



February 14, 1997

Mr. James R. Reyburn
Wisconsin Department of Natural Resources
1125 North Military Avenue
P.O. Box 10448
Green Bay, Wisconsin 54307-0448

RECEIVED
FEB 18 1997
LMD SOLID WASTE

Re: Results of Surface Water Modeling for the C.D. Besadny Wildlife Area, Kewaunee,
Wisconsin -- STS Project No. 20716XA

Dear Jim,

Enclosed are the results of surface water modeling conducted by STS Consultants, Ltd., for the above-referenced site. Results indicate downstream arsenic concentrations in the Kewaunee River are not likely to exceed Wisconsin Administrative Code NR 105 Human Cancer Criteria Standard of 50 micrograms per liter. We would appreciate it if you would circulate this information for review and comment. Following your review, we would like to set up a meeting to discuss this project.

Please call Mike Berger at 414-468-1978 if you have any questions or comments.

Sincerely,

STS CONSULTANTS LTD.

Rodney A. Hamilton, P.E.
Project Engineer

Michael T. Berger, R.M., CHMM
Microbiologist

Mark A. Bergeon, P.G.
Associate

RAH/tjl.wd

STS Consultants Ltd.
Consulting Engineers

1035 Kepler Drive
Green Bay, Wisconsin 54311
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Wisconsin Department of Natural Resources
STS Project No. 20716XA
February 14, 1997
Page 2

Copy to: Mr. Thomas P. McElligott
Quarles & Brady
411 East Wisconsin Avenue
Milwaukee, Wisconsin 53202-4497

(C416A011)

Report

PROJECT

RESULTS OF SURFACE WATER MODELING
C.D. BESADNY WILDLIFE AREA
KEWAUNEE, WISCONSIN

Project No.

20716XA

Date

FEBRUARY 1997



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Appendix C	Hydrocad Runoff Model Printouts

**RESULTS OF SURFACE WATER MODELING
C.D. BESADNY WILDLIFE AREA
KEWAUNEE, WISCONSIN
STS PROJECT NO. 20716XA -- FEBRUARY 1997**

1.0 INTRODUCTION

To determine potential arsenic loading into the Kewaunee River due to surface water transport, surface water modeling was conducted. In addition, results of both surface water modeling and preliminary groundwater modeling conducted by GeoTrans, Inc., were used to determine total potential arsenic loading into the Kewaunee River.

1.1 Surface Water Modeling

For purposes of surface water modeling, the fenced area at the site was broken into three subareas. The "Stormwater Modeling System HYDROCAD" was used to analyze the Kewaunee Marsh watersheds. This model is based on the Soil Conservation Service (SCS) Technical Release 20 Methodology and generates synthetic flood hydrographs identical to the U.S. Army Corps of Engineers HEC-1 computer model. The HYDROCAD model simulates watershed response to precipitation by representing the drainage basins as a system of interconnected hydrologic and hydraulic components. Typical input parameters to the program include basin area, overland flow travel time, soil permeability, soil infiltration relationships, land use characteristics, precipitation amounts, distribution, and base flow. See Appendix A, Figure 1 for Stormwater Runoff Model Site Map. The following table summarizes hydraulic parameters used to model surface water runoff from the site.

TABLE 1
HYDRAULIC PARAMETERS

<u>Subarea</u>	<u>Area (acres)</u>	<u>SCS Curve Number</u>
1 (north)	6.50	83
2 (center)	4.57	86
3 (south)	3.10	83

See Appendix B for a summary of hydraulic parameters used in the surface water runoff model.

1.2 Arsenic Water Balance

A water balance was conducted using the total stormwater runoff, groundwater transport, and recorded flow in the Kewaunee River. Kewaunee River flow data were obtained from the U. S. Geological Survey (U.S.G.S.) Water Resources Investigations, Open-File Report 91-4128 Flood-Frequency Characteristics of Wisconsin Streams (see Appendix B). Groundwater transport was determined from groundwater modeling conducted by GeoTrans, Inc.

Three scenarios were used to estimate potential arsenic concentrations. In each scenario, the conservative assumption was made that all surface water runoff which comes in contact with the marsh will transport the total arsenic concentration. The three water balance scenarios included:

1. Surface water runoff concentrations equal to the maximum observed marsh surface water arsenic concentration within each subarea
2. Surface water runoff concentrations equal to the average observed marsh surface water arsenic concentrations within each subarea

3. Using a mean river water arsenic concentration as observed immediately adjacent to the site to back-calculate the potential marsh surface water arsenic concentration

The following table summarizes marsh surface water arsenic concentrations used in the three scenarios.

TABLE 2
ARSENIC CONCENTRATIONS

<u>Subarea</u>	<u>Sample No.</u>	<u>Arsenic Concentration (µg/l)</u>
1 (north)	SW03-01 (WDNR)	360
	SW05-01 (WDNR)	76
	SW06-01 (WDNR)	60
	SW07-01 (WDNR)	110
2 (center)	Impacted area covered with compacted wood chips assume arsenic concentration	0 (assumed)
3 (south)	SW08-01 (WDNR)	4.6
	H-6 (STS)	19,100
River	River Water Sample (adjacent to site)	3.5
	Upstream Arsenic Concentration	0 (assumed)

Note: µg/l - micrograms per liter

The following tables summarize scenario results and calculated downstream arsenic concentrations.

TABLE 3
 MAXIMUM ARSENIC CONCENTRATION WATER BALANCE *

Rainfall Event Return Period (year)	Type II' 24-Hour Rainfall (inches)	Kewaunee River Upstream		Kewaunee Marsh Surface Water		Kewaunee Marsh Groundwater		Kewaunee River (downstream)	
		Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)
2	2.4	2,700	0	5.6	4,442.3	0.00009	300,000.0	2,705.6	9.1
5	3.2	4,370	0	9.2	4,522.5	0.00009	300,000.0	4,379.2	9.5
10	3.7	5,490	0	11.6	4,554.0	0.00009	300,000.0	5,501.6	9.6
25	4.2	6,880	0	14.1	4,572.7	0.00009	300,000.0	6,894.1	9.3
50	4.7	7,870	0	16.6	4,595.5	0.00009	300,000.0	7,906.6	9.6
100	5.0	8,870	0	18.1	4,605.1	0.00009	300,000.0	8,888.1	9.4

1 - A Type II, 24-hour rainfall is a national weather service designation which represents the duration-frequency of rainfall events in the Midwest.

* See Appendix B for sample calculations.

TABLE 4
 AVERAGE SURFACE WATER ARSENIC CONCENTRATION WATER BALANCE *

Rainfall Event Return Period (year)	Type II 24-Hour Rainfall (inches)	Kewaunee River Upstream		Kewaunee Marsh Surface Water		Kewaunee Marsh Groundwater		Kewaunee River (downstream)	
		Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)
2	2.4	2,700	0	5.6	2,210.3	0.00009	300,000.0	2,705.6	4.6
5	3.2	4,370	0	9.2	2,250.2	0.00009	300,000.0	4,379.2	4.7
10	3.7	5,490	0	11.6	2,265.8	0.00009	300,000.0	5,501.6	4.8
25	4.2	6,880	0	14.1	2,275.1	0.00009	300,000.0	6,894.1	4.6
50	4.7	7,870	0	16.6	2,286.5	0.00009	300,000.0	7,906.6	4.8
100	5.0	8,870	0	18.1	2,291.3	0.00009	300,000.0	8,888.1	4.7

* See Appendix B for sample calculations.

TABLE 5

**PROBABLE SURFACE WATER ARSENIC CONCENTRATION AS BACK-CALCULATED
 FROM OBSERVED RIVER WATER CONCENTRATIONS ADJACENT TO
 KEWAUNEE MARSH ***

Rainfall Event Return Period (year)	Type II 24-Hour Rainfall (inches)	Kewaunee River (downstream)		Kewaunee Marsh Groundwater		Kewaunee River Upstream		Calculated Kewaunee Marsh Surface Water	
		Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)	Flow (cfs)	As Conc. (µg/l)
2	2.4	2,705.6	3.5	0.00009	300,000.0	2,700	0	5.6	1,698.2
5	3.2	4,379.2	3.5	0.00009	300,000.0	4,370	0	9.2	1,659.4
10	3.7	5,501.6	3.5	0.00009	300,000.0	5,490	0	11.6	1,653.3
25	4.2	6,894.1	3.5	0.00009	300,000.0	6,880	0	14.1	1,710.6
50	4.7	7,906.6	3.5	0.00009	300,000.0	7,870	0	16.6	1,665.4
100	5.0	8,888.1	3.5	0.00009	300,000.0	8,870	0	18.1	1,716.2

* See Appendix B for sample calculations.

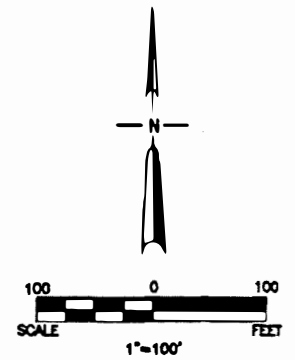
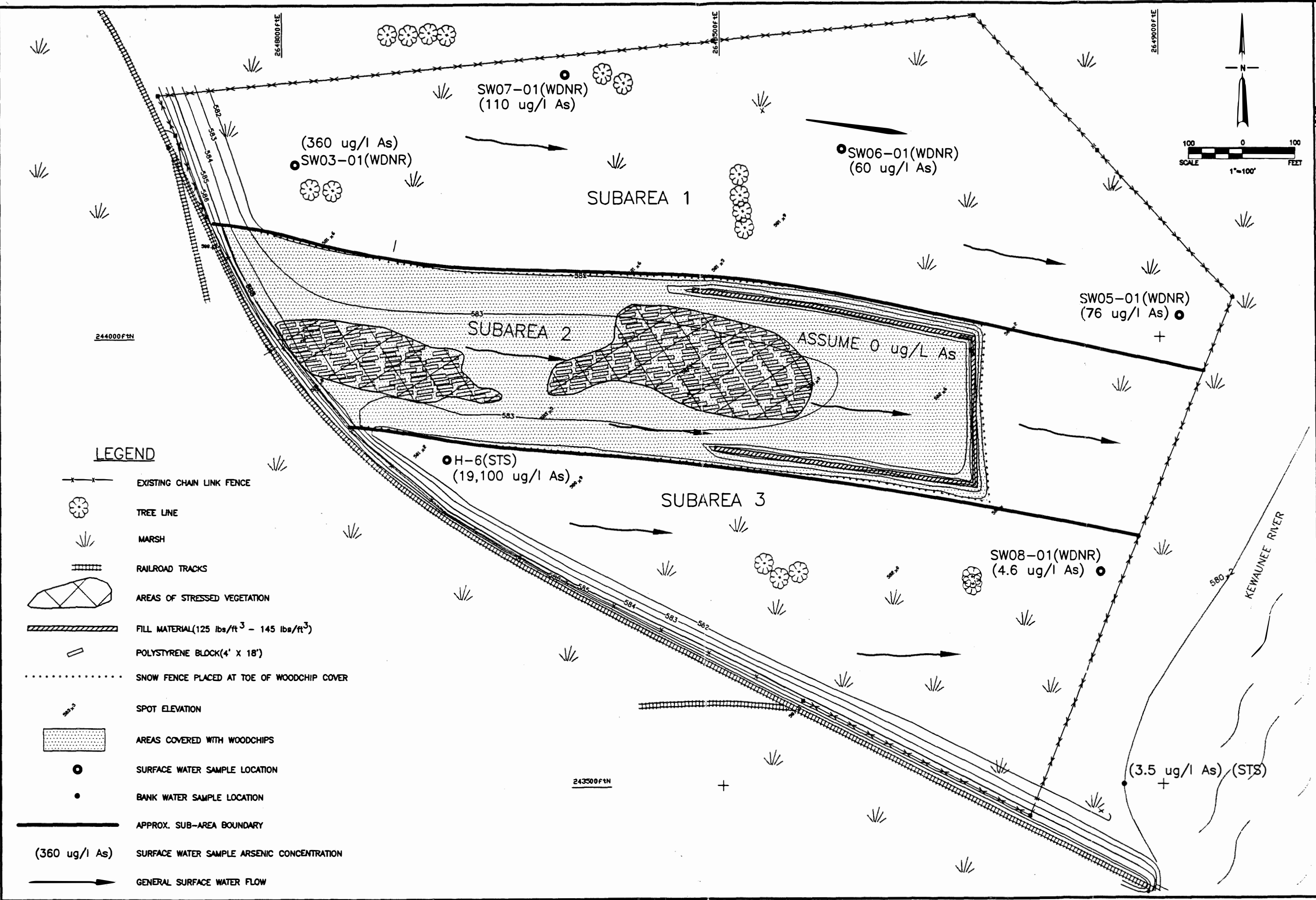
Note: See Appendix B for Kewaunee Marsh groundwater flow calculations and spreadsheet calculations used to develop Tables 3, 4, and 5.

2.0 CONCLUSIONS

Based on average marsh arsenic concentrations from surface water data and modeled maximum arsenic groundwater discharge concentrations, the potential maximum downstream arsenic concentration in the Kewaunee River was calculated to be 4.8 µg/l. Based on maximum marsh arsenic concentrations from surface water data and modeled maximum arsenic groundwater discharge concentrations, the potential maximum downstream arsenic concentration in the Kewaunee River was calculated to be 9.6 µg/L. Both calculated concentrations are comparable to concentrations measured in water samples collected from the Kewaunee River adjacent to the site. Calculated concentrations are below the Wisconsin Administrative Code NR 105 Human Cancer Criteria Standard of 50 µg/L. Results of hydraulic modeling indicate that arsenic transported to the Kewaunee River should not exceed surface water standards.

APPENDIX A

Stormwater Runoff Model Site Map



DATE	11-26-96
DRAWN BY	P.D.P.
CHECKED BY	R.A.H.
APPROVED BY	
DATE	2-4-97
DATE	
DATE	
CAD FILE	W:\DWG96\20716\XF\G416A001.DWG

KEWAUNEE MARSH ARSENIC SITE
KEWAUNEE, WISCONSIN
STORM WATER RUNOFF MODEL SITE MAP



STS PROJECT NO.	20716XA
STS PROJECT FILE	
SCALE	1" = 100'
SHEET NO.	FIGURE 1

LEGEND

- EXISTING CHAIN LINK FENCE
- TREE LINE
- MARSH
- RAILROAD TRACKS
- AREAS OF STRESSED VEGETATION
- FILL MATERIAL (125 lbs/ft³ - 145 lbs/ft³)
- POLYSTYRENE BLOCK (4' X 18')
- SNOW FENCE PLACED AT TOE OF WOODCHIP COVER
- SPOT ELEVATION
- AREAS COVERED WITH WOODCHIPS
- SURFACE WATER SAMPLE LOCATION
- BANK WATER SAMPLE LOCATION
- APPROX. SUB-AREA BOUNDARY
- (360 ug/l As) SURFACE WATER SAMPLE ARSENIC CONCENTRATION
- GENERAL SURFACE WATER FLOW

APPENDIX B

Flow Calculation Spreadsheets

Hydraulic Parameters

Kewaunee River Flow Data

Groundwater Discharge Data

Arsenic Concentrations

Sample Calculations

GeoTrans, Inc., Preliminary Results of Groundwater Modeling

Water Balance Using Maximum Observed Surface Water Arsenic Concentrations From Marsh

Kewaunee Marsh Flow Calculations											
	Volume (acre-feet)			Volume (gallons)			Peak Discharge (cfs)				
Storm (yr)	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Total	
2	0.47	0.39	0.22	153,144	127,077	71,684	2.29	2.02	1.25	5.56	
5	0.77	0.62	0.37	250,895	202,020	120,560	3.88	3.23	2.11	9.22	
10	0.98	0.77	0.47	319,321	250,895	153,144	4.93	4.02	2.68	11.63	
25	1.19	0.93	0.57	387,747	303,029	185,728	6.01	4.82	3.26	14.09	
50	1.4	1.08	0.67	456,173	351,905	218,311	7.11	5.63	3.86	16.60	
100	1.53	1.17	0.73	498,532	381,230	237,862	7.77	6.12	4.22	18.11	
Summary											
Rainfall Event		Kewaunee River (down stream)									
(year)		Flow	As Conc.								
		(cfs)	(ug/l)								
2		2,705.6	9.1								
5		4,379.2	9.5								
10		5,501.6	9.6								
25		6,894.1	9.3								
50		7,906.6	9.6								
100		8,888.1	9.4								

Water Balance Using Maximum Observed Surface Water Arsenic Concentrations From Marsh

Maximum Surface Water As Conc (ug/l)			As Conc Flowing from Marsh (ug/l)									
Area 1	Area 2	Area 3										
360	0	19,100			4,442.3							
360	0	19,100			4,522.5							
360	0	19,100			4,554.0							
360	0	19,100			4,572.7							
360	0	19,100			4,595.5							
360	0	19,100			4,605.1							

Water Balance Using Maximum Observed Surface Water Arsenic Concentrations From Marsh

Rainfall Event (year)	Kewaunee River Upstream		Kewaunee Marsh		Kewaunee Marsh Ground Water		Kewaunee River (down stream)	
	Flow	As Conc.	Flow	As Conc.	Flow	As. Conc.	Flow	As Conc.
	(cfs)	(ug/l)	(cfs)	(ug/l)	(cfs)	(ug/l)	(cfs)	(ug/l)
2	2,700	0	5.6	4,442.3	0.00009	300,000	2,705.6	9.1
5	4,370	0	9.2	4,522.5	0.00009	300,000	4,379.2	9.5
10	5,490	0	11.6	4,554.0	0.00009	300,000	5,501.6	9.6
25	6,880	0	14.1	4,572.7	0.00009	300,000	6,894.1	9.3
50	7,890	0	16.6	4,595.5	0.00009	300,000	7,906.6	9.6
100	8,870	0	18.1	4,605.1	0.00009	300,000	8,888.1	9.4

Water Balance Using Average Observed Surface Water Arsenic Concentrations in Marsh

Kewaunee Marsh Flow Calculations												
	Volume (acre-feet)			Volume (gallons)			Peak Discharge (cfs)					
Storm (yr)	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Total		
2	0.47	0.39	0.22	153,144	127,077	71,684	2.29	2.02	1.25	5.56		
5	0.77	0.62	0.37	250,895	202,020	120,560	3.88	3.23	2.11	9.22		
10	0.98	0.77	0.47	319,321	250,895	153,144	4.93	4.02	2.68	11.63		
25	1.19	0.93	0.57	387,747	303,029	185,728	6.01	4.82	3.26	14.09		
50	1.4	1.08	0.67	456,173	351,905	218,311	7.11	5.63	3.86	16.60		
100	1.53	1.17	0.73	498,532	381,230	237,862	7.77	6.12	4.22	18.11		
Summary												
Rainfall Event		Kewaunee River (down stream)										
(years)		Flow (cfs)	As Conc. (ug/l)									
2		2,705.6	4.6									
5		4,379.2	4.7									
10		5,501.6	4.8									
25		6,894.1	4.6									
50		7,906.6	4.8									
100		8,888.1	4.7									

Water Balance Using Average Observed Surface Water Arsenic Concentrations In Marsh

Average Surface Water As Conc (ug/l)			As Conc Flowing from Marsh (ug/l)								
Area 1	Area 2	Area 3									
152	0	9,553		2,210.3							
152	0	9,553		2,250.2							
152	0	9,553		2,265.8							
152	0	9,553		2,275.1							
152	0	9,553		2,286.5							
152	0	9,553		2,291.3							

Water Balance Using Average Observed Surface Water Arsenic Concentrations in Marsh

Rainfall Event (years)	Kewaunee River Upstream			Kewaunee Marsh		Kewaunee Marsh Ground Water		Kewaunee River (down stream)	
	Flow (cfs)	As Conc. (ug/l)		Flow (cfs)	As Conc. (ug/l)	Flow (cfs)	As. Conc. (ug/l)	Flow (cfs)	As Conc. (ug/l)
2	2,700	0		5.6	2,210.3	0.00009	300,000	2,705.6	4.6
5	4,370	0		9.2	2,250.2	0.00009	300,000	4,379.2	4.7
10	5,490	0		11.6	2,265.8	0.00009	300,000	5,501.6	4.8
25	6,880	0		14.1	2,275.1	0.00009	300,000	6,894.1	4.6
50	7,890	0		16.6	2,286.5	0.00009	300,000	7,906.6	4.8
100	8,870	0		18.1	2,291.3	0.00009	300,000	8,888.1	4.7

Water Balance Using Observed River Water Arsenic Concentration To Back Calculate Probable Surface Water Arsenic Concentration In Marsh

Kewaunee Marsh Flow Calculations												
	Volume (acre-feet)			Volume (gallons)			Peak Discharge (cfs)					
Storm (yr)	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Area 1	Area 2	Area 3	Total		
2	0.47	0.39	0.22	153,144	127,077	71,684	2.29	2.02	1.25	5.56		
5	0.77	0.62	0.37	250,895	202,020	120,560	3.88	3.23	2.11	9.22		
10	0.98	0.77	0.47	319,321	250,895	153,144	4.93	4.02	2.68	11.63		
25	1.19	0.93	0.57	387,747	303,029	185,728	6.01	4.82	3.26	14.09		
50	1.4	1.08	0.67	456,173	351,905	218,311	7.11	5.63	3.86	16.60		
100	1.53	1.17	0.73	498,532	381,230	237,862	7.77	6.12	4.22	18.11		
Summary												
Rainfall Event		Kewaunee Marsh Concentration										
(year)		Flow	Ar Conc.									
		(cfs)	(ug/l)									
2		5.6	1698.2									
5		9.2	1659.4									
10		11.6	1653.3									
25		14.1	1710.6									
50		16.6	1665.4									
100		18.1	1716.2									

Water Balance Using Observed River Water Arsenic Concentration To Back Calculate Probable Surface Water Arsenic Concentration in Marsh

	Average Surface Water As Conc			As Conc Flowing from Marsh						
	(ug/l)			(ug/l)						
	Area 1	Area 2	Area 3							
	152	0	9,553	2,210.3						
	152	0	9,553	2,250.2						
	152	0	9,553	2,265.8						
	152	0	9,553	2,275.1						
	152	0	9,553	2,286.5						
	152	0	9,553	2,291.3						

Water Balance Using Observed River Water Arsenic Concentration To Back Calculate Probable Surface Water Arsenic Concentration In Marsh

		Kewaunee Marsh			Kewaunee Marsh			Kewaunee Marsh				
Rainfall Event		Kewaunee River (down stream)			Ground Water		Kewaunee River Upstream			Kewaunee Marsh		
(year)		Flow	As Conc.		Flow	As Conc.	Flow	As Conc.		Flow	As Conc.	
		(cfs)	(ug/l)		(cfs)	(ug/l)	(cfs)	(ug/l)		(cfs)	(ug/l)	
2		2,705.6	3.5		0.00009	300,000	2,700	0		5.6	1,698.2	
5		4,379.2	3.5		0.00009	300,000	4,370	0		9.2	1,659.4	
10		5,501.6	3.5		0.00009	300,000	5,490	0		11.6	1,653.3	
25		6,894.1	3.5		0.00009	300,000	6,880	0		14.1	1,710.6	
50		7,906.6	3.5		0.00009	300,000	7,890	0		16.6	1,665.4	
100		8,888.1	3.5		0.00009	300,000	8,870	0		18.1	1,716.2	



STS Consultants Ltd.
CALCULATION SHEET

PROJECT KEWAUNEE MARSH		STS JOB NO.	
SUBJECT HYDROLOGIC PARAMETERS		SHEET NO.	
ORIGINATED BY RAH	DATE 12/9/96	CHECKED BY	DATE
		CALC. NO.	REV. NO.

<u>SUBAREA</u>	<u>AREA</u>	<u>SCS CURVE NUMBER</u>	<u>LENGTH</u>	<u>SLOPE</u>
1 (NORTH)	6.50 AC	83 ^①	1060'	0.001 FT/FT
2 (CENTRAL)	4.57 AC	86 ^②	L ₁ =780' L ₂ =225'	S ₁ =0.001 FT/FT S ₂ =0.001 FT/FT
3 (SOUTH)	3.10 AC	83 ^①	860'	S=0.001 FT/FT

① BRUSH/GRASS MIXTURE - POOR CURVE NUMBER = 83

② 79% OF AREA COMPACTED WOODCHIPS (CN = 87)
21% OF AREA BRUSH/GRASS MIXTURE (CN = 83)

PRECIP. VALUES FROM SCS TR-55

<u>RETURN PERIOD (YR)</u>	<u>TYPE II 24-HOUR RAINFALL (INCHES)</u>
2	2.4
5	3.2
10	3.7
25	4.2
50	4.7
100	5.0

Table 4. Flood discharges at selected recurrence intervals and WRC skew for gaging stations in Wisconsin--Continued

Station number	Station name	WRC skew	Discharge for indicated recurrence interval							SE ₁₀₀	Remarks ¹
			2	5	10	25	50	100			
04075200	Evergreen Creek near Langlade, Wis.	0.046	44.5	56.2	63.5	72.5	78.9	85.3	10.1		
04075500	Wolf River above West Branch Wolf River near Keshena, Wis.	.318	1,740	2,120	2,360	2,665	2,890	3,120	8.7		
04077000	Wolf River at Keshena Falls near Keshena, Wis.	.356	2,410	3,070	3,520	4,100	4,545	5,000	7.5		
04078500	Embarras River near Embarras, Wis.	-.070	2,340	3,460	4,235	5,240	6,000	6,780	10.8		
04079000	Wolf River at New London, Wis.	-.224	6,720	9,460	11,200	13,400	14,900	16,400	9.1		
04079700	Spaulding Creek near Big Falls, Wis.	.109	52.5	67.7	77.6	90.0	99.2	108	11.2		
04080000	Little Wolf River at Royalton, Wis.	-.522	3,195	4,850	5,880	7,095	7,930	8,715	10.7		
04081000	Waupaca River near Waupaca, Wis.	-.518	1,080	1,540	1,835	2,175	2,405	2,620	9.9		
04081010	Waupaca River tributary near Waupaca, Wis.	-.499	41.4	69.8	89.1	113	130	147	22.5		
04081900	Sawyer Creek at Oshkosh, Wis.	-.001	427	861	1,240	1,840	2,370	2,970	31.7		
		-.243	542	1,020	1,400	1,930	2,360	2,810	25.1	G	
04083000	West Branch Fond du Lac River at Fond du Lac, Wis.	-.700	760	1,140	1,370	1,620	1,780	1,930	20.1		
04083400	East Branch Fond du Lac River tributary near Eden, Wis.	-.416	57.6	96.6	123	158	183	207	23.1		
04083500	East Branch Fond du Lac River at Fond du Lac, Wis.	-.710	908	1,550	1,960	2,440	2,760	3,060	26.5		
04084500	Fox River at Rapide Croche Dam, near Wrightstown, Wis.	-.768	12,700	17,000	19,200	21,600	23,000	24,200	6.7	E	
04085030	Apple Creek near Kaukauna, Wis.	-.735	787	1,210	1,460	1,730	1,910	2,070	15.6		
04085100	East River tributary at Greenleaf, Wis.	-.162	216	379	504	678	818	965	25.8		
X 04085200	Kewaunee River near Kewaunee, Wis.	-.417	2,700	4,370	5,490	6,880	7,890	8,870	17.6	X	
04085281	East Twin River at Mishicot, Wis.	-.163	1,200	2,020	2,620	3,440	4,080	4,750	29.5		
04085300	Neahota River tributary near Denmark, Wis.	-.424	193	326	418	536	622	707	19.6		
04085400	Killbuck River near Chilton, Wis.	-.806	627	1,060	1,340	1,680	1,910	2,130	19.6		
04085427	Manitowoc River at Manitowoc, Wis.	-.154	2,590	4,270	5,510	7,170	8,470	9,820	27.7		
04085700	Sheboygan River tributary near Plymouth, Wis.	-.032	113	183	235	307	365	426	24.4		
04086000	Sheboygan River at Sheboygan, Wis.	-.655	3,140	5,000	6,150	7,480	8,380	9,200	13.6		
04086150	Milwaukee River at Kewaunee, Wis.	-.059	900	1,460	1,860	2,420	2,870	3,330	29.4		
04086200	East Branch Milwaukee River near New Fane, Wis.	-.137	214	352	455	593	702	815	31.1		
04086340	North Branch Milwaukee River near Fillmore, Wis.	-.266	789	1,380	1,820	2,420	2,880	3,360	33.5		
04086360	Milwaukee River at Waubesa, Wis.	-.391	2,110	3,530	4,520	5,770	6,710	7,630	28.6		
04086400	Milwaukee River tributary near Fredonia, Wis.	-.586	55.0	105	141	188	221	254	30.0		
04086500	Cedar Creek near Cedarburg, Wis.	-.189	951	1,860	2,600	3,670	4,570	5,530	20.1		
04087000	Milwaukee River at Milwaukee, Wis.	-.057	4,890	6,990	8,580	10,700	12,300	13,900	10.4		
04087030	Menomonee River at Menomonee Falls, Wis.	-.160	539	788	968	1,210	1,400	1,610	27.3		
04087050	Little Menomonee River near Freistadt, Wis.	-.446	182	272	328	395	441	485	14.5		
04087088	Underwood Creek at Wauwatosa, Wis.	-.298	857	1,430	1,840	2,370	2,780	3,180	34.8		
04087100	Honey Creek at Milwaukee, Wis.	-.035	319	488	609	769	894	1,020	17.7		
04087120	Menomonee River at Wauwatosa, Wis.	.023	3,400	5,870	7,430	9,920	12,000	14,100	23.1		
04087200	Oak Creek near South Milwaukee, Wis.	-.117	258	453	604	817	989	1,170	22.5		
04087204	Oak Creek at South Milwaukee, Wis.	.113	585	767	887	1,040	1,160	1,260	13.1		
04087220	Root River near Franklin, Wis.	.219	1,080	1,860	2,500	3,470	4,310	5,250	27.3		
04087230	West Branch Root River Canal tributary near North Cape, Wis.	-.603	89.4	133	180	190	210	228	15.2		
04087233	Root River Canal near Franklin, Wis.	-.274	709	975	1,140	1,340	1,480	1,810	13.5		
04087240	Root River at Racine, Wis.	-.032	1,940	2,760	3,300	4,000	4,530	5,070	16.0		
04087250	Pike Creek near Kenosha, Wis.	-.308	82.6	135	171	217	252	287	19.0		
04087257	Pike River near Racine, Wis.	-.453	878	1,180	1,350	1,540	1,870	1,790	16.8		
05332500	Namakagon River near Trago, Wis.	.573	1,170	1,620	1,960	2,440	2,830	3,260	12.8	E	
05333100	Little Frog Creek near Minong, Wis.	-.345	205	378	508	685	823	964	24.2		



STS Consultants Ltd.
CALCULATION SHEET

PROJECT KEWAUNEE MARSH				STS JOB NO.	
SUBJECT GROUND WATER DISCHARGE				SHEET NO.	
ORIGINATED BY	DATE	CHECKED BY	DATE	CALC. NO.	OF REV. NO.

FROM JAMES ERICKSON - GEOTRANS, INC.

$$\begin{aligned}
 \text{DARCY VELOCITY} &= 0.15 \text{ FT/YR} \quad (\text{AVERAGE VELOCITY OVER CROSS SECTIONAL AREA}) \\
 &= \left(0.15 \frac{\text{FT}}{\text{YR}} \left(\frac{1 \text{ YR}}{365 \text{ DAYS}}\right)\right) \left(\frac{1 \text{ DAY}}{24 \text{ HRS}}\right) \left(\frac{1 \text{ HR}}{60 \text{ MIN}}\right) \left(\frac{1 \text{ MIN}}{60 \text{ SEC}}\right) \\
 &= 4.756 \times 10^{-9} \text{ FT/SEC.}
 \end{aligned}$$

DARCY VELOCITY X CROSS-SECTIONAL AREA = TOTAL Q

LENGTH OF SITE ALONG RIVER = 960 FEET

DEPTH OF RIVER = 20 FEET

$$\therefore Q_{\text{CFS}} = 4.756 \times 10^{-9} \frac{\text{FT}}{\text{SEC}} \times (960 \text{ FT})(20 \text{ FT})$$

$$= 0.000091315 \text{ CFS}$$

$$Q = 9.1315 \times 10^{-5} \text{ CFS}$$



STS Consultants Ltd.
CALCULATION SHEET

PROJECT C.D. BESADNY WILDLIFE AREA		STS JOB NO. 20716XA	
SUBJECT SURFACE WATER A ₅ .		SHEET NO. 1 OF 1	
ORIGINATED BY RAH	DATE 12/6/96	CHECKED BY	DATE
CALC. NO.		REV. NO.	

SUBAREA	SAMPLE NO.	CONCENTRATION (ug/l)	
SUBAREA 1 (NORTH)	SW03-01 (WDNR)	360	→ MAXIMUM
	SW05-01 (WDNR)	76	
	SW06-01 (WDNR)	60	
	SW07-01 (WDNR)	110	
		AVERAGE = 152 ug/l	

SUBAREA 2
(CENTRAL)

FOR WATER BALANCE
SUBAREA A₅ CONCENTRATION
HAS BEEN ASSUMED 0.4g/l
FOR SURFACE WATER

SUBAREA 3
(SOUTH)

SW08-01 (WDNR)	4.6	
H-6 (STS)	19,100	→ MAXIMUM

AVERAGE = 9,553 ug/l

KEWAUNEE RIVER BANK WATER IMMEDIATELY DOWN STREAM OF MARSH → THE A₅ VALUE USED IS THE AVERAGE OF SAMPLES COLLECTED ON 8/12/96 & 10/23/96

• DOWN STREAM A₅ = 3.5 ug/l

• UPSTREAM A₅ = 0.4g/l (ASSUMED)



STS Consultants Ltd.
CALCULATION SHEET

PROJECT CD. BESADNY WILDLIFE AREA		STS JOB NO. 20746XA	
SUBJECT SAMPLE CALCULATIONS		SHEET NO. 1 OF	
ORIGINATED BY RAT	DATE 2/13/97	CHECKED BY	DATE
CALC. NO.		REV. NO.	

SAMPLE CALCULATIONS FOR ESTIMATING ARSENIC CONCENTRATIONS OF SURFACE WATER FLOWING FROM THE MARSH.

- FIRST TABLE IN APPENDIX B 2 YEAR STORM MAX. AS CONCENTRATIONS

$$\left[\begin{matrix} \text{AREA 1} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 1} \\ \text{AS CONC.} \\ \text{(MAX)} \end{matrix} \right] + \left[\begin{matrix} \text{AREA 2} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 2} \\ \text{AS CONC.} \\ \text{(MAX)} \end{matrix} \right] + \left[\begin{matrix} \text{AREA 3} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 3} \\ \text{AS CONC.} \\ \text{(MAX)} \end{matrix} \right] = \text{AS CONC. FLOWING FROM MARSH (MAX)}$$

TOTAL FLOW FROM MARSH

$$\left[(2.29 \text{ cfs} \times 360 \text{ ug/l}) + (2.02 \text{ cfs} \times 0.43 \text{ ug/l}) + (1.25 \text{ cfs} \times 19,100 \text{ ug/l}) \right] = 4,442.3 \text{ ug/l}$$

5.56 cfs

- SECOND TABLE IN APPENDIX B 2 YEAR STORM AVERAGE AS CONCENTRATIONS

$$\left[\begin{matrix} \text{AREA 1} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 1} \\ \text{AS CONC.} \\ \text{(AVE)} \end{matrix} \right] + \left[\begin{matrix} \text{AREA 2} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 2} \\ \text{AS CONC.} \\ \text{(AVE)} \end{matrix} \right] + \left[\begin{matrix} \text{AREA 3} \\ \text{FLOW} \end{matrix} \times \begin{matrix} \text{AREA 3} \\ \text{AS CONC.} \\ \text{(AVE)} \end{matrix} \right] = \text{AS CONC FLOWING FROM MARSH (AVE)}$$

TOTAL FLOW FROM MARSH

$$\left[(2.29 \text{ cfs} \times 152 \text{ ug/l}) + (2.02 \text{ cfs} \times 0.43 \text{ ug/l}) + (1.25 \text{ cfs} \times 9,553 \text{ ug/l}) \right] = 2,210.3 \text{ ug/l}$$

5.56 cfs

NOTE: AS CONCENTRATIONS IN SURFACE WATER DISCHARGE INCREASES AS FLOW INCREASE BECAUSE THE INCREASE OF SURFACE WATER FLOW FROM EACH SUBAREA IS NOT PROPORTIONAL AS THE YEAR OF THE EVENT STORM INCREASES



STS Consultants Ltd.
CALCULATION SHEET

PROJECT
C.D. BESADNY WILDLIFE AREA

STS JOB NO.
20716XA

SUBJECT
SAMPLE CALCULATIONS

SHEET NO.
1 OF 1

ORIGINATED BY
RAH

DATE
12/17/97

CHECKED BY

DATE

CALC. NO.

REV. NO.

THESE SAMPLE CALCULATION ARE USED TO DEVELOP TABLES 3 AND 4

EXAMPLE CALCULATION USES DATA FROM TABLE 3 AND A FIVE YEAR STORM EVENT

$$\textcircled{1} \left[\begin{array}{l} \text{KEWAUNEE RIVER} \\ \text{UPSTREAM FLOW} \end{array} \times A_s \text{ CONC.} \right] + \left[\begin{array}{l} \text{KEWAUNEE MARSH} \\ \text{SURFACE WATER FLOW} \end{array} \times A_s \text{ CONC.} \right] + \left[\begin{array}{l} \text{KEWAUNEE MARSH} \\ \text{GROUNDWATER FLOW} \end{array} \times A_s \text{ CONC.} \right] = \text{KEWAUNEE RIVER DOWN STREAM } A_s \text{ CONC.}$$

KEWAUNEE RIVER DOWN STREAM FLOW

$$\textcircled{2} \left[(4,370 \text{ cfs} \times 0.9 \text{ ug/l}) + (9.2 \text{ cfs} \times 4,522.5 \text{ ug/l}) + (0.00009 \text{ cfs} \times 300,000 \text{ ug/l}) \right] = 9.5 \text{ ug/l}$$

4,379.2 cfs

$$\textcircled{3} \text{ KEWAUNEE RIVER DOWN STREAM FLOW} = \text{KEWAUNEE RIVER UPSTREAM FLOW} + \text{KEWAUNEE MARSH SURFACE WATER FLOW} + \text{KEWAUNEE MARSH GROUND WATER FLOW}$$



STS Consultants Ltd.
CALCULATION SHEET

PROJECT C.D. BESADNY WILDLIFE AREA		STS JOB NO. 20716XA	
SUBJECT SAMPLE CALCULATIONS		SHEET NO. 1 OF 1	
ORIGINATED BY RAH	DATE 12/17/97	CHECKED BY	DATE
CALC. NO.		REV. NO.	

SAMPLE CALCULATION FOR DEVELOPING TABLE 5
EXAMPLE CALCULATION USES DATA FROM TABLE 5
AND A FIVE YEAR STORM EVENT.

$$\left[\begin{array}{l} \text{KEWAUNEE} \\ \text{RIVER} \\ \text{DOWN} \\ \text{STREAM} \\ \text{FLOW} \end{array} \times A_s \text{ CONC.} \right] + \left[\begin{array}{l} \text{KEWAUNEE} \\ \text{MARSH} \\ \text{GROUND} \\ \text{WATER} \\ \text{FLOW} \end{array} \times A_s \text{ CONC.} \right] + \left[\begin{array}{l} \text{KEWAUNEE} \\ \text{RIVER} \\ \text{UPSTREAM} \\ \text{FLOW} \end{array} \times A_s \text{ CONC.} \right] = \text{CALCULATED KEWAUNEE MARSH } A_s \text{ CONC.}$$

KEWAUNEE MARSH SURFACE WATER FLOW

$$\left[(4,379.2 \text{ cfs} \times 3.5 \text{ ug/l}) + (0.00009 \text{ cfs} \times 300,000 \text{ ug/l}) + (4,370 \text{ cfs} \times 0 \text{ ug/l}) \right]$$

9.2 cfs

1,659.4 ug/l



November 11, 1996

Mr. James R. Reyburn
Wisconsin Department of Natural Resources
1125 North Military Avenue
P.O. Box 10448
Green Bay, Wisconsin 54307-0448

Re: Preliminary Results of Groundwater Modeling for the C.D. Besadny Arsenic Site,
Kewaunee, Wisconsin -- STS Project No. 20716XA


Dear Jim,


Enclosed are the preliminary results of groundwater modeling. We will also be providing you with preliminary surface water modeling results shortly. We would appreciate it if you would circulate this information for review and comment. Following your review, we would like to arrange a meeting to discuss this information.

If you have any questions or comments regarding this project, please contact me at 406-3210. We appreciate your assistance with this project.

Sincerely,

STS CONSULTANTS LTD.


Michael T. Berger, R.M., CHMM
Microbiologist


Mark A. Bergeon, P.G.
Associate

MTB/dke.wd

Enclosures:
GeoTrans, Inc., Preliminary Modeling Results

Copy to: Mr. Thomas P. McElligott
Quarles & Brady
411 East Wisconsin Avenue
Milwaukee, Wisconsin 53202-4497

(C416A010)

STS Consultants Ltd.
Consulting Engineers

1035 Kepler Drive
Green Bay, Wisconsin 54311-8320
414.468.1978/Fax 414.468.3312

October 10, 1996

Mr. Michael T. Berger
STS Consultants Ltd.
1035 Kepler Drive
Green Bay, Wisconsin 54311

Dear Mike:

Enclosed are preliminary results from the Kewaunee Marsh arsenic transport modeling work. Figures 1 through 3 are potentiometric surface maps for the site based on State water level measurements. Figure 4 is the best fit of measured sediment/water arsenic concentrations to the Freundlich and Langmuir isotherms.

Figures 5 through 12 show the results of the BIO1D model simulations. Figures 5 and 6 show the flow paths used in the BIO1D model simulations. The flow paths are based on flow lines from the potentiometric surface map for May 1996. Figure 6 shows the combined STS and State groundwater arsenic concentration data and the one-dimensional grids used to extrapolate initial concentration data for the start of the model simulations.

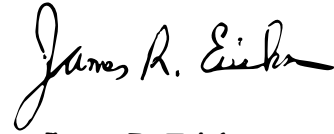
Figure 7 shows the initial concentration data used in the model simulations for the Central Flow Path. Figure 8 shows the arsenic concentration distribution from the upgradient end of the Central Flow Path to the Kewaunee River after 8000 years. Figure 9 shows the concentration breakthrough at the Kewaunee River as a function of time. The maximum concentration discharge to the river is about 300 mg/L after about 2700 years.

Figures 10 through 12 show the transport results for the Northern Flow Path. Figure 10 is the initial starting concentration data for the model simulations. Figure 11 shows the distribution of arsenic concentration in the groundwater after 3000 years and Figure 12 shows the concentration breakthrough at the river as a function of time.

All model simulation were run with the Langmuir isotherm, which is the more conservative of the two isotherms. We plan to perform a sensitivity analysis of the model for both the Freundlich and Langmuir isotherms to demonstrate that the results are not significantly impacted by the choice of isotherms.

I would like to discuss future model runs that STS and State would like to see performed for the Kewaunee Marsh site. Please call me after you have had a chance to review these results.

Sincerely,

A handwritten signature in black ink that reads "James R. Erickson". The signature is written in a cursive style with a large initial "J" and a long horizontal stroke at the end.

James R. Erickson
Principal Hydrogeologist
Boulder Office Manager

Enclosures

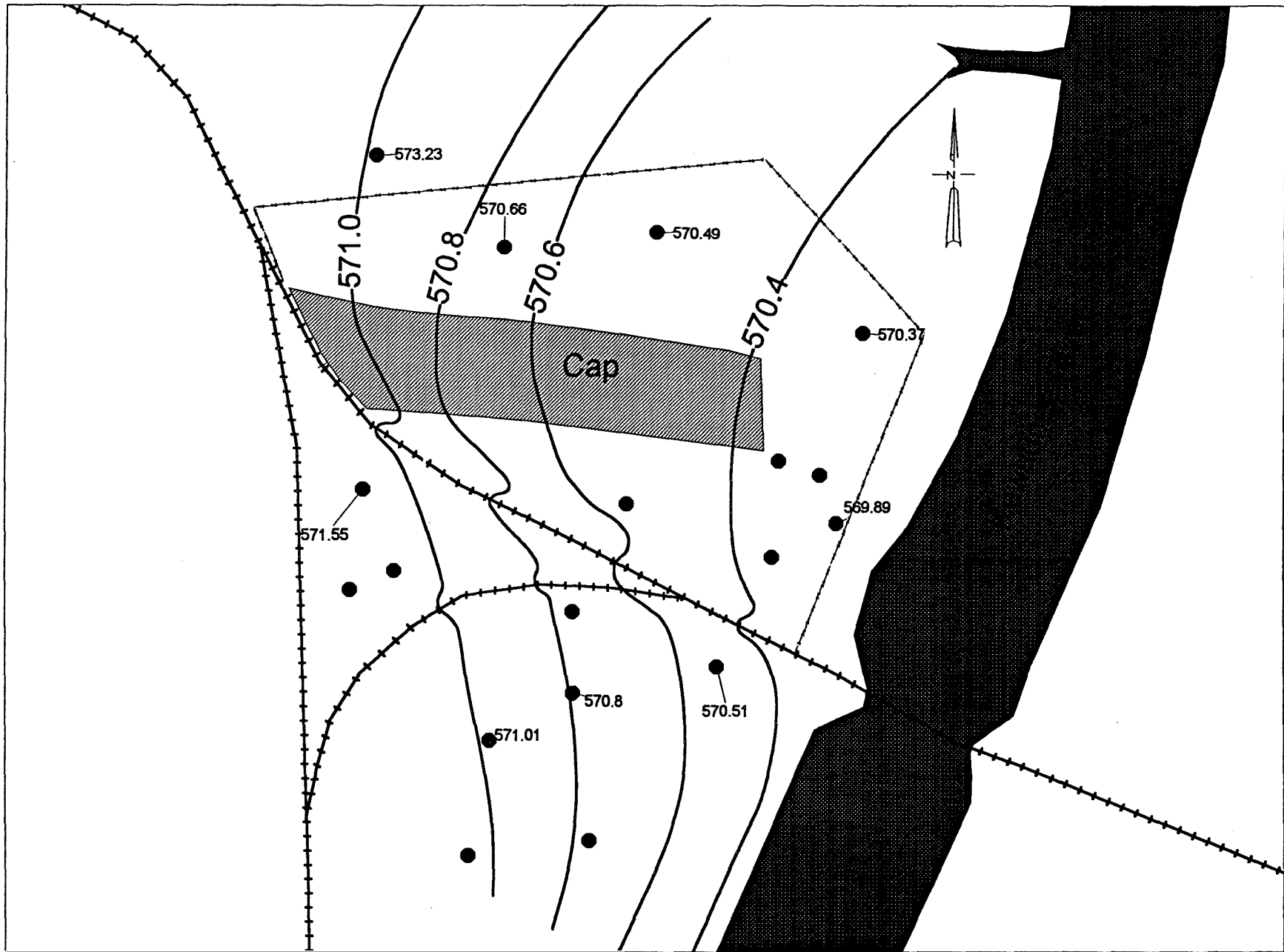


Figure 1. Potentiometric surface based on State water-level measurements at the Kewaunee marsh for May 1996.

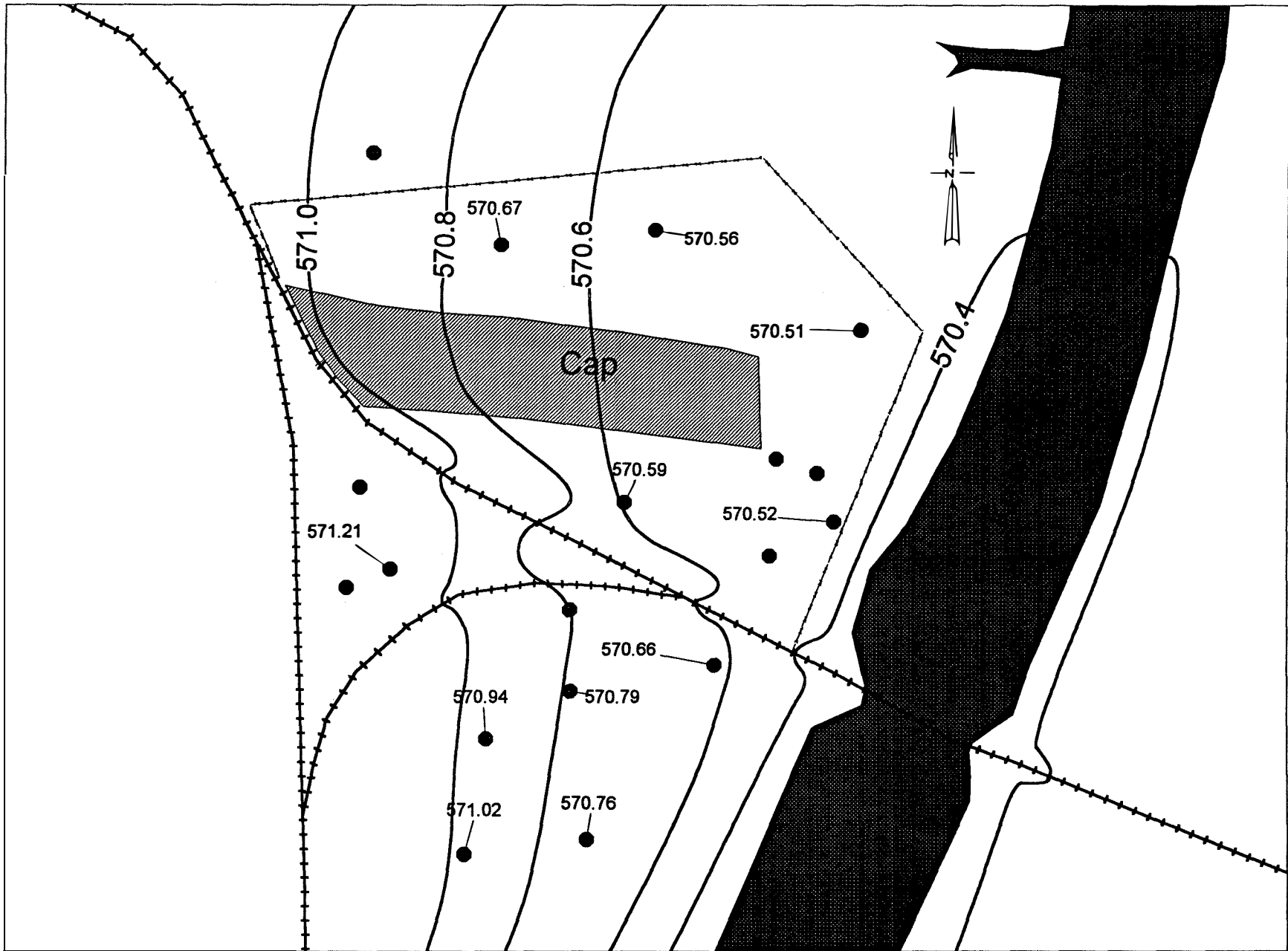


Figure 2. Potentiometric surface based on State water-level measurements at the Kewaunee marsh for August 1996.

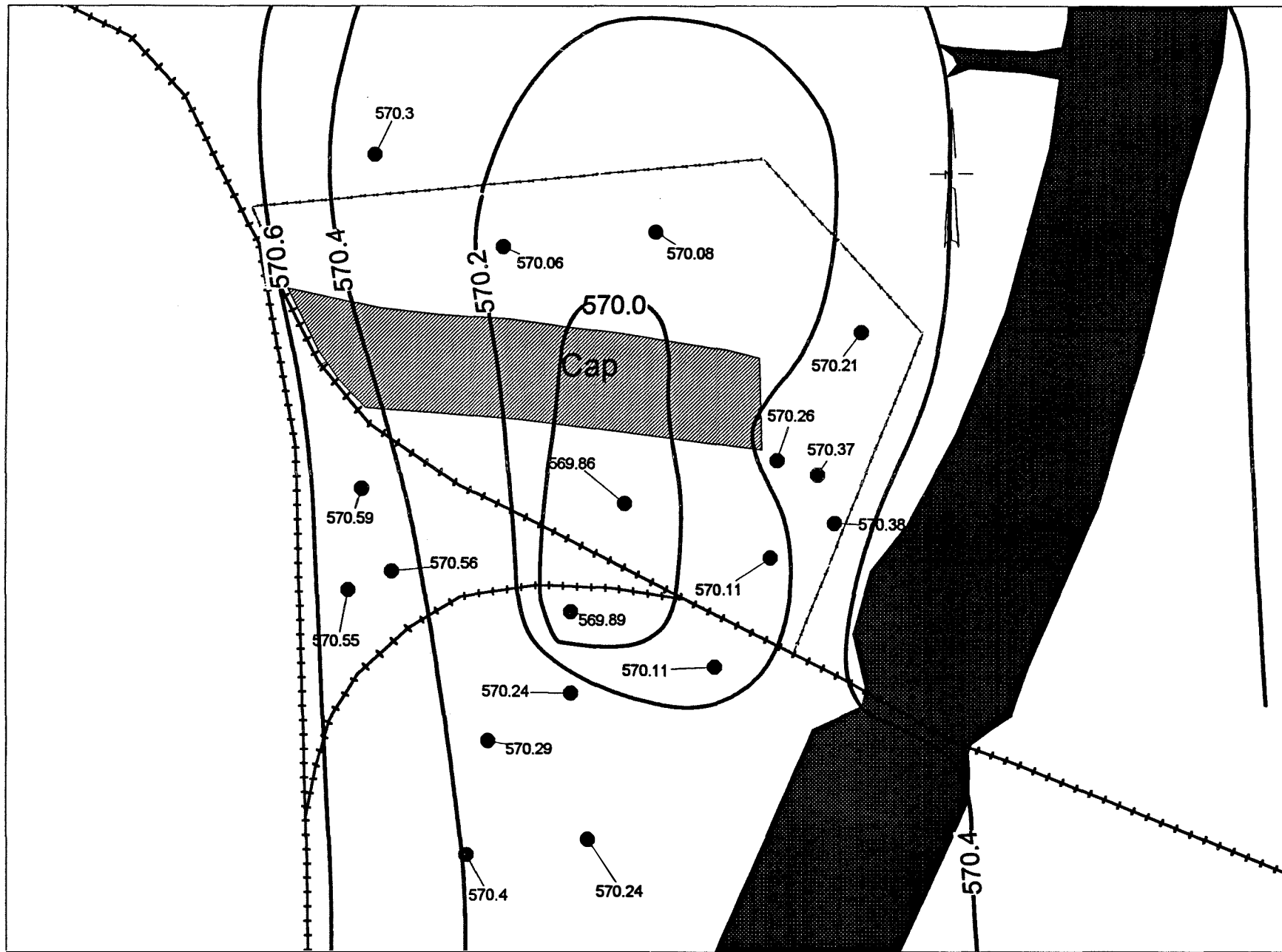


Figure 3. Potentiometric surface based on State water-level measurements at the Kewaunee marsh for September 1996.

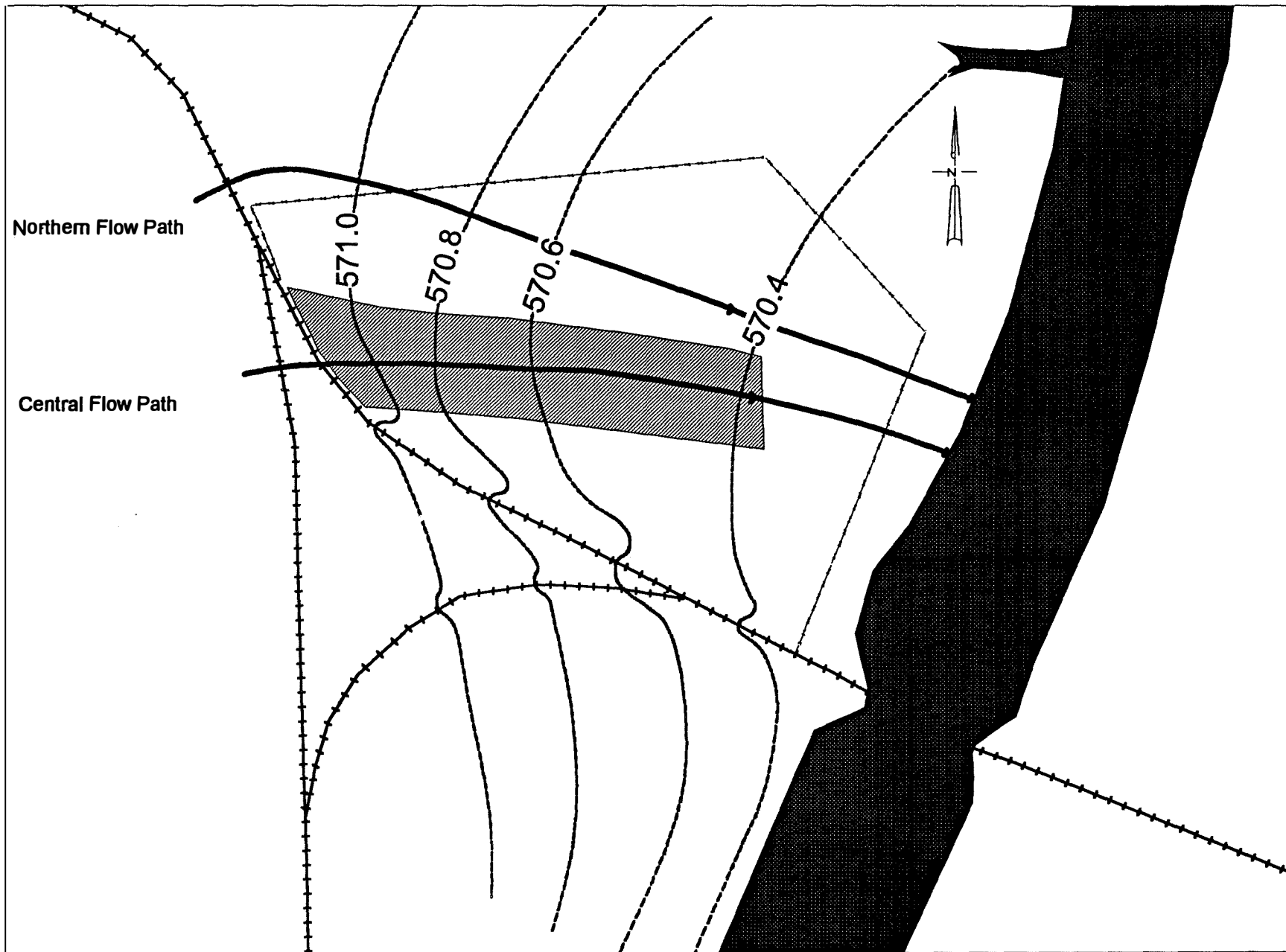


Figure 5. BIO1D flow paths for arsenic transport simulations .

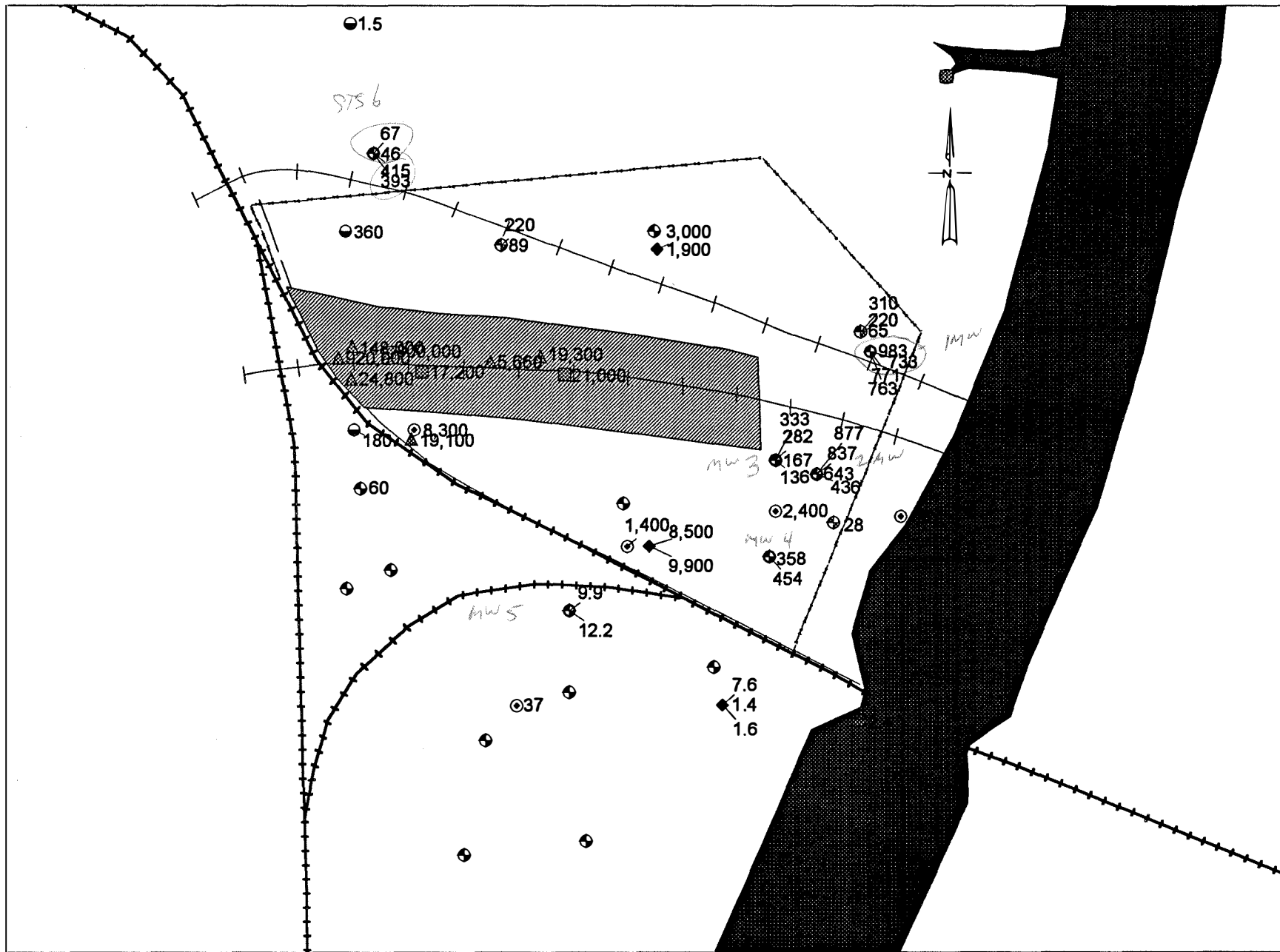
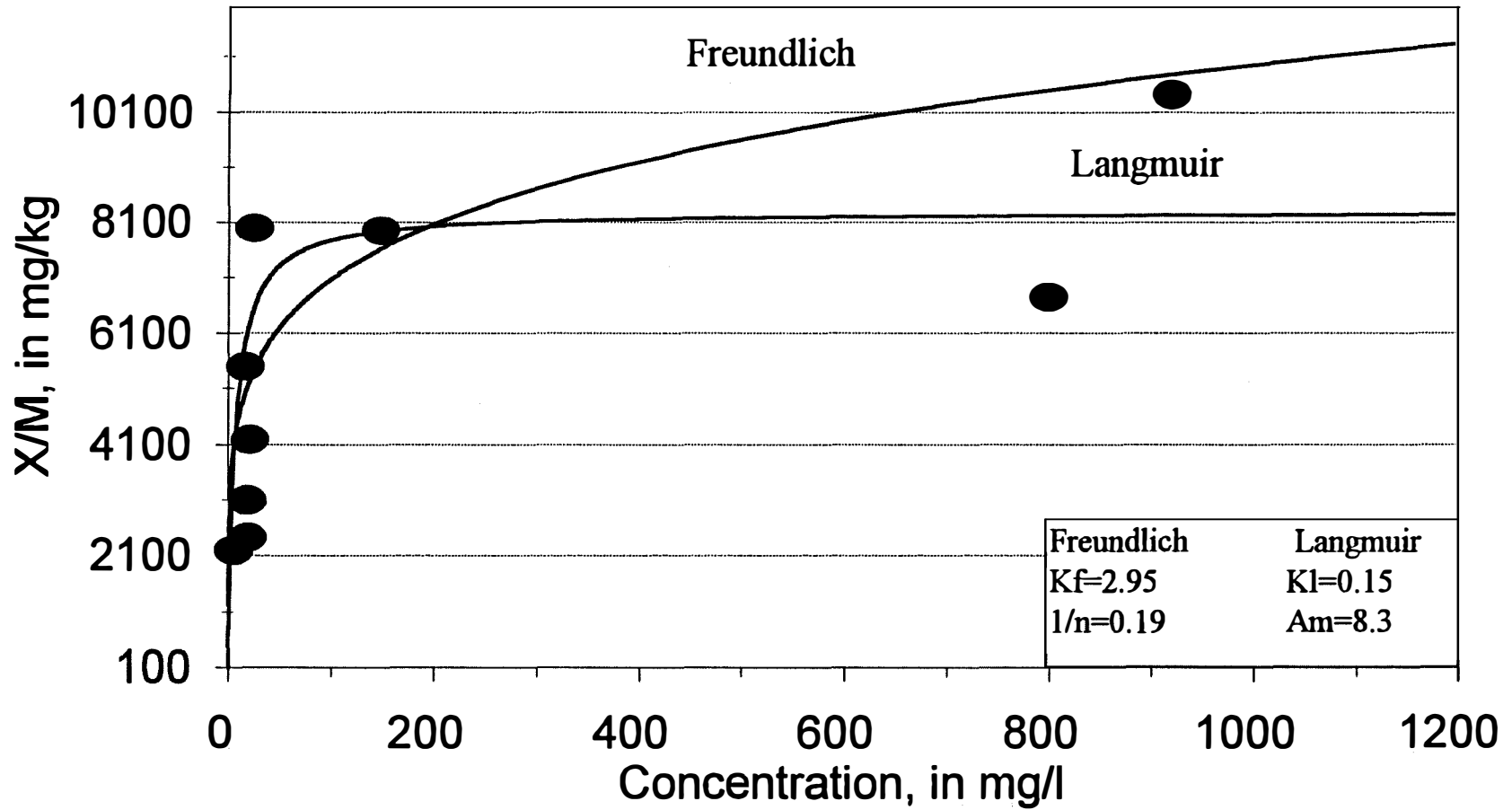


Figure 6. BIO1D flow paths and grid spacings for initial starting groundwater arsenic concentrations.

Figure 4. Measured arsenic concentration data for sediments and water versus the Langmuir and Freundlich calculated data.

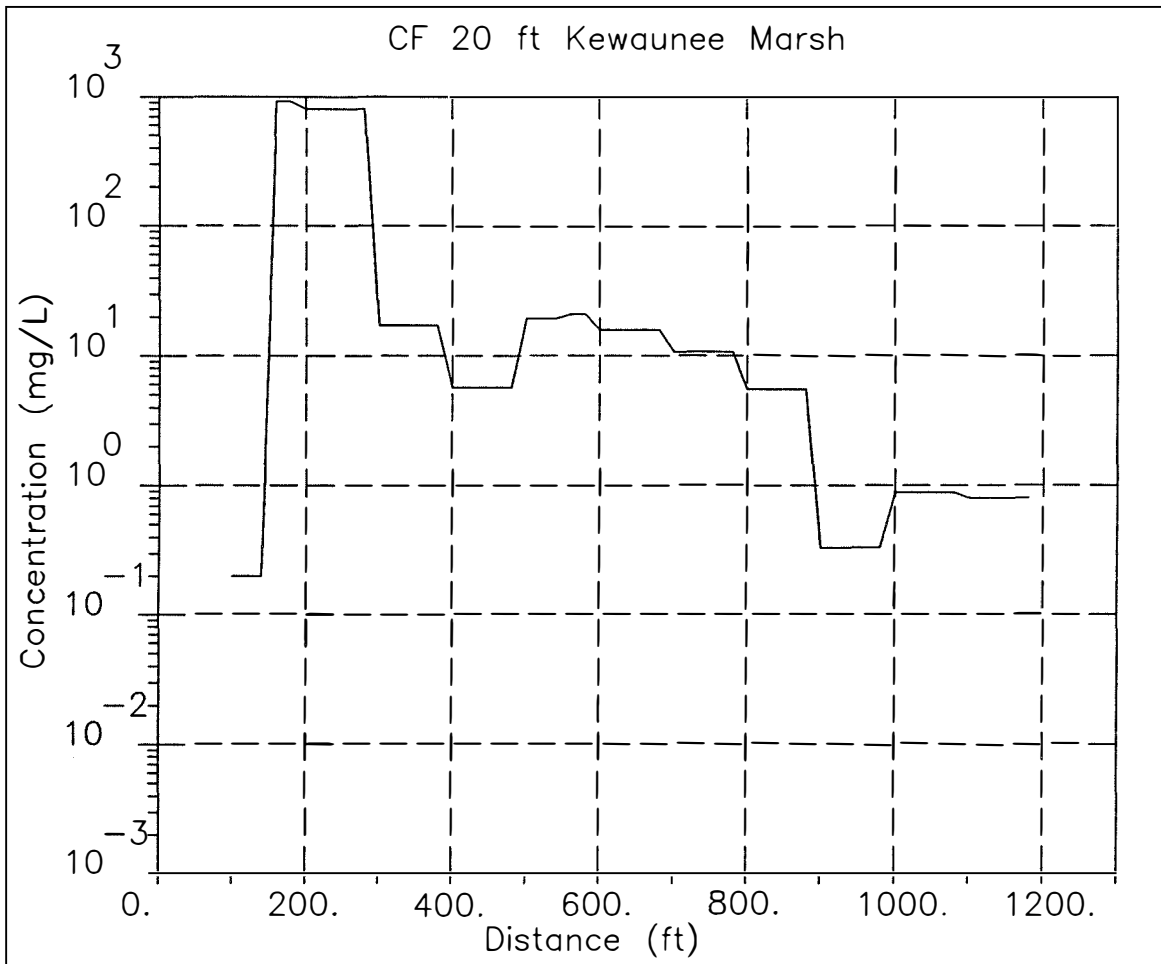


TIME (yr)

 0.00

Description	V	D	Ae	An	Li	Fr	La
Arsenic	<input type="checkbox"/>	<input type="checkbox"/>					<input type="checkbox"/>

BIO1D
 Version 1.2
 GeoTrans, Inc.



CUMULATIVE MASS BALANCE

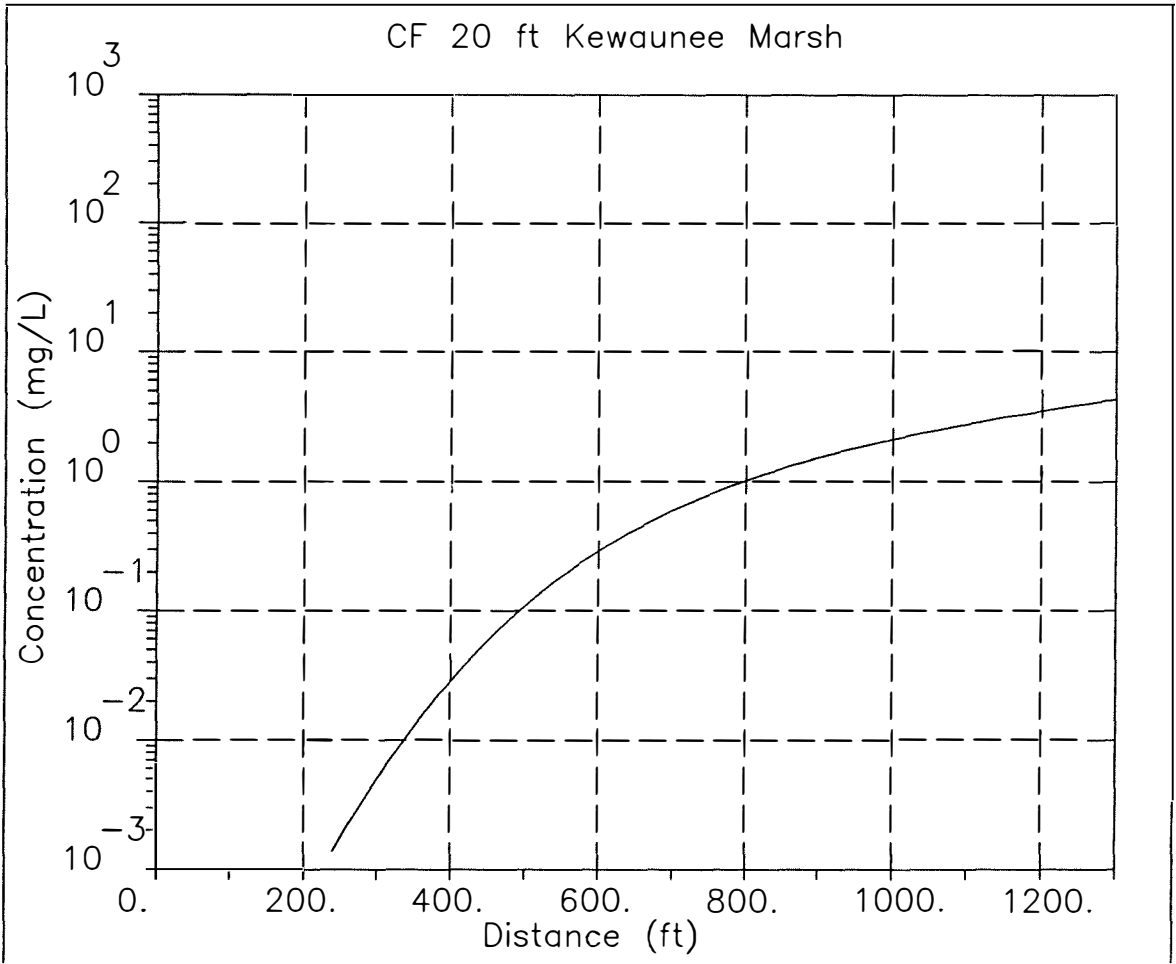
As	
in	out

Figure 7. Initial arsenic concentrations in groundwater at the start of the model simulations for the Central Flow Path.

TIME (yr)
 8000.34

Description	V	D	Ae	An	Li	Fr	La
Arsenic	□	□					□

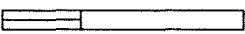
BIO1D
 Version 1.2
 GeoTrans, Inc.



CUMULATIVE MASS BALANCE

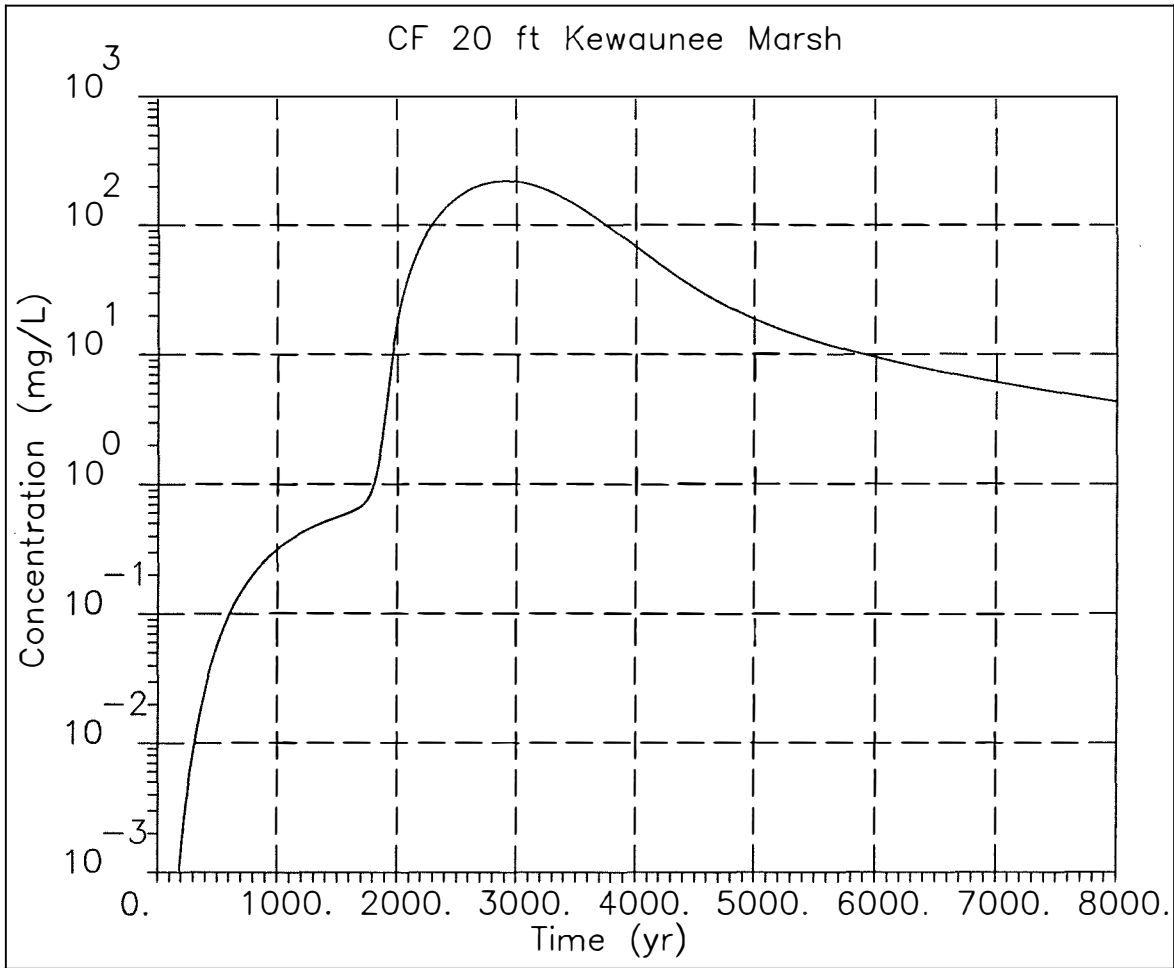
As			
in	out		
DES			
	ADS		
STO			

Figure 8. Groundwater arsenic concentrations as a function of distance for the Central Flow Path.

DISTANCE(ft)

 1300.00

Description	V	D	Ae	An	Li	Fr	La
Arsenic	□	□					□

BIO1D
 Version 1.2
 GeoTrans, Inc.



CUMULATIVE MASS BALANCE

As in	As out		
DIS	DIS		
DES	ADS		
CON	CON		

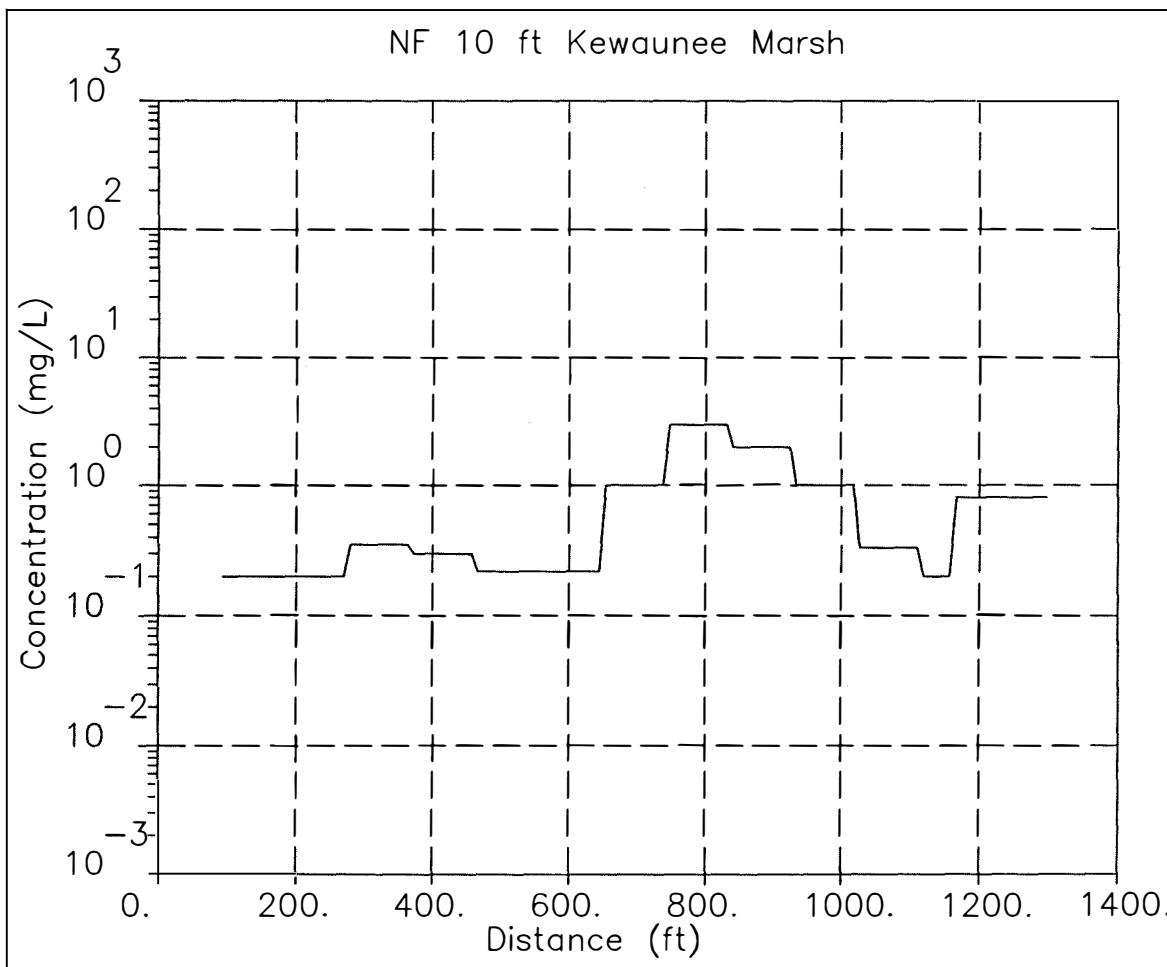
Figure 9. Groundwater arsenic concentrations discharging to river as a function of time for the Central Flow Path.

TIME (yr)

 0.00

Description	V	D	Ae	An	Li	Fr	La
Arsenic	—	□	□				□

BIO1D
 Version 1.2
 GeoTrans, Inc.



CUMULATIVE MASS BALANCE

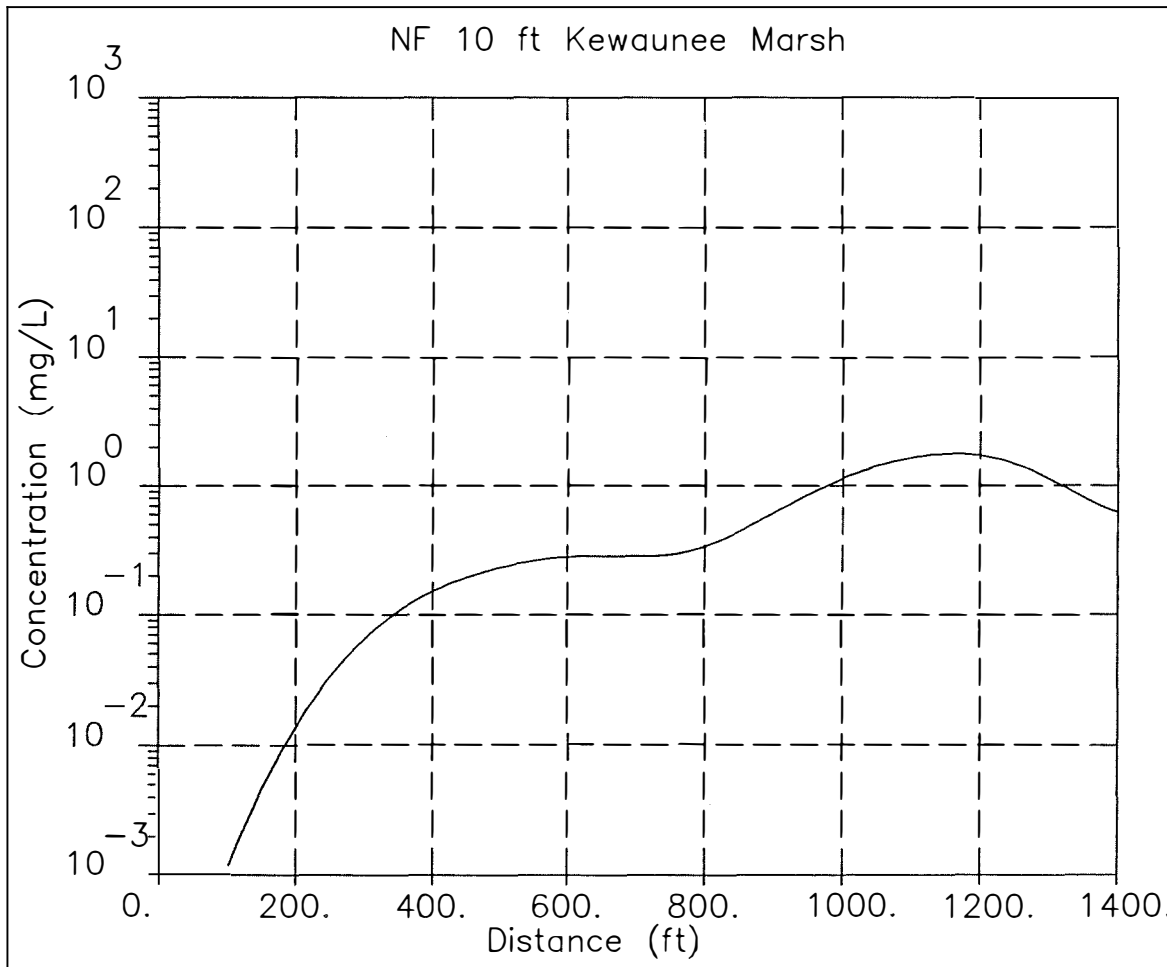
As	
in	out

Figure 10. Initial arsenic concentrations in groundwater at the start of the model simulations for the Northern Flow Path.

TIME (yr)
 3000.10

Description	V	D	Ae	An	Li	Fr	La
Arsenic	□	□					□

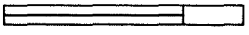
BIO1D
 Version 1.2
 GeoTrans, Inc.



CUMULATIVE MASS BALANCE

As			
in	out		
DES	ADS		
STO			

Figure 11. Groundwater arsenic concentrations as a function of distance between the marsh and river for the Northern Flow Path.

DISTANCE(ft)

 1500.00

Description	V	D	Ae	An	Li	Fr	La
Arsenic	□	□					□

BIO1D
 Version 1.2
 GeoTrans, Inc.

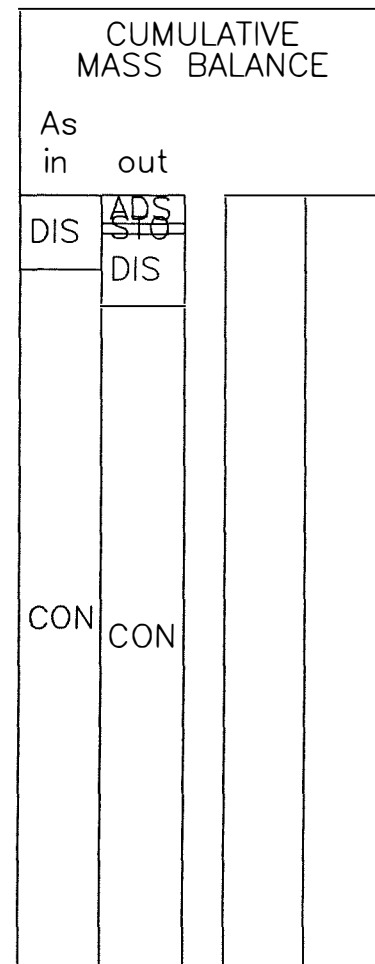
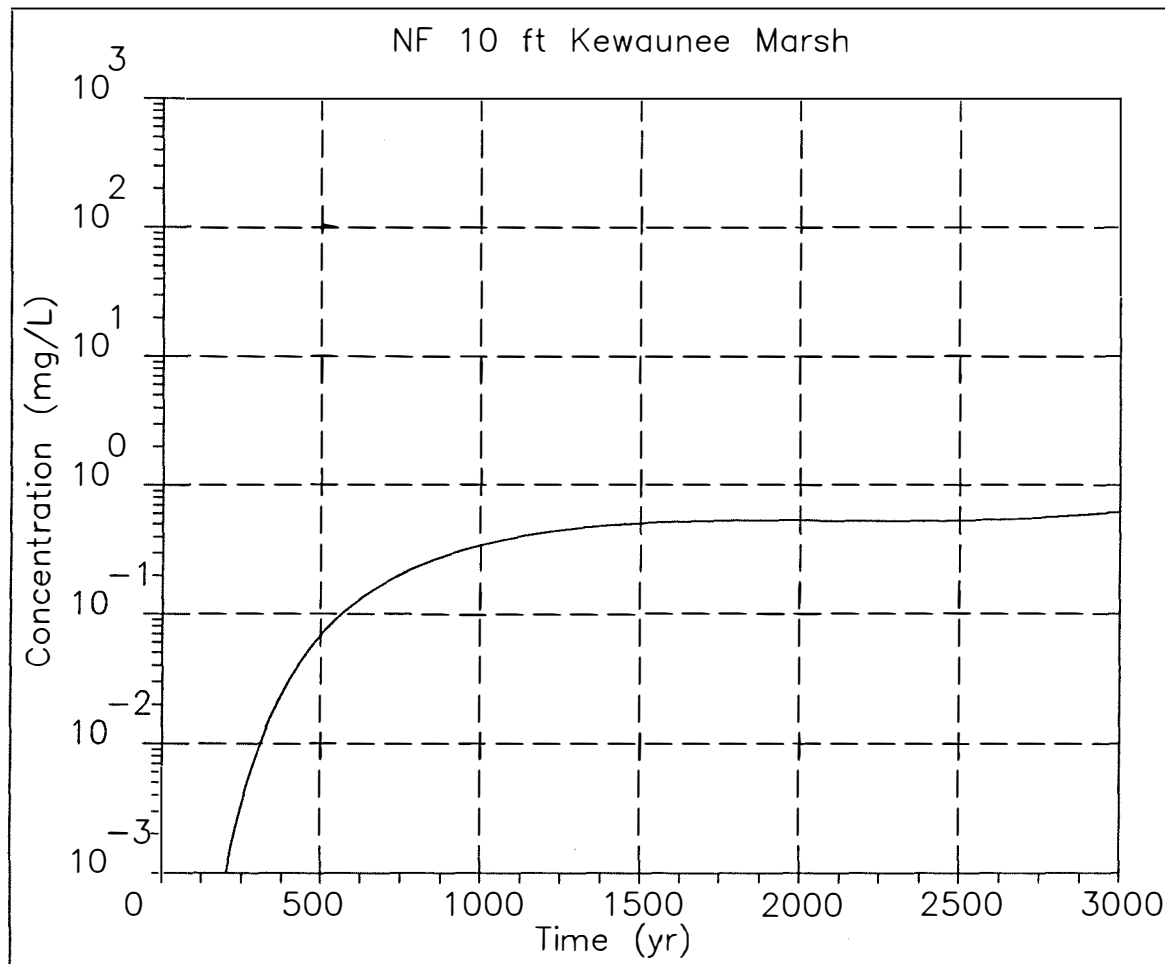


Figure 12. Groundwater arsenic concentrations discharging to the river as a function of time for the Northern Flow Path.

APPENDIX C

Hydrocad Runoff Model Printouts

TYPE II 24-HOUR RAINFALL= 2.4 IN 2yr

Prepared by Applied Microcomputer Systems

12 Nov 96

HydroCAD 4.52 000800 (c) 1986-1996 Applied Microcomputer Systems

WATERSHED ROUTING =====

- SUBCATCHMENT 1 = North Area (marsh) -> POND 1
- SUBCATCHMENT 2 = Central Area and Cap -> POND 1
- SUBCATCHMENT 3 = South Area -> POND 1
- POND 1 = Kewaunee River ->

TYPE II 24-HOUR RAINFALL= 2.4 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

HydroCAD 4.52 000800 (c) 1986-1996 Applied Microcomputer Systems

RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 2.4 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS (%CN)--			WGT'D CN C		PEAK (CFS)	Tpeak (HRS)	VOL (AF)	
1	6.50	95.6	100%83	-	-	-	83	-	2.29	13.08	.47
2	4.57	92.3	79%87	21%83	-	-	86	-	2.02	13.02	.39
3	3.10	80.8	100%83	-	-	-	83	-	1.25	12.89	.22

TYPE II 24-HOUR RAINFALL= 2.4 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

HydroCAD 4.52 000800 (c) 1986-1996 Applied Microcomputer Systems

REACH ROUTING BY STOR-IND+TRANS METHOD

REACH		BOTTOM		SIDE				PEAK	TRAVEL	PEAK
NO.	DIAM	WIDTH	DEPTH	SLOPES	n	LENGTH	SLOPE	VEL.	TIME	Qout
	(IN)	(FT)	(FT)	(FT/FT)		(FT)	(FT/FT)	(FPS)	(MIN)	(CFS)

TYPE II 24-HOUR RAINFALL= 2.4 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

HydroCAD 4.52 000800 (c) 1986-1996 Applied Microcomputer Systems

POND ROUTING BY STOR-IND METHOD

POND NO.	START	FLOOD	PEAK	PEAK	----- PEAK FLOW -----				---Qout---	
	ELEV. (FT)	ELEV. (FT)	ELEV. (FT)	STORAGE (AF)	Qin (CFS)	Qout (CFS)	Qpri (CFS)	Qsec (CFS)	ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.0	1.08	5.52	0.00			100	419.3

TYPE II 24-HOUR RAINFALL= 2.4 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

HydroCAD 4.52 000800 (c) 1986-1996 Applied Microcomputer Systems

LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 2.4 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

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SUBCATCHMENT 1 North Area (marsh)

PEAK= 2.29 CFS @ 13.08 HRS, VOLUME= .47 AF

ACRES	CN	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 2.4 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=1060' s=.001 '/'	Flow thru marsh	95.6

SUBCATCHMENT 2 Central Area and Cap

PEAK= 2.02 CFS @ 13.02 HRS, VOLUME= .39 AF

ACRES	CN	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 2.4 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=780' s=.001 '/'	Wood chips	67.4
CURVE NUMBER (LAG) METHOD L=225' s=.001 '/'	Marsh	24.9

Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 South Area

PEAK= 1.25 CFS @ 12.89 HRS, VOLUME= .22 AF

ACRES	CN	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 2.4 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=860' s=.001 '/'	Marsh	80.8

TYPE II 24-HOUR RAINFALL= 2.4 IN

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POND 1 Kewaunee River

Qin = 5.52 CFS @ 13.01 HRS, VOLUME= 1.08 AF
 Qout= 0.00 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 419.3 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)	STOR-IND METHOD
100.0	30.00	0.00	0.00	PEAK STORAGE = 1.08 AF
110.0	100.00	650.00	650.00	PEAK ELEVATION= 100.0 FT
				FLOOD ELEVATION= 110.0 FT
				START ELEVATION= 100.0 FT
				SPAN= 10-20 HRS, dt=.1 HRS
				Tdet= 378.9 MIN (0 AF)

#	ROUTE	INVERT	OUTLET DEVICES
1	P	100.0'	100" CULVERT
			n=.03 L=100' S=.001'/' Ke=.6 Cc=.9 Cd=.56

TYPE II 24-HOUR RAINFALL= 3.2 IN

5 yr

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WATERSHED ROUTING =====

SUBCATCHMENT 1	= North Area (marsh)	-> POND 1
SUBCATCHMENT 2	= Central Area and Cap	-> POND 1
SUBCATCHMENT 3	= South Area	-> POND 1
POND 1	= Kewaunee River	->

RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 3.2 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS (%CN)--				WGT'D CN	C	PEAK (CFS)	Tpeak (HRS)	VOL (AF)
1	6.50	95.6	100%83	-	-	-	83	-	3.88	13.05	.77
2	4.57	92.3	79%87	21%83	-	-	86	-	3.23	13.00	.62
3	3.10	80.8	100%83	-	-	-	83	-	2.11	12.86	.37

TYPE II 24-HOUR RAINFALL= 3.2 IN

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REACH ROUTING BY STOR-IND+TRANS METHOD

REACH NO.	DIAM (IN)	BOTTOM WIDTH (FT)	DEPTH (FT)	SIDE SLOPES (FT/FT)	n	LENGTH (FT)	SLOPE (FT/FT)	PEAK VEL. (FPS)	TRAVEL TIME (MIN)	PEAK Qout (CFS)
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TYPE II 24-HOUR RAINFALL= 3.2 IN

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POND ROUTING BY STOR-IND METHOD

POND NO.	START	FLOOD	PEAK	PEAK	----- PEAK FLOW -----				---Qout---	
	ELEV. (FT)	ELEV. (FT)	ELEV. (FT)	STORAGE (AF)	Qin (CFS)	Qout (CFS)	Qpri (CFS)	Qsec (CFS)	ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.0	1.76	9.15	.01			100	420.5

TYPE II 24-HOUR RAINFALL= 3.2 IN

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LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 3.2 IN

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SUBCATCHMENT 1 **North Area (marsh)**

PEAK= 3.88 CFS @ 13.05 HRS, VOLUME= .77 AF

ACRES	CN	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=1060' s=.001 '/'	Flow thru marsh	95.6

SUBCATCHMENT 2 **Central Area and Cap**

PEAK= 3.23 CFS @ 13.00 HRS, VOLUME= .62 AF

ACRES	CN	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=780' s=.001 '/'	Wood chips	67.4
CURVE NUMBER (LAG) METHOD L=225' s=.001 '/'	Marsh	24.9

 Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 **South Area**

PEAK= 2.11 CFS @ 12.86 HRS, VOLUME= .37 AF

ACRES	CN	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=860' s=.001 '/'	Marsh	80.8

TYPE II 24-HOUR RAINFALL= 3.2 IN

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POND 1

Kewaunee River

Qin = 9.15 CFS @ 12.99 HRS, VOLUME= 1.77 AF

Qout= .01 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 420.5 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)
100.0	30.00	0.00	0.00
110.0	100.00	650.00	650.00

STOR-IND METHOD
 PEAK STORAGE = 1.76 AF
 PEAK ELEVATION= 100.0 FT
 FLOOD ELEVATION= 110.0 FT
 START ELEVATION= 100.0 FT
 SPAN= 10-20 HRS, dt=.1 HRS
 Tdet= 399.3 MIN (0 AF)

ROUTE INVERT OUTLET DEVICES

1 P 100.0' 100" CULVERT
 n=.03 L=100' S=.001'/' Ke=.6 Cc=.9 Cd=.56

TYPE II 24-HOUR RAINFALL= 3.7 IN 10yr

Prepared by Applied Microcomputer Systems

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WATERSHED ROUTING =====

SUBCATCHMENT 1	= North Area (marsh)	->	POND 1
SUBCATCHMENT 2	= Central Area and Cap	->	POND 1
SUBCATCHMENT 3	= South Area	->	POND 1
POND 1	= Kewaunee River	->	

TYPE II 24-HOUR RAINFALL= 3.7 IN

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RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 3.7 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS (%CN)--			WGT'D CN C		PEAK (CFS)	Tpeak (HRS)	VOL (AF)	
1	6.50	95.6	100%83	-	-	-	83	-	4.93	13.04	.98
2	4.57	92.3	79%87	21%83	-	-	86	-	4.02	12.99	.77
3	3.10	80.8	100%83	-	-	-	83	-	2.68	12.85	.47

TYPE II 24-HOUR RAINFALL= 3.7 IN

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REACH ROUTING BY STOR-IND+TRANS METHOD

REACH NO.	DIAM (IN)	BOTTOM WIDTH (FT)	DEPTH (FT)	SIDE SLOPES (FT/FT)	n	LENGTH (FT)	SLOPE (FT/FT)	PEAK VEL. (FPS)	TRAVEL TIME (MIN)	PEAK Qout (CFS)
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TYPE II 24-HOUR RAINFALL= 3.7 IN

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POND ROUTING BY STOR-IND METHOD

POND NO.	START ELEV. (FT)	FLOOD ELEV. (FT)	PEAK ELEV. (FT)	PEAK STORAGE (AF)	----- Qin (CFS)	PEAK FLOW Qout (CFS)	----- Qpri (CFS)	----- Qsec (CFS)	---Qout--- ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.0	2.22	11.54	.01			100	421.0

TYPE II 24-HOUR RAINFALL= 3.7 IN

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LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 3.7 IN

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SUBCATCHMENT 1 North Area (marsh)

PEAK= 4.93 CFS @ 13.04 HRS, VOLUME= .98 AF

ACRES	CN	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=1060' s=.001 '/'	Flow thru marsh	95.6

SUBCATCHMENT 2 Central Area and Cap

PEAK= 4.02 CFS @ 12.99 HRS, VOLUME= .77 AF

ACRES	CN	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=780' s=.001 '/'	Wood chips	67.4
CURVE NUMBER (LAG) METHOD L=225' s=.001 '/'	Marsh	24.9

Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 South Area

PEAK= 2.68 CFS @ 12.85 HRS, VOLUME= .47 AF

ACRES	CN	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 3.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=860' s=.001 '/'	Marsh	80.8

TYPE II 24-HOUR RAINFALL= 3.7 IN

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POND 1 Kewaunee River

Qin = 11.54 CFS @ 12.98 HRS, VOLUME= 2.22 AF

Qout= .01 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 421.0 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)	STOR-IND METHOD
100.0	30.00	0.00	0.00	PEAK STORAGE = 2.22 AF
110.0	100.00	650.00	650.00	PEAK ELEVATION= 100.0 FT
				FLOOD ELEVATION= 110.0 FT
				START ELEVATION= 100.0 FT
				SPAN= 10-20 HRS, dt=.1 HRS
				Tdet= 402.8 MIN (0 AF)

#	ROUTE	INVERT	OUTLET DEVICES
1	P	100.0'	100" CULVERT
			n=.03 L=100' S=.001'/' Ke=.6 Cc=.9 Cd=.56

TYPE II 24-HOUR RAINFALL= 4.2 IN

Prepared by Applied Microcomputer Systems 25 yr

12 Nov 96

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WATERSHED ROUTING =====

- SUBCATCHMENT 1 = North Area (marsh) -> POND 1
- SUBCATCHMENT 2 = Central Area and Cap -> POND 1
- SUBCATCHMENT 3 = South Area -> POND 1
- POND 1 = Kewaunee River ->

TYPE II 24-HOUR RAINFALL= 4.2 IN

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RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 4.2 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS	(%CN)--	WGT'D CN	C	PEAK (CFS)	Tpeak (HRS)	VOL (AF)	
1	6.50	95.6	100%83	-	-	-	83	6.01	13.03	1.19
2	4.57	92.3	79%87	21%83	-	-	86	4.82	12.99	.93
3	3.10	80.8	100%83	-	-	-	83	3.26	12.84	.57

TYPE II 24-HOUR RAINFALL= 4.2 IN

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REACH ROUTING BY STOR-IND+TRANS METHOD

REACH NO.	DIAM (IN)	BOTTOM WIDTH (FT)	DEPTH (FT)	SIDE SLOPES (FT/FT)	n	LENGTH (FT)	SLOPE (FT/FT)	PEAK VEL. (FPS)	TRAVEL TIME (MIN)	PEAK Qout (CFS)
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TYPE II 24-HOUR RAINFALL= 4.2 IN

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POND ROUTING BY STOR-IND METHOD

POND NO.	START	FLOOD	PEAK	PEAK	----- PEAK FLOW -----				---Qout---	
	ELEV. (FT)	ELEV. (FT)	ELEV. (FT)	STORAGE (AF)	Qin (CFS)	Qout (CFS)	Qpri (CFS)	Qsec (CFS)	ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.0	2.68	13.98	.01			100	421.4

TYPE II 24-HOUR RAINFALL= 4.2 IN

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LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 4.2 IN

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SUBCATCHMENT 1 North Area (marsh)

PEAK= 6.01 CFS @ 13.03 HRS, VOLUME= 1.19 AF

<u>ACRES</u>	<u>CN</u>	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD	Flow thru marsh	95.6
L=1060' s=.001 '/'		

SUBCATCHMENT 2 Central Area and Cap

PEAK= 4.82 CFS @ 12.99 HRS, VOLUME= .93 AF

<u>ACRES</u>	<u>CN</u>	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD	Wood chips	67.4
L=780' s=.001 '/'		
CURVE NUMBER (LAG) METHOD	Marsh	24.9
L=225' s=.001 '/'		

 Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 South Area

PEAK= 3.26 CFS @ 12.84 HRS, VOLUME= .57 AF

<u>ACRES</u>	<u>CN</u>	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.2 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD	Marsh	80.8
L=860' s=.001 '/'		

TYPE II 24-HOUR RAINFALL= 4.2 IN

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POND 1 Kewaunee River

Qin = 13.98 CFS @ 12.98 HRS, VOLUME= 2.69 AF

Qout= .01 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 421.4 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)	STOR-IND METHOD
100.0	30.00	0.00	0.00	PEAK STORAGE = 2.68 AF
110.0	100.00	650.00	650.00	PEAK ELEVATION= 100.0 FT
				FLOOD ELEVATION= 110.0 FT
				START ELEVATION= 100.0 FT
				SPAN= 10-20 HRS, dt=.1 HRS
				Tdet= 403 MIN (0 AF)

#	ROUTE	INVERT	OUTLET DEVICES
1	P	100.0'	100" CULVERT
			n=.03 L=100' S=.001'/ ' Ke=.6 Cc=.9 Cd=.56

TYPE II 24-HOUR RAINFALL= 4.7 IN

SOYR

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12 Nov 96

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WATERSHED ROUTING =====

SUBCATCHMENT 1	= North Area (marsh)	->	POND 1
SUBCATCHMENT 2	= Central Area and Cap	->	POND 1
SUBCATCHMENT 3	= South Area	->	POND 1
POND 1	= Kewaunee River	->	

TYPE II 24-HOUR RAINFALL= 4.7 IN

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RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 4.7 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS (%CN)--			WGT'D CN	C	PEAK (CFS)	Tpeak (HRS)	VOL (AF)	
1	6.50	95.6	100%83	-	-	-	83	-	7.11	13.03	1.40
2	4.57	92.3	79%87	21%83	-	-	86	-	5.63	12.98	1.08
3	3.10	80.8	100%83	-	-	-	83	-	3.86	12.84	.67

TYPE II 24-HOUR RAINFALL= 4.7 IN

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REACH ROUTING BY STOR-IND+TRANS METHOD

REACH		BOTTOM		SIDE				PEAK	TRAVEL	PEAK
NO.	DIAM	WIDTH	DEPTH	SLOPES	n	LENGTH	SLOPE	VEL.	TIME	Qout
	(IN)	(FT)	(FT)	(FT/FT)		(FT)	(FT/FT)	(FPS)	(MIN)	(CFS)

TYPE II 24-HOUR RAINFALL= 4.7 IN

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POND ROUTING BY STOR-IND METHOD

POND NO.	START ELEV. (FT)	FLOOD ELEV. (FT)	PEAK ELEV. (FT)	PEAK STORAGE (AF)	----- Qin (CFS)	PEAK FLOW Qout (CFS)	----- Qpri (CFS)	----- Qsec (CFS)	---Qout--- ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.0	3.15	16.46	.01			100	421.7

TYPE II 24-HOUR RAINFALL= 4.7 IN

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LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 4.7 IN

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SUBCATCHMENT 1 North Area (marsh)

PEAK= 7.11 CFS @ 13.03 HRS, VOLUME= 1.40 AF

ACRES	CN	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=1060' s=.001 '/'	Flow thru marsh	95.6

SUBCATCHMENT 2 Central Area and Cap

PEAK= 5.63 CFS @ 12.98 HRS, VOLUME= 1.08 AF

ACRES	CN	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=780' s=.001 '/'	Wood chips	67.4
CURVE NUMBER (LAG) METHOD L=225' s=.001 '/'	Marsh	24.9

 Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 South Area

PEAK= 3.86 CFS @ 12.84 HRS, VOLUME= .67 AF

ACRES	CN	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 4.7 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=860' s=.001 '/'	Marsh	80.8

TYPE II 24-HOUR RAINFALL= 4.7 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

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POND 1

Kewaunee River

Qin = 16.46 CFS @ 12.97 HRS, VOLUME= 3.16 AF

Qout= .01 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 421.7 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)	STOR-IND METHOD
100.0	30.00	0.00	0.00	PEAK STORAGE = 3.15 AF
110.0	100.00	650.00	650.00	PEAK ELEVATION= 100.0 FT
				FLOOD ELEVATION= 110.0 FT
				START ELEVATION= 100.0 FT
				SPAN= 10-20 HRS, dt=.1 HRS
				Tdet= 400.8 MIN (0 AF)

#	ROUTE	INVERT	OUTLET DEVICES
1	P	100.0'	100" CULVERT
			n=.03 L=100' S=.001'/' Ke=.6 Cc=.9 Cd=.56

TYPE II 24-HOUR RAINFALL= 5.0 IN 100yr

Prepared by Applied Microcomputer Systems

12 Nov 96

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WATERSHED ROUTING =====

SUBCATCHMENT 1	= North Area (marsh)	-> POND 1
SUBCATCHMENT 2	= Central Area and Cap	-> POND 1
SUBCATCHMENT 3	= South Area	-> POND 1
POND 1	= Kewaunee River	->

TYPE II 24-HOUR RAINFALL= 5.0 IN

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RUNOFF BY SCS TR-20 METHOD: TYPE II 24-HOUR RAINFALL= 5.0 IN, SCS U.H.

RUNOFF SPAN = 10-20 HRS, dt= .10 HRS, 101 POINTS

SUBCAT NUMBER	AREA (ACRE)	Tc (MIN)	--GROUND COVERS (%CN)--				WGT'D CN	C	PEAK (CFS)	Tpeak (HRS)	VOL (AF)
1	6.50	95.6	100%83	-	-	-	83	-	7.77	13.02	1.53
2	4.57	92.3	79%87	21%83	-	-	86	-	6.12	12.98	1.17
3	3.10	80.8	100%83	-	-	-	83	-	4.22	12.84	.73

TYPE II 24-HOUR RAINFALL= 5.0 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

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REACH ROUTING BY STOR-IND+TRANS METHOD

REACH		BOTTOM		SIDE				PEAK	TRAVEL	PEAK
NO.	DIAM	WIDTH	DEPTH	SLOPES	n	LENGTH	SLOPE	VEL.	TIME	Qout
	(IN)	(FT)	(FT)	(FT/FT)		(FT)	(FT/FT)	(FPS)	(MIN)	(CFS)

TYPE II 24-HOUR RAINFALL= 5.0 IN

Prepared by Applied Microcomputer Systems

12 Nov 96

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POND ROUTING BY STOR-IND METHOD

POND NO.	START	FLOOD	PEAK	PEAK	----- PEAK FLOW -----				---Qout---	
	ELEV. (FT)	ELEV. (FT)	ELEV. (FT)	STORAGE (AF)	Qin (CFS)	Qout (CFS)	Qpri (CFS)	Qsec (CFS)	ATTEN. (%)	LAG (MIN)
1	100.0	110.0	100.1	3.43	17.96	.01			100	421.8

TYPE II 24-HOUR RAINFALL= 5.0 IN

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LINK

Qout

NO. NAME

SOURCE

(CFS)

TYPE II 24-HOUR RAINFALL= 5.0 IN

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SUBCATCHMENT 1 North Area (marsh)

PEAK= 7.77 CFS @ 13.02 HRS, VOLUME= 1.53 AF

ACRES	CN	
6.50	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 5.0 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=1060' s=.001 '/'	Flow thru marsh	95.6

SUBCATCHMENT 2 Central Area and Cap

PEAK= 6.12 CFS @ 12.98 HRS, VOLUME= 1.17 AF

ACRES	CN	
3.60	87	Wood Chip Cap
.97	83	Marsh
4.57	86	

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 5.0 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=780' s=.001 '/'	Wood chips	67.4
CURVE NUMBER (LAG) METHOD L=225' s=.001 '/'	Marsh	24.9

 Total Length= 1005 ft Total Tc= 92.3

SUBCATCHMENT 3 South Area

PEAK= 4.22 CFS @ 12.84 HRS, VOLUME= .73 AF

ACRES	CN	
3.10	83	Marsh

SCS TR-20 METHOD
 TYPE II 24-HOUR
 RAINFALL= 5.0 IN
 SPAN= 10-20 HRS, dt=.1 HRS

Method	Comment	Tc (min)
CURVE NUMBER (LAG) METHOD L=860' s=.001 '/'	Marsh	80.8

TYPE II 24-HOUR RAINFALL= 5.0 IN

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POND 1

Kewaunee River

Qin = 17.96 CFS @ 12.97 HRS, VOLUME= 3.44 AF

Qout= .01 CFS @ 20.00 HRS, VOLUME= 0.00 AF, ATTEN=100%, LAG= 421.8 MIN

ELEVATION (FT)	AREA (AC)	INC.STOR (AF)	CUM.STOR (AF)	STOR-IND METHOD
100.0	30.00	0.00	0.00	PEAK STORAGE = 3.43 AF
110.0	100.00	650.00	650.00	PEAK ELEVATION= 100.1 FT
				FLOOD ELEVATION= 110.0 FT
				START ELEVATION= 100.0 FT
				SPAN= 10-20 HRS, dt=.1 HRS
				Tdet= 402.6 MIN (0 AF)

#	ROUTE	INVERT	OUTLET DEVICES
1	P	100.0'	100" CULVERT
			n=.03 L=100' S=.001'/' Ke=.6 Cc=.9 Cd=.56