bowel	14 gal
West Power	24 gal
West Solv #30 Solvent	110 gal
West Foam Concentrate	4 gal
#43 West Lake Solvent	110 gal

\* Data based on WDNR Industrial Survey (December 3, 1975).

## TABLE 2

Marathon Electric Chemical and Raw Material Usage in 1974 Page 2

# <u>01LS</u>

Mobil Met 33	770 gal
Del Vac	330 gal
DTE 24	4,620 gal
Velocite #10	20 gal
Vactra #3	340 gal
DTE 103	280 gal
Vactra #1	210 gal
DTE #26	1,850 gal
Mobil Met #305	10,000 gal
Compound BB	2,035 gal
Pyrogard #53	385 gal
Mobil Fluid 220	550 gal
Delvac 1230	220 gal
Mobil 1220	275 gal
Nyvac FR200	220 gal
DTE Extra Heavy	220 gal
Solvac 500	55 gal
Vacmul UB-78	5,000 gal

# <u>PAINTS</u>

BK-259 Black Paint	440 gal
A95 Red Enamel	50 gal
A54 White Enamel	75 gal
A98 Blue Enamel	50 gal
A101 Red Lacquer	35 gal
Grey Lacquer	75 gal
#655 Epoxy Reducer	12 gal
Gray Epoxy Paint	12 gal
Gray Spray Enamel	3,500 gal
Gray Aquazen Primer	5,500 gal
Stabilizer	100 gal
Gray Dip & Bake Enamel	3,960 gal

Marathon Electric Chemical and Raw Material Usage in 1974 Page 3  $\,$ 

## VARNISHES

.

Isonel Varnish #31 Isonel Varnish Red Varnish

4,400 gal 22,000 gal 160 gal

### RAW MATERIALS

Aluminum	1,574,844#
Steel	19,961,176#
Cast Iron	12,551,800#
Copper Wire	16,256,488#

## FOUNDRY SUPPLIES

Molding Sand	538 tons
Core Sand	1,680 tons
Part rite Liquid	1,045 gal
Core Oil CWC-G	825 gal
Sand Conditioning Oil	1,705 gal
Liquid Pyrokote 2 Core Wash	580 gal
Fast Lite Solvent	605 gal
Core Binder	4,455 gal
Graphite Core Wash	65 gal
Carbon Riser	27,000#
Additrol ME-W-2 Blend	340 tons
SMZ 12M X 32M	7 tons
Carbo Carbo Sil 50	280 tons
Sodium Silicate	28 gal
Asbestos Sheets 42" X 46" X 5/32"	108 sheets
Isomica Sheets 36" X 36" X .0153	20 sheets

13076.21 CSR/mml/ [mml-400-01]

# INDUSTRIAL SURVEY PHOTOGRAPHS



View of east side of Wausau Energy Building. Building is currently leased by Marathon Press and is used for storage of printing materials.

> Wausau Energy 2112 2nd Street





South side of Wausau Energy where former Rush Distributing/Amoco Bulk Storage tanks were located. Foth and Van Dyke monitoring wells TB-2 and TB-5 visible in foreground.



### Photo 3

West side of Wausau Energy. Railroad spur located in foreground.

Wausau Energy 2102 2nd Street







View of south side of Steel Flite Scaffolding



## Photo 5

South side of Steel Flite Scaffolding and additional storage building in background.

Steel Flite Scaffolding 2308 N. Third Street



Photo 6

Loading docks and transport staging area. View looking east. Drum storage area located on concrete pad at right of photo.

> Marathon Press Park Avenue and Second



13076.21

13076.21



### Photo 7

Northwest portion of Marathon Press printing, graphics and office building. View looking east across Second Street.

Marathon Press Park Avenue and Second





Wergin Construction office and storage building. View looking northeast.



Photo 9

Wergin Construction maintenance garage. View looking northeast.

Wergin Construction 200 E. Wausau Avenue



13076.21





010 10

Wergin Construction storage area located west of C.M. ST P&P Railroad, north of E. Wausau Avenue.

### Photo 11

Wergin Construction pump island. Underground storage tanks containing regular, unleaded and diesel are located immediately east (right) of the pump island. Municipal well CW-3 is visible (metal frame building just left of small brick building) in background.

> Wergin Construction 200 East Wausau Avenue





Former Pure Oil Bulk facility. Property currently owned by Wausau Chemical. Vertical tanks used for calcium chloride storage located in background. Photo looking south across E. Wausau Avenue.

> Wausau Chemical 2001 N. River Drive





Empty drum storage area located east of Wausau Chemical building. View looking north from former bulk storage tank retainment area. Empty bulk storage tanks visible at right of photo.



Photo 14

Vertical tanks formerly used for PCE storage. Large tanks in background were removed from south side of building after the December 19, 1983 spill. Tanks located in foreground are similar to the tank that ruptured during the February 1983 spill.

Wausau Chemical Company 2001 N. River Drive



13076.21



Wausau Chemical PCE extraction system. PVC extraction wells located in foreground, air stripper located at right center of photo. View looking northeast from filtration plant.



#### Photo 16

Wausau Chemical northwest loading dock, in vicinity of the February 1983 PCE release. Photo view looking east from N. River Drive.

Wausau Chemical Company 2001 N. River Drive





Marathon Electric foundry/fabrication building. View looking southeast from main entrance.



Photo 18

Marathon Electric assembly building and former foundry building (at far right). View looking northeast from main entrance.

Marathon Electric 100 East Randolph





Marathon Electric painting and final assembly areas. Shipping located at right of building. View looking east from main entrance.



### Photo 20

Marathon Electric hazardous waste storage building, located south of foundary. View looking toward southwest.

Marathon Electric 100 East Randolph





20,000 gallon xylene tank riser pipe. The tank is located on the north side of the Marathon Electric assembly building. Photo view looking north, Randolph Street in background.



#### Photo 22

Marathon Electric cafeteria, located on north side of assembly building. Several underground storage tanks were removed during the construction of the cafeteria in 1982.

Marathon Electric 100 East Randolph





Former Marathon Box Plant location. View looking southeast. Plant was razed and relocated in 1982.



Photo 24

Existing portion of Marathon Box Plant. View looking north.

Marathon Box 207 N. First





Marathon Box storage building. View looking northeast from main entrance.



### Photo 26

Marathon Box storage building. Miscellaneous debris including pallets, drums and scrap metal in foreground.

Marathon Box 207 N. First





Marathon Box storage yard. View looking north from main entrance.



Photo 28

Pit containing oil stained sawdust.

Marathon Box 207 N. First

